

22/24-101

LOCATION NOT CHECKED

ORIGINAL -
File Original, Duplicate and Triplicate with the
REGIONAL WATER POLLUTION
CONTROL BOARD No. _____
(Insert appropriate number)

WATER WELL DRILLERS REPORT

(Sections 7076, 7077, 7078, Water Code)

STATE OF CALIFORNIA

Do Not Fill In
No 66984

State Well No. _____
Other Well No. 22/24-101

(1) OWNER:

Name Mrs. C. P. Mauser
Address 447 E/ Poplar Rd.
Porterville, Calif.

(2) LOCATION OF WELL:

County Tulare Owner's number, if any—
R. F. D. or Street No.

(3) TYPE OF WORK (check):

New Well Deepening Reconditioning Abandon

If abandonment, describe material and procedure in Item 11.

(4) PROPOSED USE (check):

Domestic Industrial Municipal
Irrigation Test Well Other

(5) EQUIPMENT:

Rotary
Cable
Dug Well

(6) CASING INSTALLED:

SINGLE <input checked="" type="checkbox"/> DOUBLE <input type="checkbox"/>				Gage or Wall	If gravel packed		
From	ft. to	ft.	Diam.		Diameter of Bore	from ft.	to ft.
480'			3/16" Wall				
Type and size of shoe or well ring				Size of gravel: 6-20			
Describe joint				78 ton			

(7) PERFORATIONS:

Type of perforator used			
Size	of perforations	in., length, by	in.
From	ft. to	ft.	Rows per ft.
480'		700 ft.	
" 220' perforated			

(8) CONSTRUCTION:

Was a surface sanitary seal provided? Yes No To what depth _____ ft.
Were any strata sealed against pollution? Yes No If yes, note depth of strata _____
From _____ ft. to _____ ft.
Method of Sealing _____

(9) WATER LEVELS:

Depth at which water was first found 90 ft.
Standing level before perforating _____ ft.
Standing level after perforating _____ ft.

(10) WELL TESTS:

Was a pump test made? Yes No If yes, by whom?
Yield: _____ gal./min. with _____ ft. draw down after _____ hrs.
Temperature of water _____ Was a chemical analysis made? Yes No
Was electric log made of well? Yes No

(11) WELL LOG:

Total depth 720 ft. Depth of completed well 700 ft.

Formations: Describe by color, character, size of material, and structure.

0 ft. to	50 ft.	
0	50	Sandy clay
50	140	Sand, clay strks.
140	152	Clay
152	230	Sand, clay strks.
230	245	Clay
245	320	Sand
320	328	Clay
328	420	Sand, clay strks.
420	440	Clay
440	550	Sand
550	572	Hard sand
572	720	Sand, clay strks.

REGISTRATION NO. 7076.1, Water Code

Work started Jan. 23 1961. Completed Feb. 7 1961

WELL DRILLER'S STATEMENT:

This well was drilled under my jurisdiction and this report is true to the best of my knowledge and belief.

NAME Knapp & Graham, Inc.
(Person, firm, or corporation) (Typed or printed)
Address 1155 W. Inyo St.
Tulare, Calif.

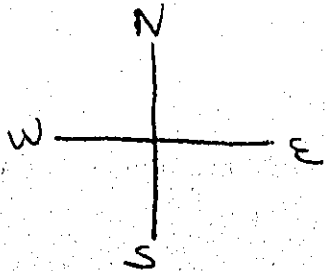
[SIGNED] _____
License No. 193493 Dated Feb. 8, 1961

22/24-1Q1

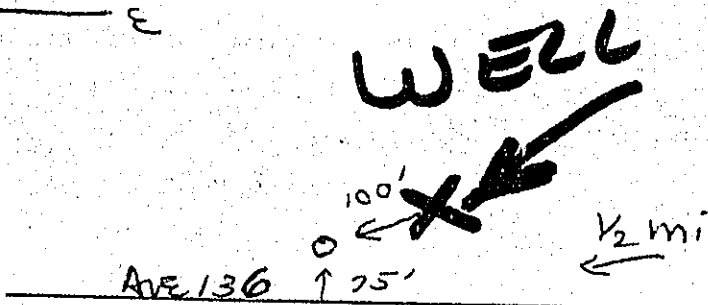
LOCATION OF
well

Log # 66984

MRS. C. P. MAUSER
447 E. Poplar Rd
Porterwille



WELL



Tipton
LOCATION NOT CHECKED

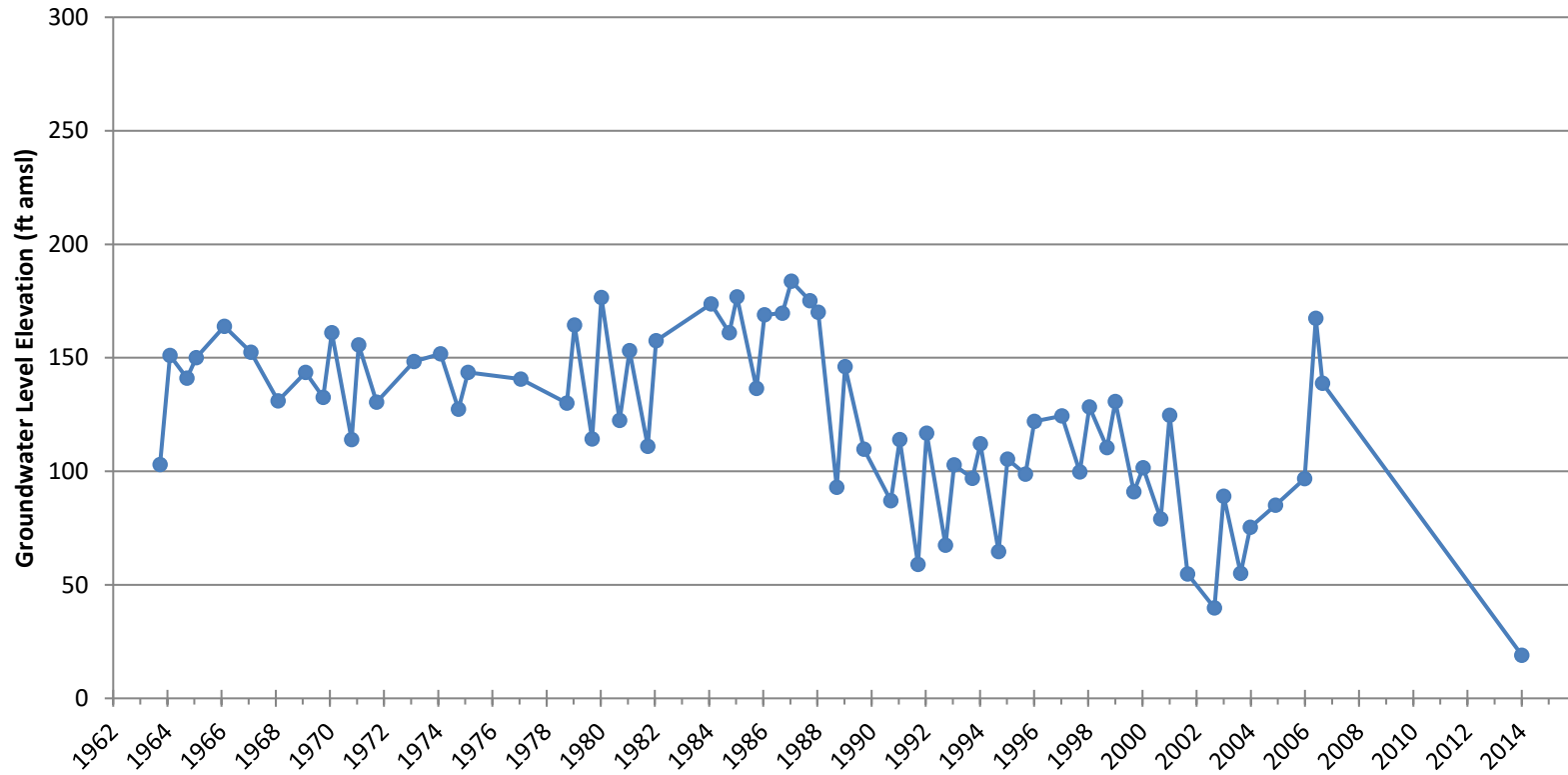
CONFIDENTIAL
Section 7076.1 Water Code

Sec 1
T22SR 24E

Pixley

Groundwater Hydrographs - Deep

22S/24E-01Q01



ORIGINAL
File with DW

24/27-86

WATER WELL DRILLERS REPORT

(Sections 7079, 7080, 7081, 7082, Water Code)

Do Not Fill In

No. 337

THE RESOURCES AGENCY OF CALIFORNIA DEPARTMENT OF WATER RESOURCES

State Well No. _____
Other Well No. 245/275-86

(1) OWNER:
Name Marko Zaninovich, Inc.
Address Rt. 1, Box 725
Delano, Calif. 93215

(2) LOCATION OF WELL:
County Tulare Owner's number, if any _____
Township, Range, and Section _____
Distance from cities, roads, railroads, etc. 1/2 mile North of Ave.
32 and 1/2 mile East of Rd. 216

(3) TYPE OF WORK (check):
New Well Deepening Reconditioning Destroying
If destruction, describe material and procedure in Item 11.

(4) PROPOSED USE (check):
Domestic Industrial Municipal
Irrigation Test Well Other

(5) EQUIPMENT:
Rotary
Cable
Other

(6) CASING INSTALLED:

STEEL:		OTHER:		If gravel packed			
From ft.	To ft.	Diam.	Gage or Wall	Diameter of Bore	From ft.	To ft.	
0	703	16"	1/4"	25 1/2	top	bottom	
703	1747	14"	1/4"				
16" to 14" slip jt.							

Size of shoe or well ring: _____ Size of gravel: 1/4"

Describe joint: collar w/ fillet weld.

(7) PERFORATIONS OR SCREEN:
Type of perforation or name of screen machine

From ft.	To ft.	Perf. per row	Rows per ft.	Size in. x in.
522	703	2	16	.100 x 2
703	1747	2	14	.100 x 2

CONFIDENTIAL
Water Code Sec. 13752

(8) CONSTRUCTION:
Was a surface sanitary seal provided? Yes No To what depth _____ ft.
Were any strata sealed against pollution? Yes No If yes, note depth of strata _____
From _____ ft. to _____ ft.
From _____ ft. to _____ ft.
Method of sealing _____

(9) WATER LEVELS:
Depth at which water was first found, if known unknown.
Standing level before perforating, if known _____ ft.
Standing level after perforating and developing _____ ft.

(10) WELL TESTS:
Was pump test made? Yes No If yes, by whom?
Yield: _____ gal./min. with _____ ft. drawdown after _____ hrs.
Temperature of water _____ Was a chemical analysis made? Yes No
Was electric log made of well? Yes No If yes, attach copy

(11) WELL LOG:

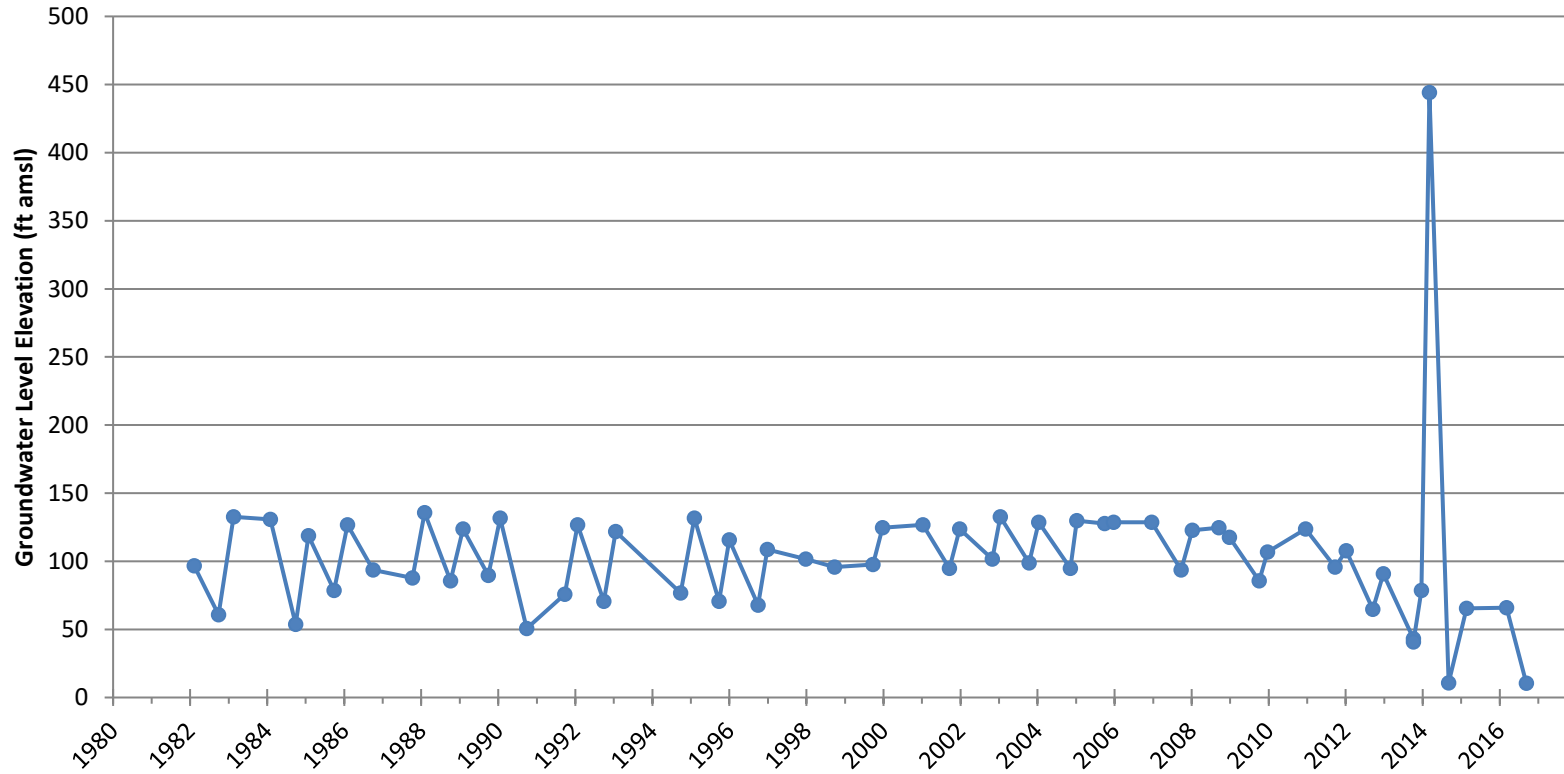
Total depth	ft.	Depth of completed well	ft.
1747		1747	
Formation: Describe by color, character, size of material, and structure			
0 ft. to	9 ft.	top soil	
9	60	sandy clay	
60	63	sand	
63	253	sandy clay	
253	257	sand	
257	473	sandy clay	
473	479	sand	
479	695	sandy clay	
695	745	blue clay	
745	748	sand	
748	812	blue clay	
812	943	sandy clay	
943	1033	sediment	
1033	1246	shale & clay	
1246	1361	blue clay	
1361	1371	hard shale	
1371	1455	shale & clay	
1455	1488	hard shale	
1488	1588	hard shale & clay	
1588	1729	hard sand	
1729	1747	sand & clay	

Work started 11/1/67 . Completed 11/14/67
WELL DRILLER'S STATEMENT:
This well was drilled under my jurisdiction and this report is true to the best of my knowledge and belief.
NAME Whitten Pumps, Inc.
(Person, firm, or corporation) (Typed or printed)
Address 1744 Inyo St.
Delano, Calif. 93215
[SIGNED] *Donald E. Whitten*
(Well Driller)
License No. 148282 Dated 11/13/68, 19__

SKETCH LOCATION OF WELL ON REVERSE SIDE

Groundwater Hydrographs - Deep

24S/27E-08L01



24/27-32KI

DUPLICATE
File Original, Duplicate and Triplicate with the
REGIONAL WATER POLLUTION
CONTROL BOARD No. 5
(Insert appropriate number)

WATER WELL DRILLERS REPORT

(Sections 7076, 7077, 7078, Water Code)

24/27-32KI (G.S.)
STATE OF CALIFORNIA

LOCATION NOT CHECKED

Do Not Fill In

No. 32108

State Well No.

Other Well No. 245/27E-32

1) OWNER:

Name Earl Thomas Enterprises

Address Rt. 2 Box 296

Delano, California

(2) LOCATION OF WELL:

County Tulare Owner's number, if any—

R. F. D. or Street No.

SE 1/4 Section 32

Township 24S

Range 27E

(3) TYPE OF WORK (check):

New well Deepening Reconditioning Abandon

If abandonment, describe material and procedure in Item 11.

(4) PROPOSED USE (check):

Domestic Industrial Municipal

Irrigation Test Well Other

(5) EQUIPMENT:

Rotary

Cable

Dug Well

(6) CASING INSTALLED:

SINGLE DOUBLE

From 1800 ft. to 0 ft. Dism.

If gravel packed

Diameter of Bore 26" from 0 to 1800 ft.

Type and size of shoe or well ring

Describe joint

Size of gravel: 3/8"

(7) PERFORATIONS:

Type of perforator used Machine

Size of perforations 1/8" x 1" cc in., length, by

From 1002 ft. to 1800 ft. Perf. per row Rows per ft.

(8) CONSTRUCTION:

Was a surface sanitary seal provided? Yes No To what depth ft.

Were any strata sealed against pollution? Yes No If yes, note depth of strata

From ft. to ft.

Method of Sealing

(9) WATER LEVELS:

Depth at which water was first found ft.

Standing level before perforating ft.

Standing level after perforating ft.

(10) WELL TESTS:

Was a pump test made? Yes No If yes, by whom?

Yield: gal./min. with ft. draw down after hrs.

Temperature of water Was a chemical analysis made? Yes No

Was electric log made of well? Yes No

(11) WELL LOG:

Total depth 1800 ft. ft. Depth of completed well 1800 ft. ft.

Formations: Describe by color, character, size of material, and structure.

0 ft. to	3 ft.	Formation
0	3	Top Soil
3	180	Sandy Clay
180	183	Sand
183	240	Hard Sand
240	310	Sandy Clay
310	356	Hard Clay
356	360	Sand
360	395	Hard Clay
395	420	Hard Sand
420	427	Sand
427	465	Sandy Clay
465	500	Blue Clay
500	516	Blue Shale
516	530	Clay
530	544	Sediment
544	569	Hard Sandy Clay
569	633	Sediment
633	650	Shale & Clay
650	679	Sediment
679	709	Blue Clay
709	712	Sand
712	739	Blue Sediment
739	742	Sand
742	767	Hard Clay
767	770	Hard Slate
770	802	Shale
802	812	Blue Clay
812	816	Sand
816	822	Clay
822	850	Sediment
850	865	Sediment Clay
865	944	Sediment
944	948	Sand
948	958	Hard Clay
958	1004	Sediment
1004	1008	Sand
1008	1080	Blue Sediment
1080	1082	Sand
1082	1108	Sediment
1108	1271	Shale & Clay
1271	1301	Hard Slate
1301	1401	Shale

0 1/2 mi North of P...
1/2 mi West of SE corner of section 32
(G.S.S.)

WELL DRILLER'S STATEMENT: 4/2/55 5/5/55
This well was drilled under my jurisdiction and this report is true to the best of my knowledge and belief.

NAME Whitten Pump Co. (Typed or printed)
Address 1744 High St. Delano, California

[SIGNED] [Signature] Well Driller
License No. 148282 Dated 5/5/55

24/27-32K1

LOG No.
32108

PAGE 2 OF 2

Well Log Continued

1401	ft. to	1410	ft.	Hard Clay
1410	" "	1413		Sand
1413		1423		Clay
1423		1426		Sand
1426		1433		Clay
1433		1435		Hard Shale
1435		1475		Shale
1475		1493		Blue Shale
1493		1500		Clay
1500		1515		Shale
1515		1522		Clay
1522		1526		Shale
1526		1551		Very Hard Slate
1551		1590		Shale
1590		1628		Sandy Shale
1628		1750		Sand & Shale
1750		1765		Sandy Clay
1765		1780		Clay
1780		1800		Blue Shale

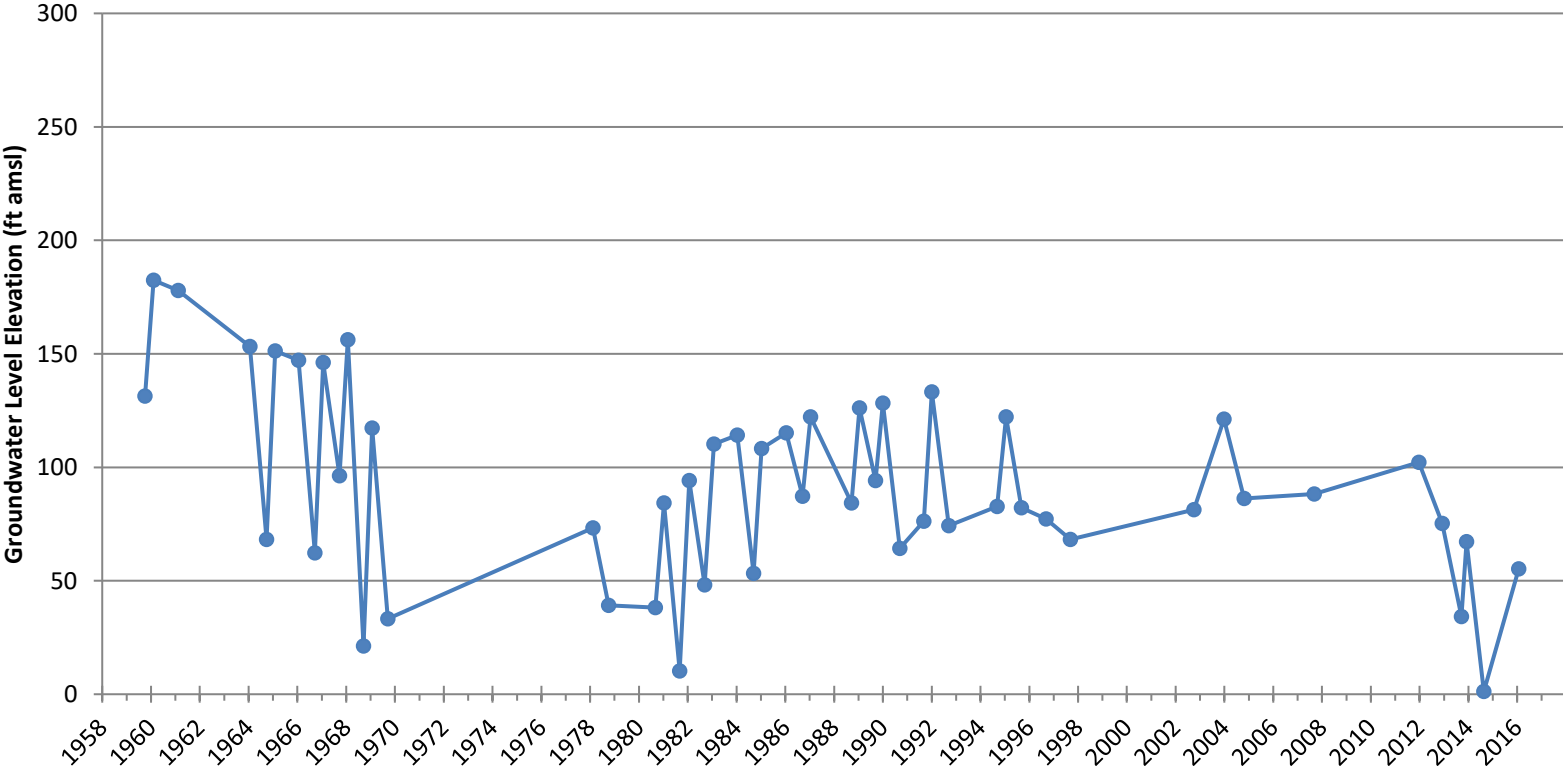
0.47 mile north, 0.47 mile west of

SECTION 32
Water Code
Section 70707 of Section 32

24/27-32K1 (USGS)

Groundwater Hydrographs - Deep

24S/27E-32K01



DUPLICATE
File Original, Duplicate and Triplicate with the
REGIONAL WATER POLLUTION
CONTROL BOARD No. 5
(Insert appropriate number)

24/24-3A1

WATER WELL DRILLERS REPORT

(Sections 7076, 7077, 7078, Water Code)

LOCATION NOT CHECKED

Do Not Fill In

No. **63263**

STATE OF CALIFORNIA

State Well No. 3A1
Other Well No. 295/296-3

(1) OWNER:

Name Jack C. Phillips Ranch
Address Star Route, Box 65
Earlimart, California

(2) LOCATION OF WELL:

County Tulare Owner's number, if any—
R. F. D. or Street No.
Southwest corner of intersection of
Ave. 48 and Rd. 92.

(3) TYPE OF WORK (check):

New well Deepening Reconditioning Abandon
If abandonment, describe material and procedure in Item 11.

(4) PROPOSED USE (check):

Domestic Industrial Municipal
Irrigation Test Well Other

(5) EQUIPMENT:

Rotary
Cable
Dug Well

(6) CASING INSTALLED:

SINGLE DOUBLE
From 600 ft. to 1002 ft. Diam. 1 1/4" Gage or Wall
16" Single Diameter of Bore 2 1/2" from Top to both to Bottom
14" Single
Type and size of shoe or well ring
Describe joint Butt Welded Size of gravel: 3/8

(7) PERFORATIONS:

Type of perforator used Machine
Size of perforations 1/8 in. length, by 1 cc in.
From 804 ft. to 1,602 ft. Perf. per row 18 Rows per ft.

(8) CONSTRUCTION:

Was a surface sanitary seal provided? Yes No To what depth ft.
Were any strata sealed against pollution? Yes No If yes, note depth of strata
From ft. to ft.
Method of Sealing

(9) WATER LEVELS:

Depth at which water was first found Unknown ft.
Standing level before perforating ft.
Rising level after perforating ft.

(10) WELL TESTS:

Was a pump test made? Yes No If yes, by whom?
Yield: gal./min. with ft. draw down after hrs.
Temperature of water Was a chemical analysis made? Yes No
Was electric log made of well? Yes No

(11) WELL LOG:

Total depth 1,602 ft. Depth of completed well 1,602 ft. 36

Formation: Describe by color, character, size of material, and structure.

0 ft. to	35 ft.	Sandy Clay
35 "	153 "	Sandy
153 "	188 "	Clay
188 "	235 "	Hard Sand
235 "	270 "	Clay
270 "	273 "	Sand
273 "	315 "	Sandy Clay
315 "	338 "	Hard Shale
338 "	430 "	Sandy Clay
430 "	436 "	Sand
436 "	458 "	Sandy Clay
458 "	582 "	Clay
582 "	643 "	Blue Clay
643 "	710 "	Sandy Clay
710 "	730 "	Sand
730 "	745 "	Sandy Clay
745 "	792 "	Shale
792 "	892 "	Clay
892 "	906 "	Sand
906 "	945 "	Sandy Clay
945 "	960 "	Blue Clay
960 "	963 "	Sand
963 "	1036 "	Hard Shale
1036 "	1070 "	Clay
1070 "	1096 "	Shale
1096 "	1125 "	Clay
1125 "	1140 "	Sand
1140 "	1170 "	Shale
1170 "	1200 "	Clay
1200 "	1247 "	Sandy Clay
1247 "	1257 "	Hard Shale
1257 "	1260 "	Sand
1260 "	1390 "	Shale
1390 "	1405 "	Sand
1405 "	1425 "	Sandy Clay
1425 "	1488 "	Shale
1488 "	1502 "	Clay
1502 "	1575 "	Shale
1575 "	1590 "	Sand
1590 "	1602 "	Hard Shale

Work started 6/7/60 19 Completed 6/24/60 19

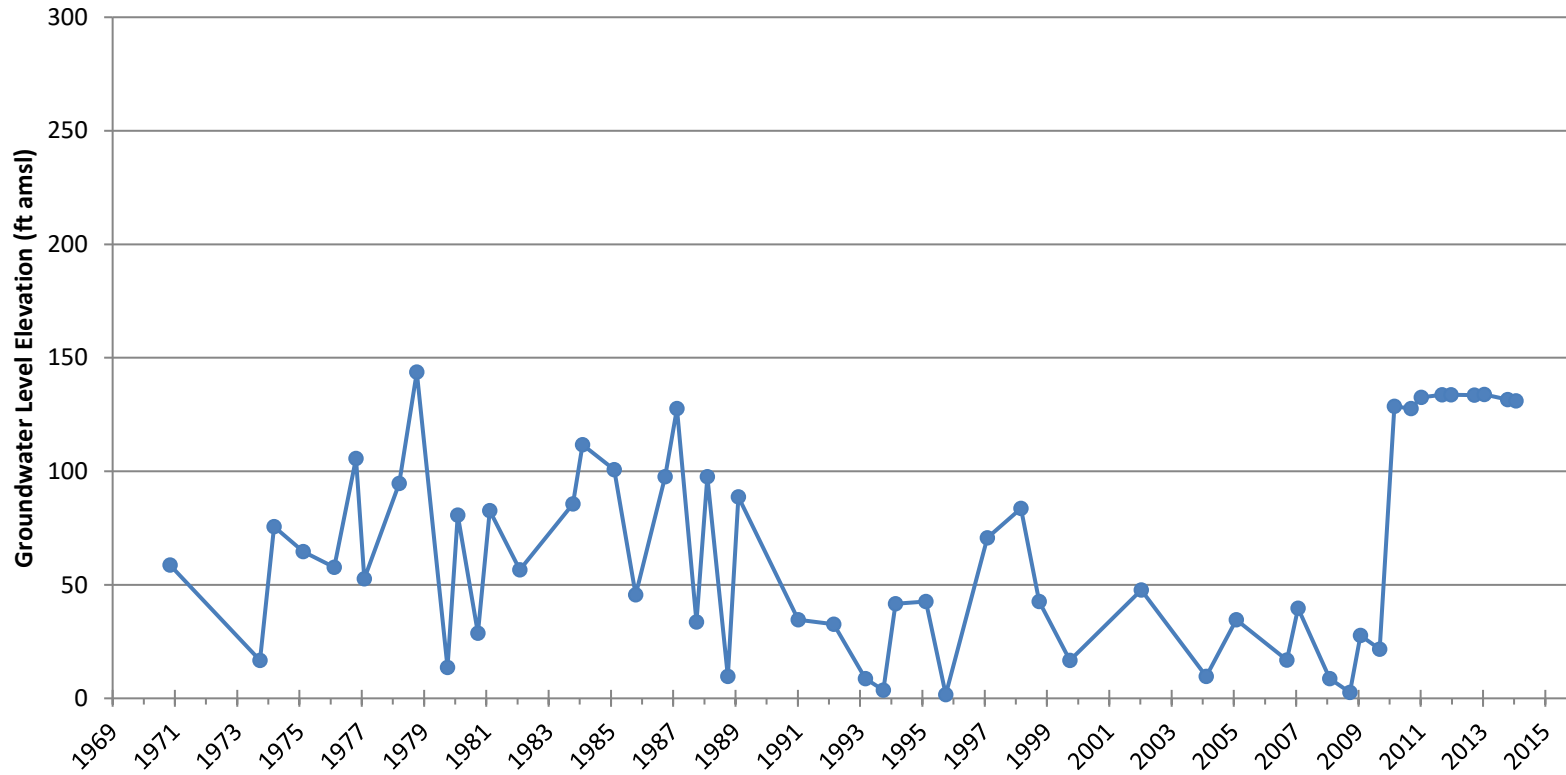
WELL DRILLER'S STATEMENT:

This well was drilled under my jurisdiction and this report is true to the best of my knowledge and belief.

NAME Whitten Pumps, Inc.
(Person, firm, or corporation) (Typed or printed)
Address 1744 High St.
Palano, Calif.
[SIGNED] Donald E. Whitten
148282 Well Driller
License No. Dated 11-1-60, 19 60

Groundwater Hydrographs - Deep

24S/24E-03A01



Owner's Well No. MW-6

Date Work Began 9/24/2010, Ended 9/24/2010

Local Permit Agency ENVIRO HEALTH, TULARE

Permit No. 10-0338 Permit Date 8/30/2010

STATE OF CALIFORNIA
WELL COMPLETION REPORT

Refer to Instruction Pamphlet

No. **EO117919**

DWR USE ONLY -- DO NOT FILL IN

STATE WELL NO./STATION NO.

LATITUDE LONGITUDE

APN/TRS/OTHER

GEOLOGIC LOG

ORIENTATION (✓) <input checked="" type="checkbox"/> VERTICAL <input type="checkbox"/> HORIZONTAL <input type="checkbox"/> ANGLE (SPECIFY)		DRILLING METHOD ROTARY FLUID WATER
DEPTH FROM SURFACE		DESCRIPTION <i>Describe material, grain, size, color, etc.</i>
Ft. to Ft.		
0 to 20	20	TOP SOIL, MEDIUMFINE/COARSE SANDS
20 to 40	40	MEDIUM/FINE/COARSE SANDS
40 to 80	80	EDIUM/FINE/COARSE SANDS WITH SOME CLAY
80 to 120	120	MEDIUM/FINE/COARSE SANDS WITH MORE CLAY
120 to 140	140	MEDIUM/FINE/COARSE SANDS, WITH SOME CLAY
140 to 160	160	MEDIUM/FINE/COARSE SANDS WITH SOME CLAY
160 to 200	200	MEDIUM/FINE/COARSE SANDS
200 to 300	300	MEDIUM/FINE/COARSE SANDS WITH SOME CLAY
300 to 340	340	MEDIUM/FINE/COARSE SANDS, SOME CLAY SOME D.G.
340 to 420	420	MEDIUM/FINE/COARSE SANDS WITH SOME CLAY
420 to 560	560	CLAY WITH SOME SANDS
560 to 620	620	CLAY WITH MORE SANDS MEDIUM/FINE
620 to 680	680	CLAY WITH SOME MEDIUM/FINE SANDS
680 to 720	720	MOSTLEY CLAY
720 to 740	740	CLAY WITH SOME MEDIUM/FINE SANDS
740 to 760	760	MEDIUM/FINE/COARSE SANDS WITH SOME CLAY AND SHALE
760 to 810	810	MEDIUM/FINE/COARSE SANDSWITH CLAY

TOTAL DEPTH OF BORING 810 (Feet)

TOTAL DEPTH OF COMPLETED WELL 805 (Feet)

WELL OWNER

Name **SURINDERPAL GILL**

Mailing Address **16964 AVENUE 32** CA **93215**

DELANO CITY STATE ZIP

WELL LOCATION

Address **1/2 MI N AVE. 26 & 1/2 MI E. ROAD 16**

City **DELANO CA 93215**

County **TULARE**

APN Book **3381** Page **003** Parcel **24**

Township **24** Range **26** Section **17**

Latitude

LOCATION SKETCH

NORTH

WEST EAST

ACTIVITY (✓)

NEW WELL

MODIFICATION/REPAIR

Deepen

Other (Specify)

DESTROY (Describe Procedures and Materials Under "GEOLOGIC LOG")

PLANNED USES (✓)

WATER SUPPLY

Domestic Public

Irrigation Industrial

MONITORING

TEST WELL

CATHODIC PROTECTION

HEAT EXCHANGE

DIRECT PUSH

INJECTION

VAPOR EXTRACTION

SPARGING

REMEDICATION

OTHER (SPECIFY)

Illustrate or Describe Distance of Well from Roads, Buildings, Fences, Rivers, etc. and attach a map. Use additional paper if necessary. PLEASE BE ACCURATE & COMPLETE.

WATER LEVEL & YIELD OF COMPLETED WELL

DEPTH TO FIRST WATER (Ft.) BELOW SURFACE

DEPTH OF STATIC

WATER LEVEL (Ft.) & DATE MEASURED

ESTIMATED YIELD * (GPM) & TEST TYPE **AIR LIFT**

TEST LENGTH **4** (Hrs.) TOTAL DRAWDOWN (Ft.)

May not be representative of a well's long-term yield.

DEPTH FROM SURFACE Ft. to Ft.	BORE-HOLE DIA. (Inches)	CASING (S)						DEPTH FROM SURFACE Ft. to Ft.	ANNULAR MATERIAL TYPE				
		TYPE (✓)	MATERIAL / GRADE	INTERNAL DIAMETER (Inches)	GAUGE OR WALL THICKNESS	SLOT SIZE IF ANY (Inches)	CE-MENT (✓)		BEN-TONITE (✓)	FILL (✓)	FILTER PACK (TYPE/SIZE)		
#1							0	130	✓				
0	200	16"	✓	PVC	4"	SCH 40	360	370		✓			
200	350	16"	✓	PVC	4"	SCH 40	464	474		✓			
#2							590	600		✓			
0	705	12 1/4"	✓	PVC	4"	SCH 40	630	640		✓			
705	805	12 1/4"	✓	PVC	4"	SCH 40	660	670		✓			

ATTACHMENTS (✓)

- Geologic Log
- Well Construction Diagram
- Geophysical Log(s)
- Soil/Water Chemical Analysis
- Other

ATTACH ADDITIONAL INFORMATION, IF IT EXISTS.

CERTIFICATION STATEMENT

I, the undersigned, certify that this report is complete and accurate to the best of my knowledge and belief.

NAME **BRADLEY & SONS**
(PERSON, FIRM, OR CORPORATION) (TYPED OR PRINTED)

ADDRESS **3625 S. HIGHLAND**

Signed

Donna Bodice

WELL DRILLER/AUTHORIZED REPRESENTATIVE

CITY **DEL REY**

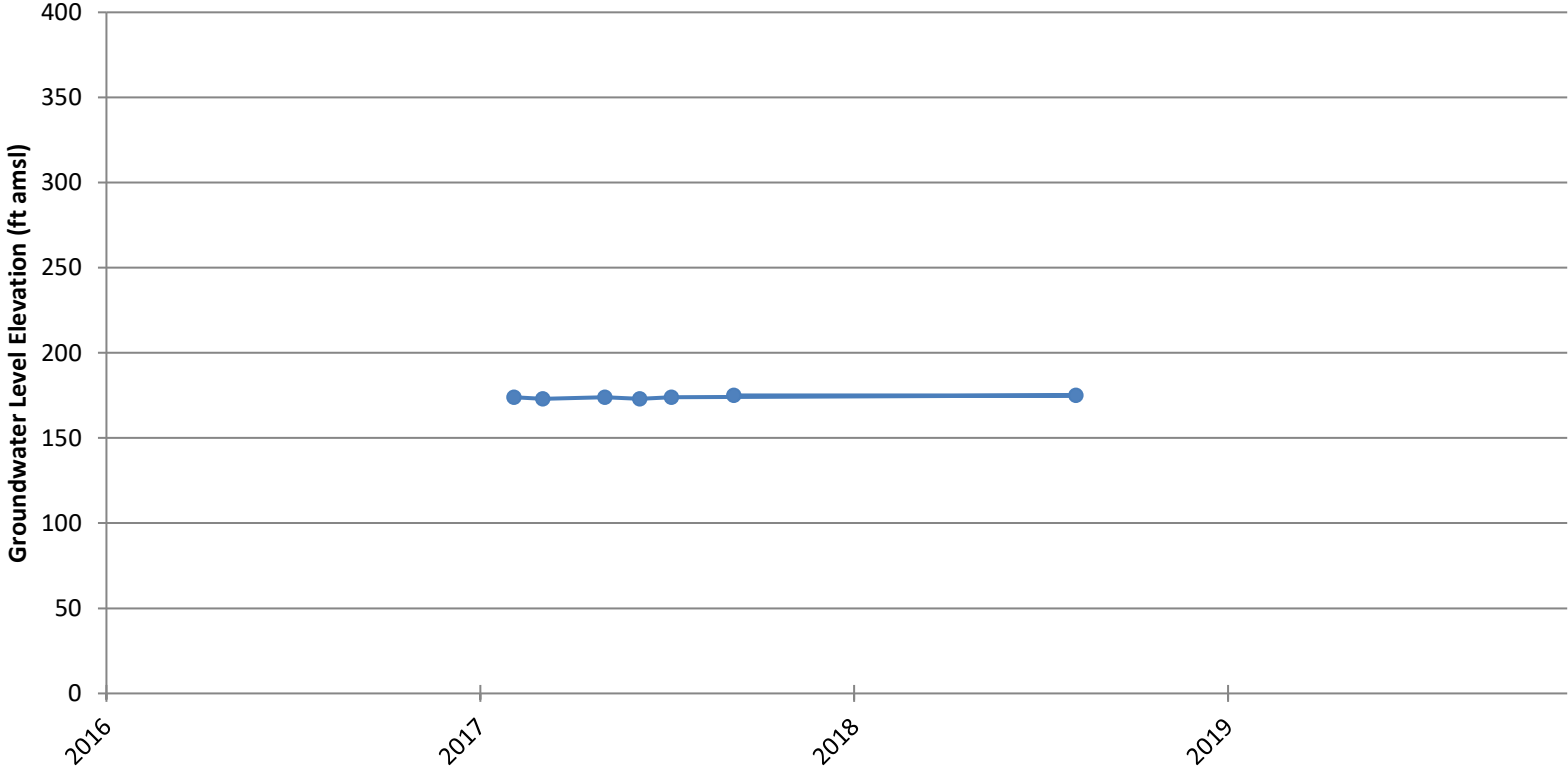
DATE SIGNED **10/06/10**

STATE **CA** ZIP **93616**

C-57 LICENSE NUMBER **414178**

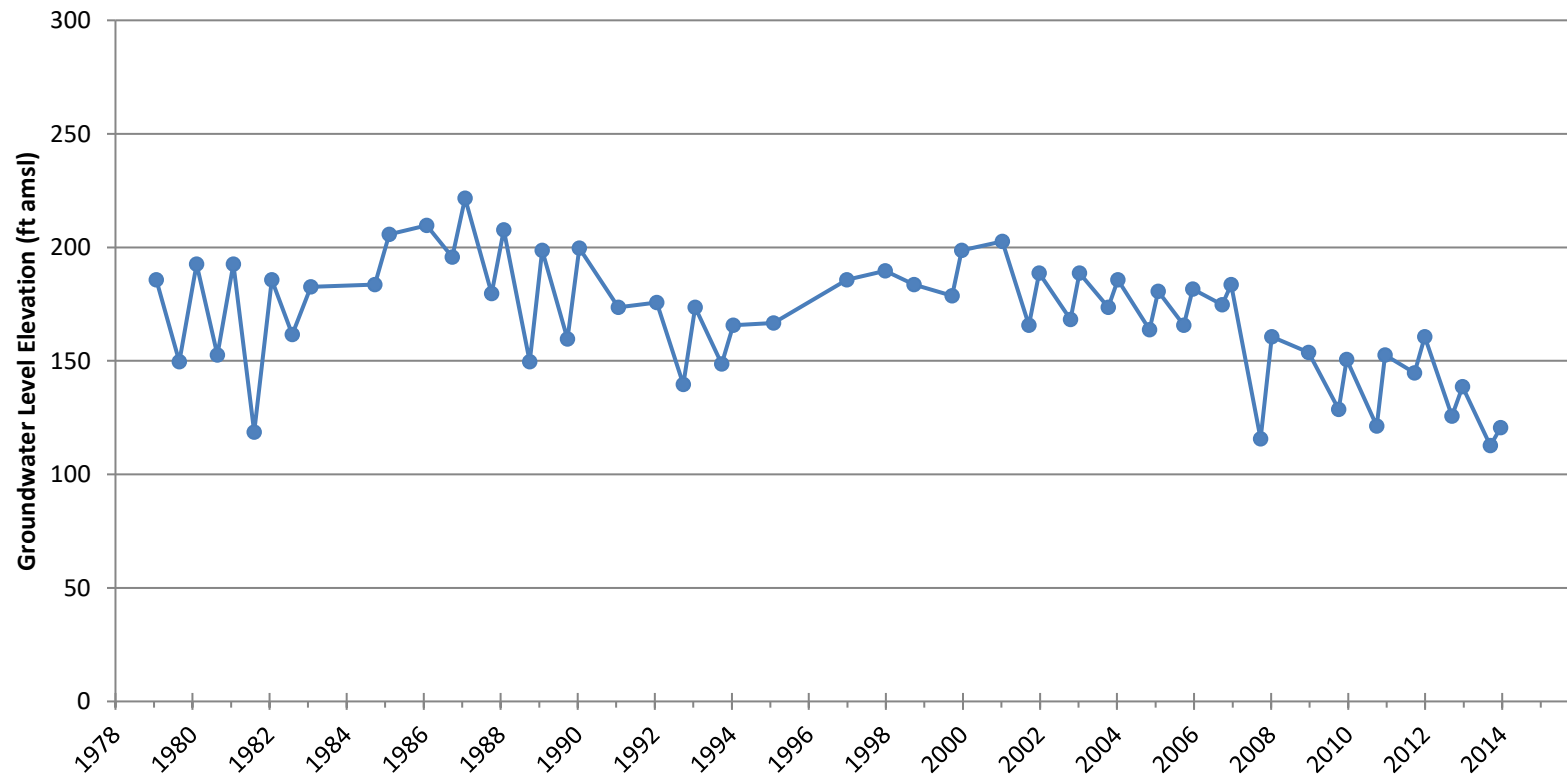
Groundwater Hydrographs - Deep

M-19



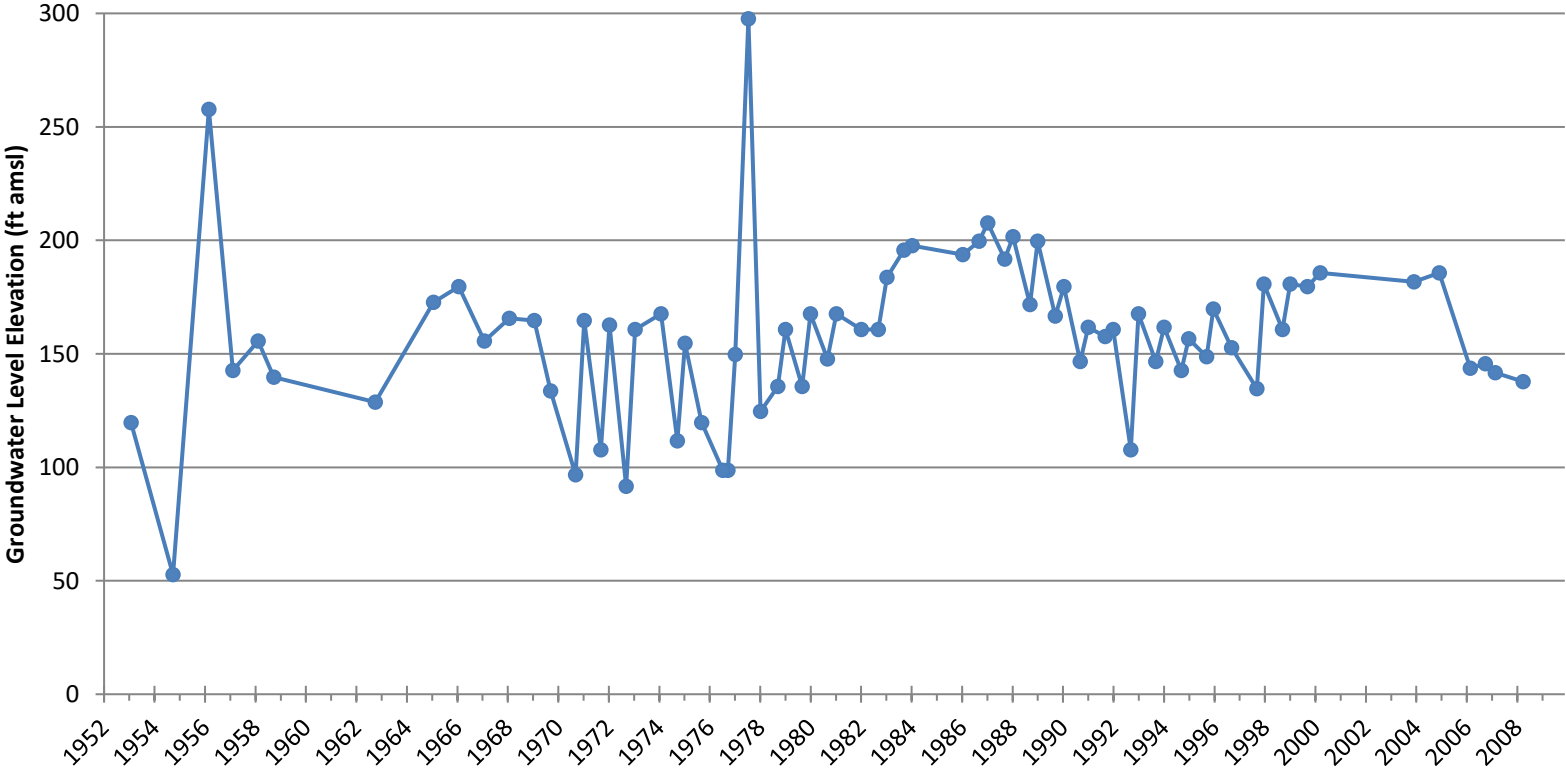
Groundwater Hydrographs - Deep

24S/25E-13F01



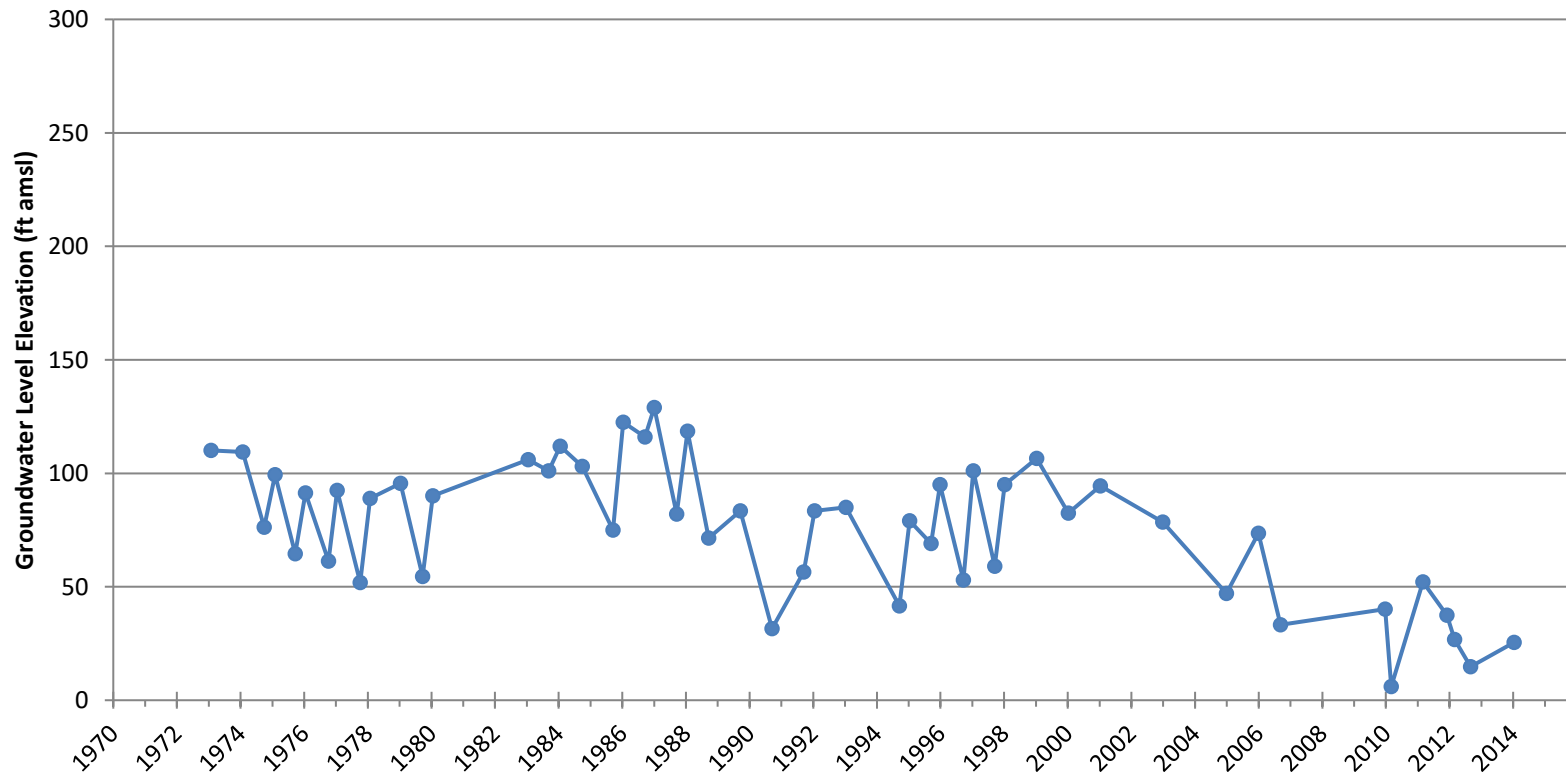
Groundwater Hydrographs - Deep

24S/25E-36J01



Groundwater Hydrographs - Deep

23S/23E-02A01



STATE OF CALIFORNIA WELL COMPLETION REPORT

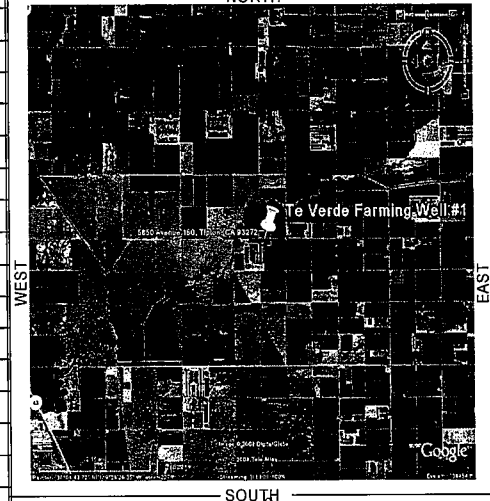
Refer to Instruction Pamphlet

DWR USE ONLY	DC NOT FILL IN
21S/23E25 STATE WELL NO./STATION NO.	1/B LATITUDE LONGITUDE
APN/TRS/OTHER	

Page 1 of 2
 Owner's Well No. _____ Well #1 _____ No. e0078297
 Date Work Began 8/16/08 Ended 10/07/08
 Local Permit Agency Tulare County Environmental Health Division
 Permit No. 08-0339 Permit Date 7/9/08

ORIENTATION (X)		X VERTICAL _____ HORIZONTAL _____ ANGLE _____ (SPECIFY)	
DEPTH FROM SURFACE		DRILLING METHOD	DESCRIPTION
FL to Ft.		Describe material, grain size, color, etc.	
50	80	Reverse Rotary	Brown clay, gravel
80	90		Brown clay
90	230		Brown clay, gravel
230	260		Gray clay, gravel
260	280		Gray clay
280	310		Gray clay, sand
310	320		Gray clay, gravel
320	360		Gray clay, sand
360	370		Gray clay
370	380		Gray clay, sand
380	410		Gray clay, gravel
410	420		Clay and cobbles, gravel
420	470		Clay and gravel
470	490		Gray clay
500	510		Gray clay, sandy
510	530		Gray clay
530	540		Gray clay, sandy
540	550		Gray clay
550	570		Clay and gravel
570	580		Coarse sand
580	590		Clay, gravel, and sand
590	610		Clay and little gravel
610	620		Clay and gravel
620	630		Gray clay and gravel
630	640		Gray clay
640	720		Gray clay and gravel
720	730		Gravel
730	740		Clay
740	760		Gray clay and gravel
760	790		Gray clay
TOTAL DEPTH OF BORING <u>1280</u> (Feet)			
TOTAL DEPTH OF COMPLETED WELL <u>1270</u> (Feet)			

WELL OWNER
 Name Te Velde Farming
 Mailing Address 5850 Ave 160
Tipton CA 93272
 CITY STATE ZIP
 Address 5850 Ave 160
Tipton CA 93272
 City STATE ZIP
Tulare County
 County
 APN Book 200 Page 190 Parcel 004
 Township 21S Range 23E Section 25
 Latitude 36 4 46.53 NORTH Longitude 119 26 11.47 WEST
 DEG. MIN. SEC. DEG. MIN. SEC.
 LOCATION SKETCH



ACTIVITY (X)
 NEW WELL
 MODIFICATION/REPAIR
 — Deepen
 — Other (Specify) _____
 — DESTROY (Describe Procedures and Materials Under "GEOLOGIC LOG")
 PLANNED USES (X)
 WATER SUPPLY
 Domestic _____ Public
 Irrigation _____ Industrial
 MONITORING _____
 TEST WELL _____
 CATHODIC PROTECTION _____
 HEAT EXCHANGE _____
 DIRECT PUSH _____
 INJECTION _____
 VAPOR EXTRACTION _____
 SPARGING _____
 REMEDIATION - OTHER (SPECIFY) _____

WATER LEVEL & YIELD OF COMPLETED WELL
 DEPTH TO FIRST WATER N/A (Ft.) BELOW SURFACE
 DEPTH OF STATIC WATER LEVEL 259.6 (Ft.) & DATE MEASURED 10/04/08-10/07/08
 ESTIMATED YIELD 2008 (GPM) & TEST TYPE Constant
 TEST LENGTH 37 (Hrs.) TOTAL DRAWDOWN 216.88 (Ft.)
 * May not be representative of a well's long-term yield.

DEPTH FROM SURFACE	BORE-HOLE DIA. (inches)	CASING (S)								
		TYPE (-)				MATERIAL / GRADE	OUTSIDE DIAMETER (inches)	GAUGE OR WALL THICKNESS	SLOT SIZE IF ANY (inches)	
Ft.	to	Ft.	BLANK	SCREEN	CON. DUCTOR					FILL PIPE
0	40	40			X		Steel	32	.375	
0	640	28	X				Steel	18	.375	
640	660	28		X			Steel	16	.312	.060 Standard Louver
660	1260	26		X			Steel	16	.312	.060 Standard Louver
1260	1270	26	X				Steel	18	.375	

DEPTH FROM SURFACE	ANNULAR MATERIAL					
	TYPE					
Ft.	to	Ft.	CE-MENT	BEN-TONITE	FILL	FILTER PACK (TYPE/SIZE)
0	20		X	X	X	
20	1260				X	1/4 x 10 Gravel Pack

ATTACHMENTS (X)
 Geologic Log
 Well Construction Diagram
 Geophysical Log(s)
 Soil/Water Chemical Analyses
 Other _____
 ATTACH ADDITIONAL INFORMATION, IF IT EXISTS.

CERTIFICATION STATEMENT
 I, the undersigned, certify that this report is complete and accurate to the best of my knowledge and belief.
Layne Christensen Company
 NAME (PERSON, FIRM OR CORPORATION) (TYPED OR PRINTED)
11001 Etiwanda Ave
 ADDRESS
Fontana CA 92337
 CITY STATE ZIP
 Signed [Signature] DATE SIGNED 10/10/08 STATE CA ZIP 91011
 WELL DRILLER AUTHORIZED REPRESENTATIVE DATE SIGNED C-57 LICENSE NUMBER

ORIGINAL
File with DWR

225/23E/16

STATE OF CALIFORNIA
WELL COMPLETION REPORT
Refer to Instruction Pamphlets

DWR USE ONLY - DO NOT FILL IN			
STATE WELL NO./STATION NO.			
LATITUDE		LONGITUDE	
APN/TRS/OTHER			

Page 1 of 1

Owner's Well No. 6535

No. 545936

Date Work Began 09/26/94, Ended 10/04/94

Local Permit Agency TULARE CO ENVIRONMENTAL HEALTH

Permit No. 30036 Permit Date 08/24/94

GEOLOGIC LOG

DEPTH FROM SURFACE		DESCRIPTION
Ft.	to Ft.	
0	3	TOP SOIL
3	15	SANDY YELLOW CLAY
15	110	SAND WITH BROWN CLAY STREAKS
110	250	SANDY BLUE CLAY W/SAND STRKS
250	300	SAND W/BLUE CLAY STREAKS
300	325	SANDY BLUE CLAY
325	400	SAND WITH BLUE CLAY STREAKS
400	420	BLUE CLAY
420	435	SANDY BLUE CLAY
435	555	CORCORAN CLAY
555	700	SAND WITH BLUE CLAY STREAKS
700	860	INTERBEDDED SAND & BLUE CLAY
860	885	SANDY BLUE CLAY
885	930	SAND WITH BLUE CLAY STREAKS
930	970	INTERBEDDED SAND & BLUE CLAY
970	1010	SAND WITH BLUE CLAY STREAKS
1010	1090	INTERBEDDED SAND & BLUE CLAY
1090	1210	SILTY BLUE SAND
1210	1300	INTERBEDDED SAND

WELL OWNER

Name CORCPORK COMPANY

Mailing Address 3922 AVENUE 120

CORCORAN CA 93212

CITY STATE ZIP

WELL LOCATION

Address HWY 43 AVE 120

City _____

County TULARE

APN Book 291 Page 060 Parcel 19001

Township 22 S Range 23 E Section 16

Latitude _____ NORTH Longitude _____ WEST

LOCATION SKETCH

ACTIVITY ()

NEW WELL

MODIFICATION/REPAIR

___ Deepen

___ Other (Specify)

___ DESTROY (Describe Procedures and Materials Under "GEOLOGIC LOG")

PLANNED USE(S) ()

___ MONITORING

WATER SUPPLY

___ Domestic

___ Public

Irrigation

___ Industrial

___ "TEST WELL"

___ CATHODIC PROTECTION

___ OTHER (Specify)

CONFINED

DRILLING METHOD ROTARY FLUID MUD

WATER LEVEL & YIELD OF COMPLETED WELL

DEPTH OF STATIC WATER LEVEL _____ (Ft.) & DATE MEASURED _____

ESTIMATED YIELD* _____ (GPM) & TEST TYPE _____

TEST LENGTH _____ (Hrs.) TOTAL DRAWDOWN _____ (Ft.)

* May not be representative of a well's long-term yield.

TOTAL DEPTH OF BORING 1270 (Feet)

TOTAL DEPTH OF COMPLETED WELL 1210 (Feet)

DEPTH FROM SURFACE	BORE-HOLE DIA. (Inches)	CASING(S)								
		TYPE ()				MATERIAL / GRADE	INTERNAL DIAMETER (Inches)	GAUGE OR WALL THICKNESS	SLOT SIZE IF ANY (Inches)	
		BLANK	SCREEN	CON. DUCTOR	FILL PIPE					
0	540	28"					ACCESS TUBE	2"	SCH 40	
0	560	28"	X				ASTM-135	16"	.312	
560	690	28"	X				DBL WILLSLOT	16"	.312	0.060
690	710	26"	X				ASTM-135	12-3/4	.312	
710	720	26"	X				DBL WILLSLOT	12-3/4	.312	0.050
720	730	26"	X				ASTM-135	12-3/4	.312	

DEPTH FROM SURFACE	ANNULAR MATERIAL				
	TYPE				
	CE-MENT ()	BEN-TONITE ()	FILL ()	FILTER PACK (TYPE/SIZE)	
0	50	X			SAND SLURRY
50	540			X	GRAVEL
540	1270			X	SAND PACK

ATTACHMENTS ()

___ Geologic Log

___ Well Construction Diagram

___ Geophysical Log(s)

___ Soil/Water Chemical Analyses

___ Other _____

ATTACH ADDITIONAL INFORMATION, IF IT EXISTS.

CERTIFICATION STATEMENT

I, the undersigned, certify that this report is complete and accurate to the best of my knowledge and belief.

NAME EATON DRILLING COMPANY, INC.

(PERSON, FIRM, OR CORPORATION) (TYPED OR PRINTED)

20 W. Kentucky Ave. Woodland CA 95695

ADDRESS CITY STATE ZIP

Signed [Signature] 10/13/94 132782657

WELL DRILLER/AUTHORIZED REPRESENTATIVE DATE SIGNED C-97 LICENSE NUMBER

ORIGINAL
File with DWR

Page 1 of 1

Owner's Well No. 6535P2

Date Work Began 09/26/94, Ended 10/04/94

Local Permit Agency TULARE CO ENVIRONMENTAL HEALTH

Permit No. 30036, Permit Date 08/24/94

STATE OF CALIFORNIA

WELL COMPLETION REPORT

Refer to Instruction Pamphlet

DWR USE ONLY - DO NOT FILL IN
STATE WELL NO./STATION NO.
LATITUDE
LONGITUDE
APN/TRS/OTHER

ORIENTATION () X VERTICAL _____ HORIZONTAL _____ ANGLE _____ (SPECIFY)
DEPTH TO FIRST WATER _____ (Ft.) BELOW SURFACE
DESCRIPTION Describe material, grain size, color, etc.
Name CORCPORK COMPANY
Mailing Address 3922 AVENUE 120
CORCORAN CA 93212
Address SAME AS PAGE ONE
City TULARE
County TULARE
APN Book 291 Page 060 Parcel 19001
Township 22 S Range 23 E Section 16
Latitude _____ NORTH Longitude _____ WEST
LOCATION SKETCH NORTH SOUTH
ACTIVITY () X NEW WELL
MODIFICATION/REPAIR
_____ Deepen
_____ Other (Specify)
DESTROY (Describe Procedures and Materials Under "GEOLOGIC LOG")
PLANNED USE(S)
()
_____ MONITORING
WATER SUPPLY
_____ Domestic
_____ Public
X _____ Irrigation
_____ Industrial
_____ "TEST WELL"
_____ CATHODIC PROTECTION
_____ OTHER (Specify)
DRILLING METHOD ROTARY FLUID MUD
WATER LEVEL & YIELD OF COMPLETED WELL
DEPTH OF STATIC WATER LEVEL _____ (Ft.) & DATE MEASURED
ESTIMATED YIELD* _____ (GPM) & TEST TYPE
TEST LENGTH _____ (Hrs.) TOTAL DRAWDOWN _____ (Ft.)
* May not be representative of a well's long-term yield.

CONCEALED
WATER CORP

DEPTH FROM SURFACE		BORE-HOLE DIA. (Inches)	CASING(S)					DEPTH FROM SURFACE		ANNULAR MATERIAL				
Ft.	to Ft.		TYPE ()				MATERIAL / GRADE	INTERNAL DIAMETER (Inches)	GAUGE OR WALL THICKNESS	SLOT SIZE IF ANY (Inches)	TYPE			
		BLANK	SCREEN	CON. DUCTOR	FILL PIPE	CE-MENT ()					BEN-TONITE ()	FILL ()	FILTER PACK (TYPE / SIZE)	
730	760	26"	X				DBL MILLSLOT	12-3/4	.312	0.050				
760	810	26"	X				ASTM-135	12-3/4	.312					
810	860	26"	X				DBL MILLSLOT	12-3/4	.312	0.050				
860	900	26"	X				ASTM-135	12-3/4	.312					
900	930	26"	X				DBL MILLSLOT	12-3/4	.312	0.050				
930	970	26"	X				ASTM-135	12-3/4	.312					

ATTACHMENTS ()
— Geologic Log
— Well Construction Diagram
— Geophysical Log(s)
— Soil/Water Chemical Analyses
— Other
ATTACH ADDITIONAL INFORMATION, IF IT EXISTS.

CERTIFICATION STATEMENT
I, the undersigned, certify that this report is complete and accurate to the best of my knowledge and belief.
NAME EATON DRILLING COMPANY, INC.
(PERSON, FIRM, OR CORPORATION) (TYPED OR PRINTED)
20 W. Kentucky Ave. Woodland CA 95695
ADDRESS CITY STATE ZIP
Signed [Signature] DATE SIGNED 10/13/94 133783C57
WELL DRILLER/AUTHORIZED REPRESENTATIVE DATE SIGNED C-57 LICENSE NUMBER

ORIGINAL
File with DWR

Page 1 of 1

Owner's Well No. 6535P3

No. 545938

Date Work Began 09/26/94, Ended 10/04/94

Local Permit Agency TULARE CO ENVIRONMENTAL HEALTH

Permit No. 30036 Permit Date 08/24/94

STATE OF CALIFORNIA
WELL COMPLETION REPORT
Refer to Instruction Pamphlet

DWR USE ONLY - DO NOT FILL IN

STATE WELL NO./STATION NO.

LATITUDE LONGITUDE

APN/TRS/OTHER

GEOLOGIC LOG

WELL OWNER

ORIENTATION (∠) VERTICAL _____ HORIZONTAL _____ ANGLE _____ (SPECIFY)

Name CORCPORK COMPANY

DEPTH TO FIRST WATER _____ (Ft.) BELOW SURFACE

Mailing Address 3922 AVENUE 120

DEPTH FROM SURFACE	
Ft.	to Ft.

DESCRIPTION

Describe material, grain size, color, etc.

CORCORAN

CA 93212
STATE ZIP

WELL LOCATION

Address SAME AS PAGE ONE

City _____

County TULARE

APN Book 291 Page 060 Parcel 19001

Township 22 S Range 23 E Section 16

Latitude _____ NORTH Longitude _____ WEST
DEG. MIN. SEC. DEG. MIN. SEC.

LOCATION SKETCH

ACTIVITY (∠)

NEW WELL

MODIFICATION/REPAIR

- ___ Deepen
- ___ Other (Specify)

DESTROY (Describe Procedures and Materials Under "GEOLOGIC LOG")

PLANNED USE(S) (∠)

___ MONITORING

WATER SUPPLY

- ___ Domestic
- ___ Public
- Irrigation
- ___ Industrial
- ___ "TEST WELL"

CATHODIC PROTECTION
___ OTHER (Specify)

WEST EAST
NORTH SOUTH
Illustrate or Describe Distance of Well from Landmarks such as Roads, Buildings, Fences, Rivers, etc. PLEASE BE ACCURATE & COMPLETE.

DRILLING METHOD ROTARY

FLUID MUD

WATER LEVEL & YIELD OF COMPLETED WELL

DEPTH OF STATIC WATER LEVEL _____ (Ft.) & DATE MEASURED _____

ESTIMATED YIELD* _____ (GPM) & TEST TYPE _____

TEST LENGTH _____ (Hrs.) TOTAL DRAWDOWN _____ (Ft.)

* May not be representative of a well's long-term yield.

TOTAL DEPTH OF BORING 1270 (Feet)
TOTAL DEPTH OF COMPLETED WELL 1210 (Feet)

DEPTH FROM SURFACE Ft. to Ft.	BORE-HOLE DIA. (Inches)	CASING(S)						DEPTH FROM SURFACE Ft. to Ft.	ANNULAR MATERIAL				
		TYPE (∠)				MATERIAL / GRADE	INTERNAL DIAMETER (Inches)		GAUGE OR WALL THICKNESS	SLOT SIZE IF ANY (Inches)	TYPE		
		BLANK	SCREEN	CON- DUCTOR	FILL PIPE								
970	1000	26"	X			DBL MILLSLOT	12-3/4	.312	0.050				
1000	1020	26"				COMPRESSON		SECTION					
1020	1050	26"	X			DBL MILLSLOT	12-3/4	.312	0.050				
1050	1060	26"	X			ASTM-135	12-3/4	.312					
1060	1080	26"	X			DBL MILLSLOT	12-3/4	.312	0.050				
1080	1090	26"	X			ASTM-135	12-3/4	.312					

ATTACHMENTS (∠)

- ___ Geologic Log
- ___ Well Construction Diagram
- ___ Geophysical Log(s)
- ___ Soil/Water Chemical Analyses
- ___ Other _____

ATTACH ADDITIONAL INFORMATION, IF IT EXISTS.

CERTIFICATION STATEMENT

I, the undersigned, certify that this report is complete and accurate to the best of my knowledge and belief.

NAME EATON DRILLING COMPANY, INC.
(PERSON, FIRM, OR CORPORATION) (TYPED OR PRINTED)

ADDRESS 20 W. Kentucky Ave. City Woodland STATE CA ZIP 95605

Signed [Signature]
WELL DRILLER/AUTHORIZED REPRESENTATIVE

DATE SIGNED 10/13/94 LICENSE NUMBER 122782657

ORIGINAL
File with DWR

STATE OF CALIFORNIA
WELL COMPLETION REPORT

Page 1 of 1

Refer to Instruction Pamphlet

Owner's Well No. 6535P4

No. 545939

Date Work Began _____, Ended _____

Local Permit Agency TULARE CO ENVIRONMENTAL HEALTH

Permit No. 30036

Permit Date 08/24/94

DWR USE ONLY - DO NOT FILL IN

STATE WELL NO./STATION NO.	
LATITUDE	LONGITUDE
APN/TRS/OTHER	

GEOLOGIC LOG

WELL OWNER

ORIENTATION (∠) VERTICAL _____ HORIZONTAL _____ ANGLE _____ (SPECIFY)

Name CORCPORK COMPANY

DEPTH TO FIRST WATER _____ (Ft.) BELOW SURFACE

Mailing Address 3922 AVENUE 120

DEPTH FROM SURFACE	
Ft.	to Ft.

DESCRIPTION

Describe material, grain size, color, etc.

CITY CORCORAN

STATE CA ZIP 93212

WELL LOCATION

Address SAME AS PAGE ONE

City _____

County TULARE

APN Book 291 Page 060 Parcel 19001

Township 22 S Range 23 E Section 16

Latitude _____ NORTH Longitude _____ WEST

LOCATION SKETCH

ACTIVITY (∠)

NEW WELL

MODIFICATION/REPAIR

_____ Deepen

_____ Other (Specify)

DESTROY (Describe Procedures and Materials Under "GEOLOGIC LOG")

PLANNED USE(S)

(∠) _____

_____ MONITORING

WATER SUPPLY

_____ Domestic

_____ Public

Irrigation

_____ Industrial

_____ "TEST WELL"

_____ CATHODIC PROTECTION

_____ OTHER (Specify)

WEST EAST SOUTH NORTH

Illustrate or Describe Distance of Well from Landmarks such as Roads, Buildings, Fences, Rivers, etc. PLEASE BE ACCURATE & COMPLETE.

DRILLING METHOD ROTARY

FLUID MUD

WATER LEVEL & YIELD OF COMPLETED WELL

DEPTH OF STATIC WATER LEVEL _____ (Ft.) & DATE MEASURED _____

ESTIMATED YIELD* _____ (GPM) & TEST TYPE _____

TEST LENGTH _____ (Hrs.) TOTAL DRAWDOWN _____ (Ft.)

* May not be representative of a well's long-term yield.

TOTAL DEPTH OF BORING 1270 (Feet)

TOTAL DEPTH OF COMPLETED WELL 1210 (Feet)

DEPTH FROM SURFACE Ft. to Ft.	BORE-HOLE DIA. (Inches)	CASING(S)						ANNULAR MATERIAL					
		TYPE (∠)				MATERIAL/ GRADE	INTERNAL DIAMETER (Inches)	GAUGE OR WALL THICKNESS	SLOT SIZE IF ANY (Inches)	TYPE			
		BLANK	SCREEN	CON- DUCTOR	FILL PIPE								
1090	1140	26"	X			DBL WILLSLOT	12-3/4	.312	0.050				
1140	1150	26"	X			ASTM-135	12-3/4	.312					
1150	1210	26"	X			DBL WILLSLOT	12-3/4	.312	0.050				

ATTACHMENTS (∠)

- _____ Geologic Log
- _____ Well Construction Diagram
- _____ Geophysical Log(s)
- _____ Soil/Water Chemical Analyses
- _____ Other _____

ATTACH ADDITIONAL INFORMATION, IF IT EXISTS.

CERTIFICATION/STATEMENT

I, the undersigned, certify that this report is complete and accurate to the best of my knowledge and belief.

NAME EATON DRILLING COMPANY, INC.

(PERSON, FIRM, OR CORPORATION) (TYPED OR PRINTED)

20 W. Kentucky Ave.

Woodland

CA 95695

ADDRESS

CITY

STATE

ZIP

Signed _____

WELL DRILLER/AUTHORIZED REPRESENTATIVE

10/13/94

DATE SIGNED

133783C57

C-57 LICENSE NUMBER

23/26-151

9-063
(December 1949)

UNITED STATES
DEPARTMENT OF THE INTERIOR
GEOLOGICAL SURVEY
WATER RESOURCES DIVISION

(Conflict in shaded sheet)

No. 23/26-151

OTHER Nos. Maze #1

WELL LOG

State California County Tulare Subarea DUCOR-Famoso

Owner Maze T.D. = 1913 E-10

Location 0.49 miles N of sec. line (E Ave 88) + 50 ft. W of Rd. 208
T.D. = 1830 complete

Drilled by Hilton Drilling Co. Address 17th + I st., Bakersfield

Date 12-6-56 Casing diam. _____ Land-surf. alt. 410

Source of data Examination of dry rotary samples - Partial log
(Enter type of well, perforations, yield, and drawdown at end of log)

CORRELATION	MATERIAL	THICKNESS (feet)	DEPTH (feet)
1030-1110	sand, medium to coarse	80	
1110-1230	sand, and clay, dark green	120	
1230-1270	sand, medium to coarse, some dark green clay	40	
1270-1290	sand, medium to coarse	20	
1290-1390	clay, sandy, dark greenish	100	
1390-1430	sand, fine to coarse	40	
1430-1450	clay, dark green	20	
1470-1490	sand, medium to coarse	20	
1490-1510	clay, dark green	20	
1510-1630	clay, sandy, dark green	120	
1630-1650	sand, clayey, to coarse	20	
1650-1690	clay, sandy, dark green	40	
1690-1700	sand, clayey, to coarse	10	
1700-1780	Gravel, 2-8mm with some dark green clay & sand	80	
1780-1820	Gravel 2-8mm + dark green clay	40	
1820-1840	Gravel 2-8mm with some dark green clay & sand	20	
1840-1900	Gravel 2-8mm + dark green clay	60	

RECORD BY George J. Hilton DATE 12-6-56

SHEET 1 OF 1

23/26-151

23/26-151

23/26-151 Maze (Camp, S.A.) #1 12-14-56
1830 ft pipe, perf 1390-1830, Schlumberger
gr ran. to 2100'
3 mi W Terrabella 1/2 mi S on 208.

- 0-20 Surf km
20-46 Sd & Gravel
46-84 Sdy brn clay
84-290 Sdy brn clay w/ streaks of sd.
290-314 Tough sdy brown clay
314-378 Sdy brn clay w/ streaks of sd
378-390 Hard sd
390-620 Sdy brn clay w/ streaks of sd
620-975 Sdy blue clay w/ streaks of sd.
975-1015 Hard sdy blue clay & shale.
1015-1127 Hard blue clay w/ streaks of shale
1127-1350 Hard sdy clay
1350-1830 Sdy blue clay w/ streaks of sd.

ORIGINAL

File with DWR

STATE OF CALIFORNIA THE RESOURCES AGENCY DEPARTMENT OF WATER RESOURCES WATER WELL DRILLERS REPORT

Do not fill in

No. 085678

22/27-16

Notice of Intent No.

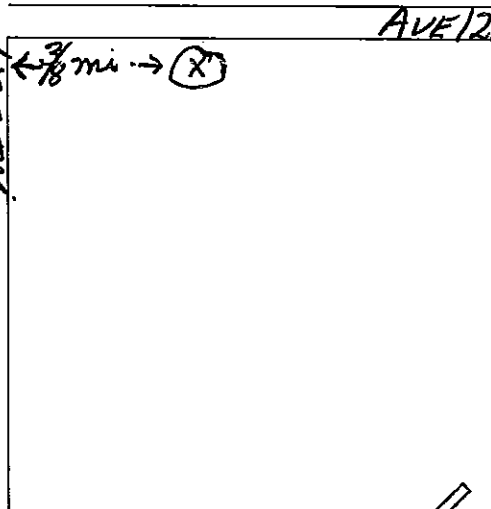
Local Permit No. or Date

State Well No. Other Well No.

(1) OWNER: Name Buttes Farmland Development Address P. O. Box 1206 City Delano, CA Zip 93215

(2) LOCATION OF WELL (See instructions): County Tulare Owner's Well Number Well address if different from above Township 22 Range 27 Section 16 Distance from cities, roads, railroads, fences, etc. 3/8 mile East of Road 224 on South side of Ave. 128.

(12) WELL LOG: Total depth 1240. Depth of completed well 1240. from ft. to ft. Formation (Describe by color, character, size or material) 0 - 90 Sand 90 - 94 Gravel 94 - 237 Gravel 237 - 277 Gravel 277 - 338 Clay w/Sand Streaks 338 - 399 Clay w/Gravel Streaks 399 - 522 Clay w/Sand Streaks 522 - 590 Blue Clay 590 - 700 Blue Clay 700 - 770 Clay 770 - 936 Sandy Clay 936 - 1088 Sand w/Clay Streaks 1088 - 1166 Sandy Clay 1166 - 1186 Coarse Sand & Clay 1186 - 1240 Sand w/Shade Streaks



(3) TYPE OF WORK: New Well [X] Deepening [] Reconstruction [] Reconditioning [] Horizontal Well [] Destruction [] (Describe destruction materials and procedures in Item 12) (4) PROPOSED USE: Domestic [] Irrigation [X] Industrial [] Test Well [] Stock [] Municipal [] Other []

(5) EQUIPMENT: Rotary [X] Reverse [] Cable [] Air [] Other [] Bucket [] (6) GRAVEL PACK: Yes [X] No [] Size 1/4" Diameter of bore 27-1/2" Packed from 0 to 1240 ft.

(7) CASING INSTALLED: Steel [X] Plastic [] Concrete [] (8) PERFORATIONS: Type of perforation or size of screen Table with columns: From ft., To ft., Dia. in., Casing or Wall, Slot size. Row 1: 0, 1240, 1 1/4", 1/4", 800', 1240', 125x2-1/2"

(9) WELL SEAL: Was surface sanitary seal provided? Yes [] No [X] If yes, to depth ___ ft. Were strata sealed against pollution? Yes [] No [X] Interval ___ ft. Method of sealing

(10) WATER LEVELS: Depth of first water, if known Unknown ft. Standing level after well completion ___ ft.

(11) WELL TESTS: Was well test made? Yes [X] No [] If yes, by whom? Type of test Pump [] Bailer [] Air lift [] Depth to water at start of test ___ ft. At end of test ___ ft. Discharge ___ gal/min after ___ hours Water temperature Chemical analysis made? Yes [] No [X] If yes, by whom? Was electric log made? Yes [X] No [] If yes, attach copy to this report

Work started 11-5-1979 Completed 11-30-1979

WELL DRILLER'S STATEMENT: This well was drilled under my jurisdiction and this report is true to the best of my knowledge and belief. SIGNED: [Signature] (Well Driller) NAME: Whitten Pumps, Inc. (Person, firm, or corporation) (Typed or printed) Address: Rt. 1 Box 1101 City: Delano, CA Zip: 93215 License No.: 148282 Date of this report: 3-24-80

Rd 224

Ave 128

3/8 mi -> (X)

WATER CODE SEC. 13752

OUTSIDE CORC. CLAY AREA

*The free Adobe Reader may be used to view and complete this form. However, software must be purchased to complete, save, and reuse a saved form.

File Original with DWR

Page 1 of 4

Owner's Well Number #2

Date Work Began 03/28/2009 Date Work Ended 5/20/2009

Local Permit Agency Tulare County Environmental Health Services

Permit Number 09-138 Permit Date 3/16/09

State of California

Well Completion Report

Refer to Instruction Pamphlet

No. **e0094537**

DWR Use Only - Do Not Fill In

025/26E-24

State Well Number/Site Number

Latitude N Longitude W

APN/TRS/Other

Geologic Log		
Orientation <input checked="" type="radio"/> Vertical <input type="radio"/> Horizontal <input type="radio"/> Angle Specify <u> </u>		
Drilling Method <u>Reverse Rotary</u> Drilling Fluid <u>Polybore</u>		
Depth from Surface		Description
Feet to Feet		Describe material, grain size, color, etc
40	110	Sand Gravel
110	150	Sand
150	190	Sand Gravel Clay
190	240	Sand Clay
240	290	Sand
290	360	Sand Clay
360	400	Clay
400	1,120	Sand Clay
1120	1,270	Clay
Total Depth of Boring <u>1270</u> Feet		
Total Depth of Completed Well <u>1240</u> Feet		

Well Owner

Name Gill & Sons Farm

Mailing Address 16964 Ave 32

City Delano State CA Zip 93292

Well Location

Address 1/4 Mile North of Ave 112 / 50' West of Rd. 208

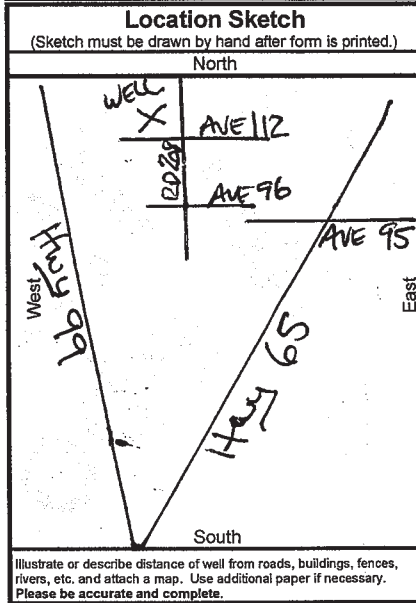
City Pixley County Tulare

Latitude N Longitude W

Datum Decimal Lat. Decimal Long.

APN Book 302 Page 280 Parcel 013

Township 22S Range 26E Section 24 S



Activity

New Well

Modification/Repair

Deepen

Other

Destroy

Describe procedures and materials under "GEOLOGIC LOG"

Planned Uses

Water Supply

Domestic Public

Irrigation Industrial

Cathodic Protection

Dewatering

Heat Exchange

Injection

Monitoring

Remediation

Sparging

Test Well

Vapor Extraction

Other

Water Level and Yield of Completed Well

Depth to first water 270 (Feet below surface)

Depth to Static

Water Level 270 (Feet) Date Measured 05/06/2009

Estimated Yield * 2,600 (GPM) Test Type Constant Rate

Test Length 12.0 (Hours) Total Drawdown 190 (Feet)

*May not be representative of a well's long term yield.

Casings							
Depth from Surface	Borehole Diameter	Type	Material	Wall Thickness	Outside Diameter	Screen Type	Slot Size if Any
Feet to Feet	(Inches)			(Inches)	(Inches)		(Inches)
0	40	42	Conductor	A53 Grade B	.375	30	
0	670	26	Blank	A53 Grade B	.312	16	
670	700	26	Ful Flo	Ful Flo A139	.312	16	Louver 0.080
700	800	26	Standard Flo	SF A139	.312	16	Louver
800	820	26	Ful Flo	Ful flo A139	.312	16	Louver 0.080
820	840	26	Standard Flo	SF A139	.312	16	Louver

Annular Material			
Depth from Surface	Fill	Description	
Feet to Feet			
0	40	Cement	Annular Seal
0	1,270	Filter Pack	4x16 SRI

Attachments

Geologic Log

Well Construction Diagram

Geophysical Log(s)

Soil/Water Chemical Analyses

Other

Attach additional information, if it exists.

Certification Statement

I, the undersigned, certify that this report is complete and accurate to the best of my knowledge and belief

Name Bakersfield Well & Pump Co.

7212 Fruitvale Ave Bakersfield CA 93308

Address City State Zip

Signed [Signature] 7/13/2009 440537

C-57 Licensed Water Well Contractor Date Signed C-57 License Number

*The free Adobe Reader may be used to view and complete this form. However, software must be purchased to complete, save, and reuse a saved form.

3/6

File Original with DWR

State of California

Well Completion Report

Refer to Instruction Pamphlet

No. e0094537

Page 3 of 4

Owner's Well Number #2

Date Work Began 03/28/2009 Date Work Ended 5/20/2009

Local Permit Agency Tulare County Environmental Health Services

Permit Number 09-138 Permit Date 3/16/09

DWR Use Only - Do Not Fill In	
<u>22S/26E-24</u>	
State Well Number/Site Number	
Latitude	Longitude
APN/TRS/Other	

Geologic Log		
Orientation <input checked="" type="radio"/> Vertical <input type="radio"/> Horizontal <input type="radio"/> Angle Specify _____		
Drilling Method <u>Reverse Rotary</u> Drilling Fluid <u>Polybore</u>		
Depth from Surface	Description	
Feet to Feet	Describe material, grain size, color, etc	
40	110	Sand Gravel
110	150	Sand
150	190	Sand Gravel Clay
190	240	Sand Clay
240	290	Sand
290	360	Sand Clay
360	400	Clay
400	1,120	Sand Clay
1120	1,270	Clay
Total Depth of Boring <u>1270</u> Feet		
Total Depth of Completed Well <u>1240</u> Feet		

Well Owner		
Name	<u>Gill & Sons Farm</u>	
Mailing Address	<u>16964 Ave 32</u>	
City	<u>Delano</u>	State <u>CA</u> Zip <u>93292</u>

Well Location		
Address <u>1/4 Mile North of Ave 112 / 50' West of Rd. 208</u>		
City	<u>Pixley</u>	County <u>Tulare</u>
Latitude	Longitude	
Deg. Min. Sec. N	Deg. Min. Sec. W	
Datum	Decimal Lat.	Decimal Long.
APN Book <u>302</u>	Page <u>280</u>	Parcel <u>013</u>
Township <u>22S</u>	Range <u>26E</u>	Section <u>24 S</u>

Location Sketch	
(Sketch must be drawn by hand after form is printed.)	
North	
West	East
South	
Illustrate or describe distance of well from roads, buildings, fences, rivers, etc. and attach a map. Use additional paper if necessary. Please be accurate and complete.	

Activity	
<input checked="" type="radio"/> New Well	
<input type="radio"/> Modification/Repair	
<input type="radio"/> Deepen	
<input type="radio"/> Other	
<input type="radio"/> Destroy	
Describe procedures and materials under "GEOLOGIC LOG"	
Planned Uses	
<input checked="" type="radio"/> Water Supply	
<input type="checkbox"/> Domestic	<input type="checkbox"/> Public
<input checked="" type="checkbox"/> Irrigation	<input type="checkbox"/> Industrial
<input type="radio"/> Cathodic Protection	
<input type="radio"/> Dewatering	
<input type="radio"/> Heat Exchange	
<input type="radio"/> Injection	
<input type="radio"/> Monitoring	
<input type="radio"/> Remediation	
<input type="radio"/> Sparging	
<input type="radio"/> Test Well	
<input type="radio"/> Vapor Extraction	
<input type="radio"/> Other	

Water Level and Yield of Completed Well			
Depth to first water	<u>270</u>	(Feet below surface)	
Depth to Static			
Water Level	<u>270</u>	(Feet)	Date Measured <u>05/06/2009</u>
Estimated Yield *	<u>2,600</u>	(GPM)	Test Type <u>Constant Rate</u>
Test Length	<u>12.0</u>	(Hours)	Total Drawdown <u>190</u> (Feet)
*May not be representative of a well's long term yield.			

Casings								
Depth from Surface	Borehole Diameter	Type	Material	Wall Thickness	Outside Diameter	Screen Type	Slot Size if Any	
Feet to Feet	(Inches)			(Inches)	(Inches)		(Inches)	
1,030	1,060	26	Ful Flo	Ful Flo A139	.312	16	Louwer	0.080
1,060	1,110	26	Standard Flo	SF A139	.312	16	Louwer	
1,110	1,130	26	Ful Flo	Ful Flo A139	.312	16	Louwer	0.080
1,130	1,145	26	Standard Flo	SF A139	.312	16	Louwer	
1,145	1,170	26	Ful Flo	Ful flo A139	.312	16	Louwer	0.080
1,170	1,200	26	Standard Flo	SF A139	.312	16	Louwer	

Annular Material			
Depth from Surface	Fill	Description	
Feet to Feet			
0	40	Cement	Annular Seal
0	1,270	Filter Pack	4x16 SRI

Attachments	
<input type="checkbox"/> Geologic Log	
<input type="checkbox"/> Well Construction Diagram	
<input type="checkbox"/> Geophysical Log(s)	
<input type="checkbox"/> Soil/Water Chemical Analyses	
<input type="checkbox"/> Other	
Attach additional information, if it exists.	

Certification Statement			
I, the undersigned, certify that this report is complete and accurate to the best of my knowledge and belief			
Name <u>Bakersfield Well & Pump Co.</u>			
Person, Firm or Corporation			
<u>7212 Fruitvale Ave.</u>	<u>Bakersfield</u>	<u>CA</u>	<u>93308</u>
Address	City	State	Zip
Signed <u>[Signature]</u>	<u>7/13/2009</u>	<u>440537</u>	
C-57 Licensed Water Well Contractor	Date Signed	C-57 License Number	

*The free Adobe Reader may be used to view and complete this form. However, software must be purchased to complete, save, and reuse a saved form.

File Original with DWR

State of California

Well Completion Report

Refer to Instruction Pamphlet

No. **e0094537**

Page 4 of 4

Owner's Well Number #2

Date Work Began 03/28/2009 Date Work Ended 5/20/2009

Local Permit Agency Tulare County Environmental Health Services

Permit Number 09-138 Permit Date 3/16/09

DWR Use Only - Do Not Fill In			
<u>22S/26E-24</u>			
State Well Number/Site Number			
Latitude		Longitude	
APN/TRS/Other			

Geologic Log	
Orientation	<input checked="" type="radio"/> Vertical <input type="radio"/> Horizontal <input type="radio"/> Angle Specify _____
Drilling Method	Reverse Rotary _____ Drilling Fluid Polybore _____

Depth from Surface Feet to Feet	Description Describe material, grain size, color, etc	
40	110	Sand Gravel
110	150	Sand
150	190	Sand Gravel Clay
190	240	Sand Clay
240	290	Sand
290	360	Sand Clay
360	400	Clay
400	1,120	Sand Clay
1120	1,270	Clay

Well Owner	
Name	<u>Gill & Sons Farm</u>
Mailing Address	<u>16964 Ave 32</u>
City	<u>Delano</u> State <u>CA</u> Zip <u>93292</u>

Well Location	
Address	<u>1/4 Mile North of Ave 112 / 50' West of Rd. 208</u>
City	<u>Pixlev</u> County <u>Tulare</u>
Latitude	_____ N Longitude _____ W
Datum	_____ Decimal Lat. _____ Decimal Long. _____
APN Book	<u>302</u> Page <u>280</u> Parcel <u>013</u>
Township	<u>22S</u> Range <u>26E</u> Section <u>24 S</u>

Location Sketch	
(Sketch must be drawn by hand after form is printed.)	
North	
South	
<small>Illustrate or describe distance of well from roads, buildings, fences, rivers, etc. and attach a map. Use additional paper if necessary. Please be accurate and complete.</small>	

Activity	
<input checked="" type="radio"/> New Well	
<input type="radio"/> Modification/Repair	
<input type="radio"/> Deepen	
<input type="radio"/> Other _____	
<input type="radio"/> Destroy	
<small>Describe procedures and materials under "GEOLOGIC LOG"</small>	
Planned Uses	
<input checked="" type="radio"/> Water Supply	
<input type="checkbox"/> Domestic <input type="checkbox"/> Public	
<input checked="" type="checkbox"/> Irrigation <input type="checkbox"/> Industrial	
<input type="radio"/> Cathodic Protection	
<input type="radio"/> Dewatering	
<input type="radio"/> Heat Exchange	
<input type="radio"/> Injection	
<input type="radio"/> Monitoring	
<input type="radio"/> Remediation	
<input type="radio"/> Sparging	
<input type="radio"/> Test Well	
<input type="radio"/> Vapor Extraction	
<input type="radio"/> Other _____	

Total Depth of Boring		<u>1270</u>	Feet
Total Depth of Completed Well		<u>1240</u>	Feet

Water Level and Yield of Completed Well

Depth to first water	<u>270</u>	(Feet below surface)
Depth to Static		
Water Level	<u>270</u>	(Feet) Date Measured <u>05/06/2009</u>
Estimated Yield *	<u>2.600</u>	(GPM) Test Type <u>Constant Rate</u>
Test Length	<u>12.0</u>	(Hours) Total Drawdown <u>190</u> (Feet)
*May not be representative of a well's long term yield.		

Casings								Annular Material			
Depth from Surface Feet to Feet	Borehole Diameter (Inches)	Type	Material	Wall Thickness (Inches)	Outside Diameter (Inches)	Screen Type	Slot Size if Any (Inches)	Depth from Surface Feet to Feet	Fill	Description	
1,200	1,220	26	Ful Flo	Ful Flo A139	.312	16	Louver	0	40	Cement Annular Seal	
1,220	1,240	26	Blank	A53 Grade B	.312	16		0	1,270	Filter Pack 4x16 SRI	

Attachments	
<input type="checkbox"/> Geologic Log	
<input type="checkbox"/> Well Construction Diagram	
<input type="checkbox"/> Geophysical Log(s)	
<input type="checkbox"/> Soil/Water Chemical Analyses	
<input type="checkbox"/> Other _____	
Attach additional information, if it exists.	

Certification Statement			
I, the undersigned, certify that this report is complete and accurate to the best of my knowledge and belief			
Name <u>Bakersfield Well & Pump Co.</u>			
Person, Firm or Corporation			
Address <u>7212 Fruitvale Ave</u>		City <u>Bakersfield</u> State <u>CA</u> Zip <u>93308</u>	
Signed _____		Date Signed <u>7/13/2009</u>	
C-57 Licensed Water Well Contractor		440537 C-57 License Number	

4/5

24/27-34

ORIGINAL
File Original, Duplicate and Triplicate with the
REGIONAL WATER POLLUTION
CONTROL BOARD No. _____
(Insert appropriate number)

WATER WELL DRILLERS REPORT
(Sections 7076, 7077, 7078, Water Code)

Do Not Fill In
No. 118749
State Well No. 24/27E-34
Other Well No. _____

THE RESOURCES AGENCY OF CALIFORNIA

(1) OWNER:

Name Buena Vista Orchards
Address P.O. Box 1458
McFarland, Calif. 93250

(2) LOCATION OF WELL:

County Kern Owner's number, if any—
R. F. D. or Street No. 1/4 mile East of Hwy 65 and 1/4
mile North of Ave. 2

(3) TYPE OF WORK (check):

New well Deepening Reconditioning Abandon
If abandonment, describe material and procedure in Item 11.

(4) PROPOSED USE (check):

Domestic Industrial Municipal
Irrigation Test Well Other

(5) EQUIPMENT:

Rotary
Cable
Dug Well

(6) CASING INSTALLED:

SINGLE DOUBLE
From 0 ft. to 1750 ft. 1 1/4" diam. 1/4" Gage or Wall
Diameter of Bore 2 1/2" from top to bottom
Type and size of shoe or well ring Size of gravel: 1/4"
Describe joint: collar w/ fillet weld

(7) PERFORATIONS:

Type of perforator used machine
Size of perforations .125 x 2 in., length, by 6 cc in.
From 600 ft. to 1750 ft. 2 Perf. per row 14 Rows per ft.

(8) CONSTRUCTION:

Was a surface sanitary seal provided? Yes No To what depth ft.
Were any strata sealed against pollution? Yes No If yes, note depth of strata
From ft. to ft.
Method of Sealing

(9) WATER LEVELS:

Depth at which water was first found unknown ft.
Standing level before perforating ft.
Standing level after perforating ft.

(10) WELL TESTS:

Was a pump test made? Yes No If yes, by whom?
Yield: gal./min. with ft. draw down after hrs.
Temperature of water Was a chemical analysis made? Yes No
Was electric log made of well? Yes No

(11) WELL LOG:

Total depth 1750 ft. Depth of completed well 1750 ft.
Formation: Describe by color, character, size of material, and structure.
0 ft. to 9 ft. top soil
9 " 127 " sand
127 " 409 " sandy clay
409 " 564 " clay
564 " 740 " sandy clay
740 " 743 " sand
743 " 881 " blue clay
881 " 943 " sandy clay
943 " 1066 " hard shale
1066 " 1220 " sandy clay
1220 " 1370 " blue shale
1370 " 1441 " hard blue shale
1441 " 1565 " hard shale
1565 " 1750 " shale w/ sand streaks

CONFIDENTIAL
Water Code Sec. 13752

Work started 12-28-68 19 Completed 1-15-68 19

WELL DRILLER'S STATEMENT:
This well was drilled under my jurisdiction and this report is true to the best of my knowledge and belief.

NAME Whitten Pumps, Inc.
(Person, firm, or corporation) (Typed or printed)
Address 1744 Inyo St.
Delano, Calif. 93215
[SIGNED] [Signature]
Well Driller
License No. 148282 Dated 10-23-68 19

24/27-20

ORIGINAL File Original, Duplicate and Triplicate with the REGIONAL WATER POLLUTION CONTROL BOARD No. 5 (Insert appropriate number)

WATER WELL DRILLERS REPORT

(Sections 7076, 7077, 7078, Water Code)

STATE OF CALIFORNIA

LOCATION NOT CHECKED Do Not Fill In

No. 60087

State Well No.

Other Well No. 245/27E-20

(1) OWNER:

Name Lanza Vineyards Address P.O. Box 397 Delano, Calif.

(2) LOCATION OF WELL:

County Tulare Owner's number, if any— R. F. D. or Street No. 1/4 mile North of Ave. 16 3/8 mile East of Rd. 216

(3) TYPE OF WORK (check):

New well [X] Deepening [] Reconditioning [] Abandon [] If abandonment, describe material and procedure in Item 11.

(4) PROPOSED USE (check):

Domestic [] Industrial [] Municipal [] Irrigation [X] Test Well [] Other [] Rotary Cable [X] Dug Well []

(5) EQUIPMENT:

Rotary Cable [X] Dug Well []

(6) CASING INSTALLED:

SINGLE [X] DOUBLE [] From 1,824 ft. to 14" single Top to bottom Diameter of Bore 26 3/4" If gravel packed Size of gravel 3/8" Describe joint Butt welded

(7) PERFORATIONS:

Type of perforator used Machine Size of perforations 1/8 X 1cc in., length, by From 648 ft. to 1824 ft. Perf. per row 21 Rows per ft. 3

(8) CONSTRUCTION:

Was a surface sanitary seal provided? [] Yes [X] No To what depth ft. Were any strata sealed against pollution? [] Yes [X] No If yes, note depth of strata From ft. to ft. Method of Sealing

(9) WATER LEVELS:

Depth at which water was first found not known ft. Standing level before perforating ft. Standing level after perforating ft.

(10) WELL TESTS:

Was a pump test made? [] Yes [X] No If yes, by whom? Yield: gal./min. with ft. draw down after hrs. Temperature of water Was a chemical analysis made? [] Yes [X] No Was electric log made of well? [] Yes [X] No

(11) WELL LOG:

Table with columns for depth (ft.) and formation description. Total depth 1824 ft. Depth of completed well 1824 ft. Formation: Describe by color, character, size of material, and structure. 0 ft. to 86 ft. Sandy Top Soil, 86 to 196 Sandy Clay, 196 to 200 Hard Sand, 200 to 285 Sandy Clay, 285 to 302 Hard Sand, 302 to 460 Sandy Clay, 460 to 500 Sandy Clay, 500 to 540 Hard Clay, 540 to 543 Sand, 543 to 620 Hard Clay, 620 to 640 Hard Shale, 640 to 723 Hard Clay, 723 to 763 Shale, 763 to 840 Blue Clay, 840 to 843 Sand, 843 to 1042 Blue Clay, 1042 to 1105 Shale, 1105 to 1125 Soft Clay, 1125 to 1140 Shale, 1140 to 1230 Blue Clay, 1230 to 1233 Sand, 1233 to 1275 Blue Shale, 1275 to 1295 Hard Shale, 1295 to 1450 Clay, 1450 to 1452 Hard Shale, 1452 to 1481 Clay, 1481 to 1515 Hard Shale, 1515 to 1526 Clay, 1526 to 1570 Hard Shale, 1570 to 1574 Sand, 1574 to 1616 Hard Shale, 1616 to 1626 Sand, 1626 to 1636 Shale, 1636 to 1691 Clay & Shale, 1691 to 1739 Sand, 1739 to 1824 Hard Shale

CONFIDENTIAL Section 7076.1, Water Code

Work started 12/26/59 Completed 1/21/60

WELL DRILLER'S STATEMENT:

This well was drilled under my jurisdiction and this report is true to the best of my knowledge and belief.

NAME Whitten Pumps, Inc. Address 1744 High Street Delano, Calif.

[SIGNED] [Signature] Well Driller License No. 148282 Dated 7-15-60

File Original with DWR

State of California
Well Completion Report

Refer to Instruction Pamphlet
No. e059519

DWR Use Only - Do Not Fill In

23S/27E-34

State Well Number/Site Number

Latitude Longitude

APN/TRS/Other

Page 1 of 2

Owner's Well Number _____

Date Work Began 07/12/2007 Date Work Ended 9/25/2007

Local Permit Agency Tulare County Environmental Health Department

Permit Number 07-0234 Permit Date 5/23/07

Geologic Log		
Orientation <input checked="" type="radio"/> Vertical <input type="radio"/> Horizontal <input type="radio"/> Angle Specify _____		
Drilling Method <u>Direct Rotary</u>		Drilling Fluid <u>Bentonite mud</u>
Depth from Surface		Description
Feet	to Feet	Describe material, grain size, color, etc
0	32	Drill conductor
32	115	Fine to coarse sand
115	125	80% fine to coarse sand, 20% clay
125	135	Coarse sand with some clay
135	155	Fine to coarse sand
155	186	Fine to coarse sand with a little clay
186	245	5% fine to medium sand, 95% brown clay
245	330	95% brown and white clay, 5% medium sand
330	345	60% brown clay, 40% fine to medium sand
345	350	Brown clay
350	370	70% brown clay, 30% fine to medium sand
370	470	80% brown clay, 20% fine to medium sand
470	483	60% white and brown clay, 40% fine to medium sand
483	493	90% white and brown clay, 10% sand
493	503	80% fine to medium sand, 20% clay
503	535	95% blue & brown clay, 5% fine sand
535	567	Blue and brown clay, with some shale and fine sand
567	785	80% blue and brown clay, 20% sand
785	816	Hard blue and brown clay with some sand
816	878	90% blue-green shale and fine sand
878	888	80% blue clay and shale with some fine sand
888	898	90% clay and hard shale with fine to medium sand
898	970	Clay and hard shale
970	1,006	Clay and hard shale with some fine sand
1006	1,038	80% blue clay with shale and fine sand
1038	1,058	70% blue clay and shale with fine to medium sand
1058	1,100	80% blue clay and shale with fine sand
1100	1,110	60% clay and shale, 40% fine to coarse sand
1110	1,130	Blue clay and shale with some fine sand
Total Depth of Boring <u>1832</u>		Feet
Total Depth of Completed Well <u>1800</u>		Feet

Well Owner

Name JAY, LLC

Mailing Address 5060 California Avenue, Suite 910

City Bakersfield State CA Zip 93309

Well Location

Address Hwy 56 & 240th, 1 mile SW

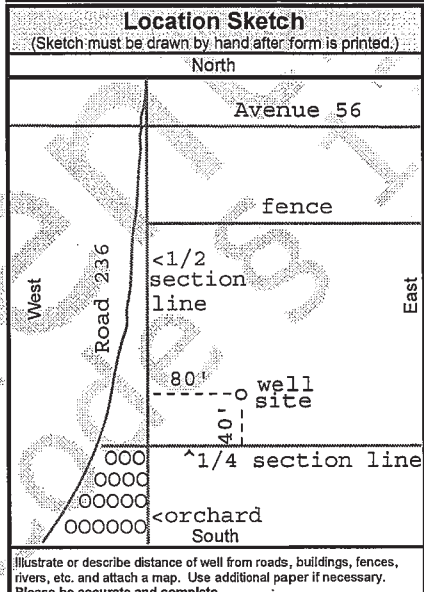
City Ducor County Tulare

Latitude 35 52 51 N Longitude 119 2 37 W
Deg. Min. Sec. Deg. Min. Sec.

Datum WGS84 Decimal Lat. _____ Decimal Long. _____

APN Book 321 Page 160 Parcel 009

Township 23S Range 27E Section 34



Activity

New Well
 Modification/Repair
 Deepen
 Other _____

Destroy
Describe procedures and materials under "GEOLOGIC LOG"

Planned Uses

Water Supply
 Domestic Public
 Irrigation Industrial

Cathodic Protection
 Dewatering
 Heat Exchange
 Injection
 Monitoring
 Remediation
 Sparging
 Test Well
 Vapor Extraction
 Other _____

Water Level and Yield of Completed Well

Depth to first water 511 (Feet below surface)

Depth to Static _____

Water Level 511 (Feet) Date Measured 09/25/2007

Estimated Yield * 2,000 (GPM) Test Type Constant Rate

Test Length 8.0 (Hours) Total Drawdown 26 (Feet)

*May not be representative of a well's long term yield. PL 537

Casings							Annular Material				
Depth from Surface	Borehole Diameter	Type	Material	Wall Thickness	Outside Diameter	Screen Type	Slot Size if Any	Depth from Surface	Fill	Description	
Feet to Feet	(Inches)			(Inches)	(Inches)		(Inches)	Feet to Feet			
0	20	36	Conductor	A53B	.375	30		0	150	Cement	10-sack
0	160	26	Solid	A53B	.375	16		150	1,832	Filter Pack	1/4 x 10 Gravel
160	760	26	Solid	A53B	.312	16					
760	880	26	Perforated	A53B	.312	16	Millslot	0.070			
880	1,000	26	Perforated	A53B	.312	16	Millslot	0.070			
1,000	1,260	26	Perforated	A53B	.312	16	Millslot	0.040			

Attachments

Geologic Log
 Well Construction Diagram
 Geophysical Log(s)
 Soil/Water Chemical Analyses
 Other _____

Attach additional information, if it exists.

Certification Statement

I, the undersigned, certify that this report is complete and accurate to the best of my knowledge and belief

Name Rottman Drilling Co.

Person, Firm or Corporation
46471 N. Division Street Lancaster CA 93535-5906
Address City State Zip

Signed *Michael W. Fortman* 10/26/07 316599
C-57 Licensed Water Well Contractor Date Signed C-57 License Number

*The free Adobe Reader may be used to view and complete this form. However, software must be purchased to complete, save, and reuse a saved form.

2/2

File Original with DWR

State of California

Well Completion Report

Refer to Instruction Pamphlet

No. e059520

DWR Use Only - Do Not Fill In.

23S/27E-34

State Well Number/Site Number

Latitude Longitude

APN/TRS/Other

Page 2 of 2

Owner's Well Number

Date Work Began 07/12/2007 Date Work Ended 9/25/2007

Local Permit Agency Tulare County Environmental Health Department

Permit Number 07-0234 Permit Date 5/23/07

Geologic Log		
Orientation <input checked="checked" type="radio"/> Vertical <input type="radio"/> Horizontal <input type="radio"/> Angle Specify _____		
Drilling Method Direct Rotary Drilling Fluid Bentonite mud		
Depth from Surface	Description	
Feet to Feet	Describe material, grain size, color, etc	
1,130	1,200	Blue clay and shale with some fine sand
1,200	1,210	Blue clay, 30% fine to medium sand
1,210	1,240	blue clay, shale, and some fine sand
1,240	1,290	Fie to medium sand with some clay
1,290	1,330	Blue clay with some sand
1,330	1,400	Grey-blue clay and shale
1,400	1,440	Fine to coarse sand with some clay
1,440	1,452	70% clay with fine to medium sand
1,452	1,534	Fine to coarse sand, 30%clay
1,534	1,630	Fine to coarse sand, 30%clay with some silt
1,630	1,693	Fine to coarse sand with some clay and silt
1,693	1,724	Fine sand with some silty clay
1,724	1,755	Fine to coarse sand with silty blue-green clay
1,755	1,774	Blue-green silty clay with shale and fine sand
1,774	1,786	Coarse sand with hard silty clay
1,786	1,817	Hard blue clay with a little sand or shale
1,817	1,832	Hard blue clay
Total Depth of Boring 1832 Feet		
Total Depth of Completed Well 1800 Feet		

Well Owner

Name JAY, LLC

Mailing Address 5060 California Avenue, Suite 910

City Bakersfield State CA Zip 93309

Well Location

Address Hwy 56 & 240th, 1 mile SW

City Ducor County Tulare

Latitude 35 52 51 N Longitude 119 2 37 W
Deg. Min. Sec. Deg. Min. Sec.

Datum WGS84 Decimal Lat. _____ Decimal Long. _____

APN Book 321 Page 160 Parcel 009

Township 23S Range 27E Section 34

Location Sketch

(Sketch must be drawn by hand after form is printed.)

North

SEE PAGE 1

West East

South

Illustrate or describe distance of well from roads, buildings, fences, rivers, etc. and attach a map. Use additional paper if necessary. Please be accurate and complete.

Activity

New Well
 Modification/Repair
 Deepen
 Other _____
 Destroy
Describe procedures and materials under "GEOLOGIC LOG"

Planned Uses

Water Supply
 Domestic Public
 Irrigation Industrial

Cathodic Protection
 Dewatering
 Heat Exchange
 Injection
 Monitoring
 Remediation
 Sparging
 Test Well
 Vapor Extraction
 Other _____

Water Level and Yield of Completed Well

Depth to first water 511 (Feet below surface)

Depth to Static _____

Water Level 511 (Feet) Date Measured 09/25/2007

Estimated Yield * 2,000 (GPM) Test Type Constant Rate

Test Length 8.0 (Hours) Total Drawdown 26 (Feet)

*May not be representative of a well's long term yield. PL 537

Casings								
Depth from Surface	Borehole Diameter	Type	Material	Wall Thickness	Outside Diameter	Screen Type	Slot Size if Any	
Feet to Feet	(Inches)			(Inches)	(Inches)		(Inches)	
1,260	1,500	26	Perforated	A53B	.312	16	Millslot	0.080
1,500	1,740	26	Perforated	A53B	.312	16	Millslot	0.070

Annular Material			
Depth from Surface	Fill	Description	
Feet to Feet			
0	150	Cement	10-sack
150	1,832	Filter Pack	1/4 x 10 Gravel

Attachments

Geologic Log
 Well Construction Diagram
 Geophysical Log(s)
 Soil/Water Chemical Analyses
 Other _____

Attach additional information, if it exists.

Certification Statement

I, the undersigned, certify that this report is complete and accurate to the best of my knowledge and belief

Name Rottman Drilling Co.
 Person, Firm or Corporation
 46471 N. Division Street Lancaster CA 93535-5906
Address City State Zip

Signed *Robert W. Rottman* Date Signed 10/26/07
 C-57 Licensed Water Well Contractor 316599
 C-57 License Number

STATE OF CALIFORNIA
WELL COMPLETION REPORT

DWR USE ONLY — DO NOT FILL IN

238127E-27

STATE WELL NO./STATION NO.

LATITUDE _____ LONGITUDE _____

APN/TRS/OTHER _____

Page 1 of 1

Owner's Well No. North
Date Work Began 6-4-04, Ended 8-20-04

No. **0925804**

Local Permit Agency Tulare County Environmental Health
Permit No. 5400542 Permit Date 5-19-04

GEOLOGIC LOG			WELL OWNER	
ORIENTATION () <input checked="" type="checkbox"/> VERTICAL _____ HORIZONTAL _____ ANGLE _____ (SPECIFY)			Name <u>Ducor Community Services Dist</u>	
DRILLING METHOD <u>Reverse Circulation</u> FLUID <u>Poly Bore</u>			Mailing Address <u>P.O. Box 137</u>	
DEPTH FROM SURFACE			City <u>Ducor</u> CA 93218	
DESCRIPTION			STATE _____ ZIP _____	
Describe material, grain size, color, etc.			WELL LOCATION	
Ft.	to	Ft.	Address <u>14 Mile N. of Ave 56 75' West Brady</u>	
0	60	Clay & Gravel	City <u>Ducor</u>	
60	200	Sand & Clay	County <u>Tulare</u>	
200	240	Sand & Little Clay	APN Book <u>321</u> Page <u>080</u> Parcel <u>025</u>	
240	370	Sand & Grey Clay	Township <u>23</u> Range <u>27E</u> Section <u>27</u>	
370	380	Clay & Little Sand	Lat _____ N Long _____ W	
380	390	Green Clay & Sand	DEG. MIN. SEC. DEG. MIN. SEC.	
390	400	Clay & Little Sand	LOCATION SKETCH	
400	410	Sand & Clay	NORTH	
410	440	Green Clay & Sand	WEST	
440	540	Green Clay & Fine Sand	EAST	
540	550	Green Clay Sand & Little Rock	SOUTH	
550	930	Sand & Grey Clay	Illustrate or Describe Distance of Well from Roads, Buildings, Fences, Rivers, etc. and attach a map. Use additional paper if necessary. PLEASE BE ACCURATE & COMPLETE.	
930	940	Grey Clay	ACTIVITY ()	
940	960	Fine Sand & Grey Clay	<input checked="" type="checkbox"/> NEW WELL	
960	1000	Sand Grey Clay & Shell	MODIFICATION/REPAIR	
1000	1060	Sand & Grey Clay	_____ Deepen	
1060	1090	Sand Grey Clay & Little Rock	_____ Other (Specify)	
1090	1150	Sand & Grey Clay	DESTROY (Describe Procedures and Materials Under "GEOLOGIC LOG")	
1150	1230	Sand Shell & Grey Clay	USES ()	
1230	1270	Shell & Grey Clay	WATER SUPPLY	
1270	1290	Fine Sand & Shell, Grey Clay	_____ Domestic <input checked="" type="checkbox"/> Public	
1290	1380	Fine Sand & Grey Clay	_____ Irrigation _____ Industrial	
1380	1430	Grey Clay	MONITORING _____	
1430	1460	Fine Sand & Grey Clay	TEST WELL _____	
1460	1500	Grey Clay	CATHODIC PROTECTION _____	
TOTAL DEPTH OF BORING <u>1425</u> (Feet)			HEAT EXCHANGE _____	
TOTAL DEPTH OF COMPLETED WELL <u>1405</u> (Feet)			DIRECT PUSH _____	
			INJECTION _____	
			VAPOR EXTRACTION _____	
			SPARGING _____	
			REMEDICATION _____	
			OTHER (SPECIFY) _____	
WATER LEVEL & YIELD OF COMPLETED WELL				
DEPTH TO FIRST WATER <u>502</u> (Ft.) BELOW SURFACE				
DEPTH OF STATIC WATER LEVEL <u>502</u> (Ft.) & DATE MEASURED <u>7-26-04</u>				
ESTIMATED YIELD * <u>550</u> (GPM) & TEST TYPE <u>Constant/ Flowmeter</u>				
TEST LENGTH <u>24</u> (Hrs.) TOTAL DRAWDOWN <u>97</u> (Ft.)				
* May not be representative of a well's long-term yield.				

DEPTH FROM SURFACE	BORE-HOLE DIA. (Inches)	CASING (S)					ANNULAR MATERIAL					
		TYPE ()	MATERIAL / GRADE	INTERNAL DIAMETER (Inches)	GAUGE OR WALL THICKNESS	SLOT SIZE IF ANY (Inches)	CE-MENT ()	BEN-TONITE ()	FILL ()	FILTER PACK (TYPE/SIZE)		
0	50	42		x	ASTM 139	30	5/16					
+2	1015	26	x		ASTM A 606	14	5/16					
1015	1035	26	x		ASTM A 606	14	5/16	Comp Section				6x16
1035	1385	26	x		A 606 Full Flo	14	5/16	.060				CCST
1385	1405	26	x		ASTM A 606	14	5/16					
+2	1010	26		x	A53 Grade B	3	Sch.40					

ATTACHMENTS ()

____ Geologic Log

____ Well Construction Diagram

____ Geophysical Log(s)

____ Soil/Water Chemical Analyses

____ Other _____

ATTACH ADDITIONAL INFORMATION, IF IT EXISTS.

CERTIFICATION STATEMENT

I, the undersigned, certify that this report is complete and accurate to the best of my knowledge and belief.

NAME Bakersfield Well & Pump Co.
(PERSON, FIRM, OR CORPORATION) (TYPED OR PRINTED)

ADDRESS 7212 Fruitvale Ave Bakersfield CA 93308
CITY STATE ZIP

Signed [Signature] DATE SIGNED 11-11-04 C-57 LICENSE NUMBER 440537
C-57 LICENSED WATER WELL CONTRACTOR

23/27-19R1

LOCATION NOT CHECKED

ORIGINAL File Original, Duplicate and Triplicate with the REGIONAL WATER POLLUTION CONTROL BOARD No. (Insert appropriate number)

WATER WELL DRILLERS REPORT

(Sections 7076, 7077, 7078, Water Code)

STATE OF CALIFORNIA

Do Not Fill In No. 14164

State Well No. 19R Other Well No. 23/27-34

(1) OWNER:

Name Guimarra Vineyards Co. Address P. O. Box 1653 Bakersfield, Calif.

(2) LOCATION OF WELL:

County Tulare Owner's number, if any 5 R. F. D. or Street No. E. End of Road 64

(3) TYPE OF WORK (check):

New well [X] Deepening [] Reconditioning [] Abandon [] If abandonment, describe material and procedure in Item 11.

(4) PROPOSED USE (check):

Domestic [] Industrial [] Municipal [] Irrigation [X] Test Well [] Other []

(5) EQUIPMENT:

Rotary [X] Cable [] Dug Well []

(6) CASING INSTALLED:

Table with columns for From, to, Diam., Gage or Wall, Diameter of Bore, from, to, Size of gravel. Includes entries for 0-795, 785, 780-1610, and 1610-1817.

(7) PERFORATIONS:

Type of perforator used Machine Size of perforations 125 mesh in., length, by 2" in. From 645 to 1610 Perf. per row 14 rows on 6" centers Rows per ft.

(8) CONSTRUCTION:

Was a surface sanitary seal provided? [] Yes [] No To what depth ft. Were any strata sealed against pollution? [X] Yes [] No If yes, note depth of strata From 1610 ft. to 1817 ft. Method of Sealing cemented

(9) WATER LEVELS:

Depth at which water was first found ft. Standing level before perforating ft. Standing level after perforating ft.

(10) WELL TESTS:

Was a pump test made? [X] Yes [] No If yes, by whom? I.S.A. Camp Co. Yield: 3500 gal./min. with 37 ft. draw down after 6 hrs. Temperature of water: Was chemical analysis made? [] Yes [] No Was electric log made of well? [X] Yes [] No

(11) WELL LOG:

Total depth 1817' ft. Depth of completed well 1610' ft. Formation: Describe by color, character, size of material, and structure. 0 to 75 ft. Surface 75 to 130 Sand with str of clay 130 to 360 Sandy brown clay 360 to 460 Sandy br. clay w/ stks of sand 460 to 696 Sandy blue " " " " 696 to 800 Sandy clay 800 to 845 Hard Sand 845 to 900 Hard Sandy Blue Clay 900 to 960 Sand w/ thin streaks blue clay 960 to 1127 Blue shale 1127 to 1220 Hard blue shale w/ stks hard sand 1220 to 1517 Blue clay w/ streaks of sand 1517 to 1817 Sand w/ streaks of blue clay and hard shale

CONFIDENTIAL Section 7076.1, Water Code

Work started 6-5-57 19 Completed 6-21-57 19

WELL DRILLER'S STATEMENT:

This well was drilled under my jurisdiction and this report is true to the best of my knowledge and belief.

NAME HYLTON DRILLING CO. (Person, firm, or corporation) (Typed or printed) Address 716 Eye Street Bakersfield, Calif.

[SIGNED] [Signature] Well Driller License No. 111580 Dated June 25, 1957

ORIGINAL
File with DWR

Page 1 of 2

Owner's Well No. _____

Date Work Began 5-19-08, Ended 6-30-08

Local Permit Agency TULARE COUNTY

Permit No. 08-0200 Permit Date 4-23-08

STATE OF CALIFORNIA
WELL COMPLETION REPORT

Refer to Instruction Pamphlet

No. **0942277**

DWR USE ONLY - DO NOT FILL IN

23S/27E-07 / 15
STATE WELL NO./STATION NO.

LATITUDE _____ LONGITUDE _____

APN/TRS/OTHER _____

GEOLOGIC LOG

WELL OWNER

ORIENTATION ()		DRILLING METHOD		FLUID		ANGLE (SPECIFY)	
		<input checked="" type="checkbox"/> VERTICAL		<input type="checkbox"/> HORIZONTAL		<input type="checkbox"/> _____	
		Rotary		Mud			
DEPTH FROM SURFACE		DESCRIPTION					
Ft.	to Ft.	Describe material, grain size, color, etc.					
0	50	TOP SOIL					
50	100	SAND					
100	140	SANDY CLAY					
140	150	SAND					
150	180	CLAY					
180	190	SAND					
190	290	CLAY					
290	310	SAND					
310	350	SANDY CLAY					
350	360	SAND					
360	390	SANDY CLAY					
390	410	SAND					
410	490	SANDY CLAY					
490	510	SAND					
510	660	SANDY CLAY					
660	690	SAND					
690	730	SANDY CLAY					
730	750	SAND					
750	820	SANDY CLAY					
820	830	CLAY					
830	850	SAND					
850	960	SANDY CLAY					
960	980	SAND					
980	1010	SHALE					
1010	1050	SANDY CLAY					
1050	1060	CLAY					
1060	1080	SAND					
1080	1090	CLAY					
1090	1100	SAND					
1100	1110	CLAY					
TOTAL DEPTH OF BORING _____ (Feet)							
TOTAL DEPTH OF COMPLETED WELL _____ (Feet)							

Name: DOLE FRESH FRUIT CO

Mailing Address: 1 DOLE AVE
WESTLAKE VILLAGE CA 91362

Address: 1490 RD 208 100 N 1/2 AVE 80
City: TERRA BELLA
County: TULARE

APN Book 320 Page 010 Parcel 013
Township 23S Range 27E Section 07

Lat _____ N Long _____ W

LOCATION SKETCH

WEST RD. 208 EAST

← 1/4 → X NEW WELL

AVE 80

SOUTH

Illustrate or Describe Distance of Well from Roads, Buildings, Fences, Rivers, etc. and attach a map. Use additional paper if necessary. PLEASE BE ACCURATE & COMPLETE.

ACTIVITY ()

NEW WELL

MODIFICATION/REPAIR

___ Deepen

___ Other (Specify) _____

___ DESTROY (Describe Procedures and Materials Under "GEOLOGIC LOG")

USES ()

WATER SUPPLY

Domestic ___ Public ___

Irrigation ___ Industrial ___

MONITORING ___

TEST WELL ___

CATHODIC PROTECTION ___

HEAT EXCHANGE ___

DIRECT PUSH ___

INJECTION ___

VAPOR EXTRACTION ___

SPARGING ___

REMEDICATION ___

OTHER (SPECIFY) _____

WATER LEVEL & YIELD OF COMPLETED WELL

DEPTH TO FIRST WATER _____ (Ft.) BELOW SURFACE

DEPTH OF STATIC WATER LEVEL 476 (Ft.) & DATE MEASURED 8-6-08

ESTIMATED YIELD 1300 (GPM) & TEST TYPE Pump

TEST LENGTH 16 (Hrs.) TOTAL DRAWDOWN 551 (Ft.)

* May not be representative of a well's long-term yield.

DEPTH FROM SURFACE	BORE-HOLE DIA. (Inches)	CASING (S)							
		TYPE ()				MATERIAL / GRADE	INTERNAL DIAMETER (Inches)	GAUGE OR WALL THICKNESS	SLOT SIZE IF ANY, (Inches)
Ft.	to Ft.	BLANK	SCREEN	CON-DUCTOR	FILL PIPE				
0	40				X	A53B	3 3/4	.188	
0	625	X				A53B	15 1/4	.312	
625	1800		X			A53B	15 1/4	.312	.90

DEPTH FROM SURFACE	ANNULAR MATERIAL TYPE				
		CE-MENT ()	BEN- TONITE ()	FILL ()	FILTER PACK (TYPE/SIZE)
Ft.	to Ft.				
0	30	X			
30	1800				1/4" GRAVEL

ATTACHMENTS ()

___ Geologic Log

___ Well Construction Diagram

Geophysical Log(s)

___ Soil/Water Chemical Analyses

___ Other _____

ATTACH ADDITIONAL INFORMATION, IF IT EXISTS.

CERTIFICATION STATEMENT

I, the undersigned, certify that this report is complete and accurate to the best of my knowledge and belief.

NAME Whitten Pump Inc.
(PERSON, FIRM, OR CORPORATION) (TYPED OR PRINTED)

ADDRESS 502 COUNTYLINE RD DELANO CA 93215
CITY STATE ZIP

Signed Paul A. Whitt DATE SIGNED 8/11/2008
C-57 LICENSED WATER WELL CONTRACTOR C-57 LICENSE NUMBER 148282

ORIGINAL
File with DWR

Page 2 of 2

Owner's Well No. _____

Date Work Began 5-19-08, Ended 6-30-08

Local Permit Agency Tulare County

Permit No. 08-0200 Permit Date _____

(Continued)

STATE OF CALIFORNIA WELL COMPLETION REPORT

Refer to Instruction Pamphlet

No. **0942278**

DWR USE ONLY -- DO NOT FILL IN	
<u>23S / 27E + 07</u>	<u>2</u>
STATE WELL NO./STATION NO.	
LATITUDE	LONGITUDE
APN/TRS/OTHER	

GEOLOGIC LOG

WELL OWNER

ORIENTATION () VERTICAL _____ HORIZONTAL _____ ANGLE _____ (SPECIFY)

Name DOLE FRESH FRUIT CO

DRILLING METHOD _____ FLUID _____

Mailing Address _____

DEPTH FROM SURFACE
Ft. to Ft.

DESCRIPTION
Describe material, grain size, color, etc.

CITY _____ STATE _____ ZIP _____

1110	1130	SAND
1130	1140	CLAY
1140	1150	SAND
1150	1170	CLAY
1170	1190	SAND
1190	1220	CLAY
1220	1250	SAND
1250	1290	SANDY CLAY
1290	1310	CLAY
1310	1330	SAND
1330	1350	CLAY
1350	1360	SAND
1360	1440	CLAY
1440	1450	SANDY CLAY
1450	1570	SAND
1570	1580	CLAY
1580	1610	SAND
1610	1670	CLAY
1670	1720	SAND
1720	1760	SANDY CLAY
1760	1800	SAND

WELL LOCATION

Address _____

City _____

County _____

APN Book _____ Page _____ Parcel _____

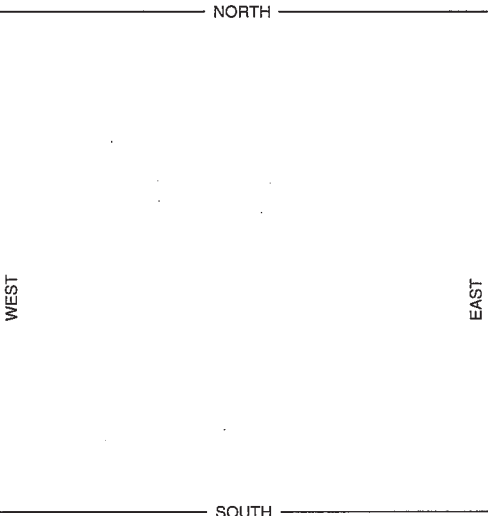
Township 23S Range 27E Section 07

Lat _____ N Long _____ W

DEG. MIN. SEC. DEG. MIN. SEC.

LOCATION SKETCH

ACTIVITY ()



NEW WELL

MODIFICATION/REPAIR
 Deepen
 Other (Specify) _____

DESTROY (Describe Procedures and Materials Under "GEOLOGIC LOG") _____

USES ()
 WATER SUPPLY
 Domestic Public
 Irrigation Industrial

MONITORING _____
 TEST WELL _____
 CATHODIC PROTECTION _____
 HEAT EXCHANGE _____
 DIRECT PUSH _____
 INJECTION _____
 VAPOR EXTRACTION _____
 SPARGING _____
 REMEDIATION _____
 OTHER (SPECIFY) _____

Illustrate or Describe Distance of Well from Roads, Buildings, Fences, Rivers, etc. and attach a map. Use additional paper if necessary. PLEASE BE ACCURATE & COMPLETE.

WATER LEVEL & YIELD OF COMPLETED WELL

DEPTH TO FIRST WATER _____ (Ft.) BELOW SURFACE

DEPTH OF STATIC

WATER LEVEL _____ (Ft.) & DATE MEASURED _____

ESTIMATED YIELD * _____ (GPM) & TEST TYPE _____

TEST LENGTH _____ (Hrs.) TOTAL DRAWDOWN _____ (Ft.)

* May not be representative of a well's long-term yield.

TOTAL DEPTH OF BORING _____ (Feet)

TOTAL DEPTH OF COMPLETED WELL _____ (Feet)

DEPTH FROM SURFACE Ft. to Ft.	BORE-HOLE DIA. (Inches)	CASING (S)										
		TYPE ()				MATERIAL / GRADE	INTERNAL DIAMETER (Inches)	GAUGE OR WALL THICKNESS	SLOT SIZE IF ANY (Inches)			
BLANK	SCREEN	CON-DUCTOR	FILL PIPE									

DEPTH FROM SURFACE Ft. to Ft.	ANNULAR MATERIAL			
	TYPE			
	CE-MENT ()	BEN-TONITE ()	FILL ()	FILTER PACK (TYPE/SIZE)

ATTACHMENTS ()

- Geologic Log
- Well Construction Diagram
- Geophysical Log(s)
- Soil/Water Chemical Analyses
- Other _____

ATTACH ADDITIONAL INFORMATION, IF IT EXISTS.

CERTIFICATION STATEMENT

I, the undersigned, certify that this report is complete and accurate to the best of my knowledge and belief.

NAME _____
(PERSON, FIRM, OR CORPORATION) (TYPED OR PRINTED)

ADDRESS _____ CITY _____ STATE _____ ZIP _____

Signed Juan A. White
C-57 LICENSED WATER WELL CONTRACTOR

DATE SIGNED 8/11/2008

C-57 LICENSE NUMBER _____

STATE OF CALIFORNIA
WELL COMPLETION REPORT

Refer to Instruction Pamphlet

No. **783343**

DWR USE ONLY - DO NOT FILL IN

23S/26E-23R1

STATE WELL NO./STATION NO.

LATITUDE _____ LONGITUDE _____

APN/TRS/OTHER _____

GEOLOGIC LOG

ORIENTATION (±)		DRILLING METHOD		FLUID		DESCRIPTION <i>Describe material, grain size, color, etc.</i>
Ft.	to Ft.	VERTICAL	HORIZONTAL	ANGLE	(SPECIFY)	
		<input checked="" type="checkbox"/>				
0	260					SANDY CLAY
260	275					SAND
275	500					SANDY CLAY
500	515					SAND
515	570					SANDY CLAY
570	590					CLAY
590	635					SANDY CLAY
635	660					SAND
660	700					SANDY CLAY
700	720					SAND
720	770					SANDY CLAY
770	795					CLAY
795	875					SANDY CLAY
875	895					SAND
895	960					SANDY CLAY
960	995					SAND
995	1105					SANDY CLAY
1105	1120					SAND
1120	1145					CLAY
1145	1165					SAND
1165	1240					SANDY CLAY
1240	1265					CLAY
1265	1510					CLAY WITH SAND STREAKS
1510	1530					SAND
1530	1620					SANDY CLAY
1620	1645					SAND
1645	1670					SANDY CLAY
1670	1685					SAND
1685	1690					SANDY CLAY
1690	1720					SAND
TOTAL DEPTH OF BORING		1720	Feet			
TOTAL DEPTH OF COMPLETED WELL		1700	Feet			

WELL OWNER

Name **A.L.G. ENTERPRISES**
Mailing Address **RT. 2, BOX 299 DELANO CA. 93215**
CITY STATE ZIP

WELL LOCATION
Address **1-1/8 MILE NORTH OF AVENUE 56 AND**
City **1/4 MILE WEST OF ROAD 200**
County **TULARE COUNTY ENVIRONMENTAL HEALTH**
APN Book **319** Page **160** Parcel **01**
Township **23S** Range **26E** Section **23R**
Latitude _____ Longitude _____

LOCATION SKETCH

ACTIVITY (±)
 NEW WELL
MODIFICATION/REPAIR
— Deepen
— Other (Specify)
— DESTROY (Describe Procedures and Materials Under "GEOLOGIC LOG")
PLANNED USES (±)
WATER SUPPLY
 Domestic Public
 Irrigation Industrial
MONITORING _____
TEST WELL _____
CATHODIC PROTECTION _____
HEAT EXCHANGE _____
DIRECT PUSH _____
INJECTION _____
VAPOR EXTRACTION _____
SPARGING _____
REMEDICATION _____
OTHER (SPECIFY) _____

Illustrate or Describe Distance of Well from Roads, Buildings, Fences, Rivers, etc. and attach a map. Use additional paper if necessary. **PLEASE BE ACCURATE & COMPLETE.**

WATER LEVEL & YIELD OF COMPLETED WELL

DEPTH TO FIRST WATER _____ (Ft.) BELOW SURFACE
DEPTH OF STATIC WATER LEVEL _____ (Ft.) & DATE MEASURED _____
ESTIMATED YIELD * _____ (GPM) & TEST TYPE _____
TEST LENGTH _____ (Hrs.) TOTAL DRAWDOWN _____ (Ft.)
* May not be representative of a well's long-term yield.

DEPTH FROM SURFACE Ft. to Ft.	BORE-HOLE DIA. (Inches)	CASING (S)						ANNULAR MATERIAL					
		TYPE (±)				MATERIAL GRADE	INTERNAL DIAMETER (Inches)	GAUGE OR WALL THICKNESS	SLOT SIZE IF ANY (Inches)	TYPE			
		BLANK	SCREEN	CON-DOCTOR	FILL PIPE								
0	600	27	X			A53B	15.37	.312		X			
600	1700	27	X			A53B	15.37	.312	100X2-1/2				1/4" GRAVEL
0	30				X	A252	3.75						

- ATTACHMENTS (±)**
- Geologic Log
 - Well Construction Diagram
 - Geophysical Log(s)
 - Soil/Water Chemical Analyses
 - Other _____
- ATTACH ADDITIONAL INFORMATION, IF IT EXISTS.

CERTIFICATION STATEMENT

I, the undersigned, certify that this report is complete and accurate to the best of my knowledge and belief.

NAME **WHITTEN PUMPS, INC.**
(PERSON, FIRM OR CORPORATION) (TYPED OR PRINTED)
502 COUNTY LINE RD. DELANO CA. 93215
ADDRESS CITY STATE ZIP
Signed *Ronald E. Ryan* DATE SIGNED **3/9/01** 148282
WELL DRILLER/AUTHORIZED REPRESENTATIVE C-57 LICENSE NUMBER

STATE OF CALIFORNIA
WELL COMPLETION REPORT

DWR USE ONLY - DO NOT FILL IN

235/26E-11

STATE WELL NO./STATION NO.

LATITUDE _____ LONGITUDE _____

APN/TRS/OTHER _____

Page 1 of 1

Owner's Well No. _____ No. **0915717**

Date Work Began 3/16/05, Ended 4/13/05

Local Permit Agency Environmental Health Services

Permit No. 23791 Permit Date 2/24/05

GEOLOGIC LOG			WELL OWNER	
ORIENTATION () _____ VERTICAL _____ HORIZONTAL _____ ANGLE _____ (SPECIFY)			Name <u>Road 208 Ranches</u>	
DEPTH FROM SURFACE			Mailing Address <u>20191 Ave. 128</u>	
Ft. to Ft.			City <u>Porterville</u> State <u>Ca.</u> ZIP <u>93257</u>	
DESCRIPTION			WELL LOCATION	
Describe material, grain size, color, etc.			Address <u>Ave. 56 E. to 192, 192 N. to Ave. 80,</u>	
			City <u>Ave. 80, 3/8 mi. E. On L. side of rd.</u>	
			County <u>Tulare</u>	
			APN Book _____ Page _____ Parcel _____	
			Township <u>23</u> Range <u>26</u> Section <u>11</u>	
			Lat _____ Long _____	
			DEG. MIN. SEC. N Long DEG. MIN. SEC. W	
			LOCATION SKETCH	
			ACTIVITY ()	
			<input checked="" type="checkbox"/> NEW WELL	
			MODIFICATION/REPAIR	
			<input type="checkbox"/> Deepen <input type="checkbox"/> Other (Specify) _____	
			DESTROY (Describe Procedures and Materials Under "GEOLOGIC LOG")	
			USES ()	
			WATER SUPPLY	
			<input checked="" type="checkbox"/> Domestic _____ Public <input checked="" type="checkbox"/> Irrigation _____ Industrial	
			MONITORING _____	
			TEST WELL _____	
			CATHODIC PROTECTION _____	
			HEAT EXCHANGE _____	
			DIRECT PUSH _____	
			INJECTION _____	
			VAPOR EXTRACTION _____	
			SPARGING _____	
			REMEDICATION _____	
			OTHER (SPECIFY) _____	
			WATER LEVEL & YIELD OF COMPLETED WELL	
			DEPTH TO FIRST WATER _____ (Ft.) BELOW SURFACE	
			DEPTH OF STATIC WATER LEVEL _____ (Ft.) & DATE MEASURED _____	
			ESTIMATED YIELD * _____ (GPM) & TEST TYPE _____	
			TEST LENGTH _____ (Hrs.) TOTAL DRAWDOWN _____ (Ft.)	
			* May not be representative of a well's long-term yield.	
TOTAL DEPTH OF BORING <u>1069</u> (Feet)				
TOTAL DEPTH OF COMPLETED WELL <u>1011</u> (Feet)				

DEPTH FROM SURFACE	BORE-HOLE DIA. (Inches)	CASING (S)						DEPTH FROM SURFACE	ANNULAR MATERIAL				
		TYPE ()				MATERIAL / GRADE	INTERNAL DIAMETER (Inches)		GAUGE OR WALL THICKNESS	SLOT SIZE IF ANY (Inches)	TYPE		
Ft. to Ft.		BLANK	SCREEN	CON-DUCTOR	FILL PIPE								
0 to 1011	27 1/2						16	312	.090				
Blank Casing - 567'													
Perf. " - 444'													
0 - 50' top sanitary seal													

ATTACHMENTS ()

Geologic Log
 Well Construction Diagram
 Geophysical Log(s)
 Soil/Water Chemical Analyses
 Other _____

ATTACH ADDITIONAL INFORMATION, IF IT EXISTS.

CERTIFICATION STATEMENT

I, the undersigned, certify that this report is complete and accurate to the best of my knowledge and belief.

NAME WASCO DRILLING COMPANY, INC.

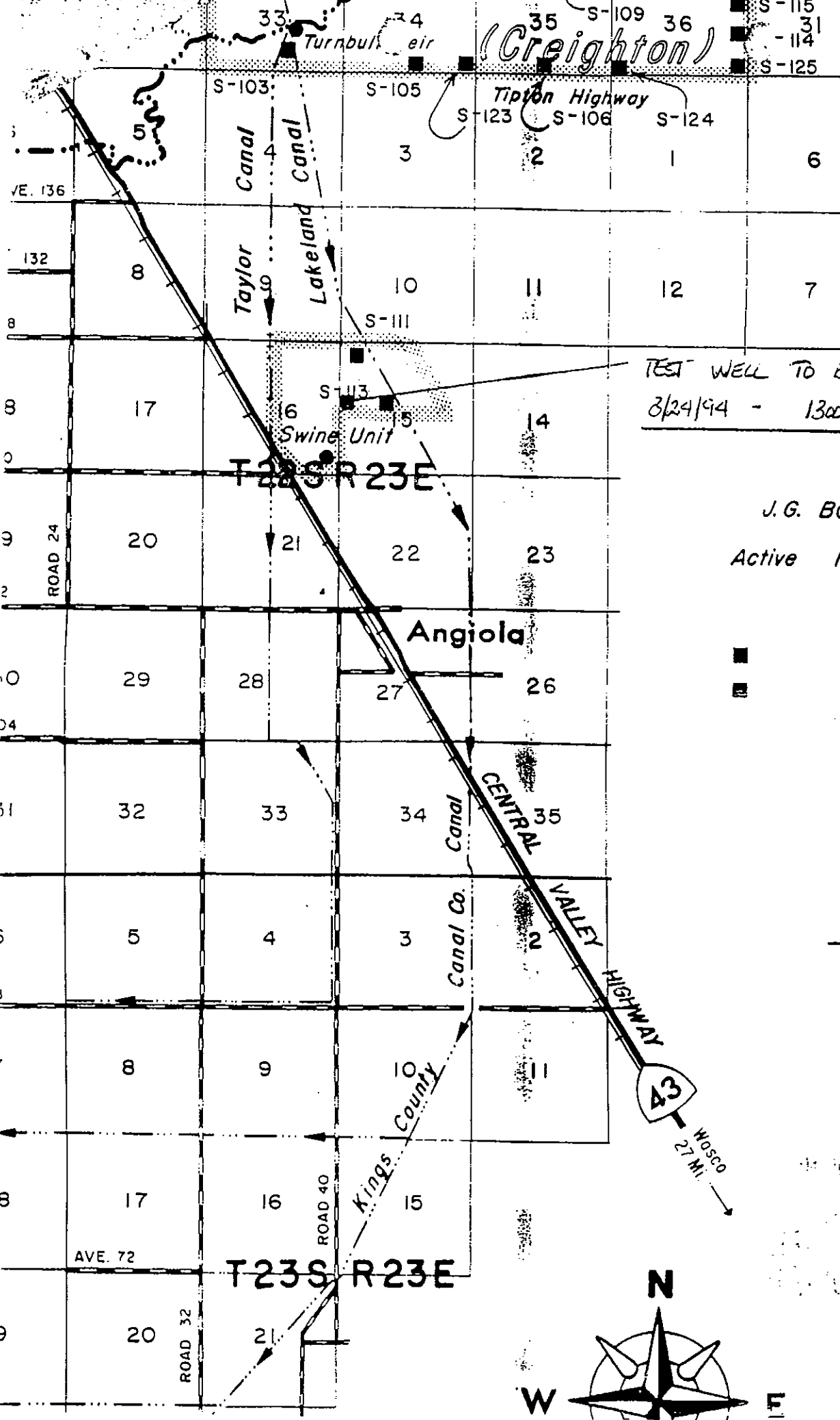
(PERSON, FIRM, OR CORPORATION) (TYPED OR PRINTED)

P. O. Box 181 Wasco Ca. 93280

ADDRESS CITY STATE ZIP

Signed [Signature] 4/18/05 582658

C-57 LICENSED WATER WELL CONTRACTOR DATE SIGNED C-57 LICENSE NUMBER

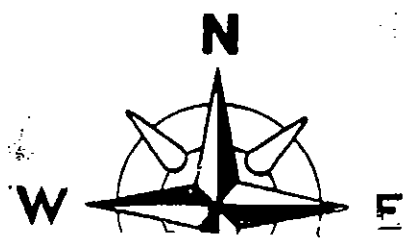
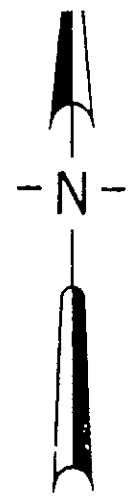


(Creighton)

TEST WELL TO BE DRILLED
3/24/94 - 1300 FT.

J.G. BOSWELL CO.

Active Irrigation Wells
6535-T



23/24-27C

ORIGINAL File Original, Duplicate and Triplicate with the REGIONAL WATER POLLUTION CONTROL BOARD No. 5 (Insert appropriate number)

WATER WELL DRILLERS REPORT

(Sections 7076, 7077, 7078, Water Code)

STATE OF CALIFORNIA

LOCATION NOT CHECKED Do Not Fill In

No. 63272

State Well No. 27C1

Other Well No. 23/24E-27

(1) OWNER:

Name Dr. A. W. Carlson Address P.O. Box 427 McFarland, Calif.

(2) LOCATION OF WELL:

County Tulare Owner's number, if any-- R. F. D. or Street No. 1/2 mile East of Road 88 and 1 mile North of Ave. 56. 125' S of 0.45 mi E/O NW Cor.

(3) TYPE OF WORK (check):

New well [X] Deepening [] Reconditioning [] Abandon [] If abandonment, describe material and procedure in Item 11.

(4) PROPOSED USE (check):

Domestic [] Industrial [] Municipal [] Irrigation [X] Test Well [] Other []

(5) EQUIPMENT:

Rotary [X] Cable [] Dug Well []

(6) CASING INSTALLED:

SINGLE [X] DOUBLE [] From 600 ft. to 1002 ft. Diam. 16" 1/4 single 14" 1/4 single If gravel packed Diameter of Bore 26" from Top to bottom Size of gravel: 3/8" Describe joint Butt Welded

(7) PERFORATIONS:

Type of perforator used Machine Size of perforations 1/8 X 1cc in., length, by From 804 ft. to 1602 ft. Perf. per row 18 Rows per ft.

(8) CONSTRUCTION:

Was a surface sanitary seal provided? [] Yes [X] No To what depth ft. Were any strata sealed against pollution? [] Yes [X] No If yes, note depth of strata From ft. to ft. Method of Sealing

(9) WATER LEVELS:

Depth at which water was first found Unknown ft. Standing level before perforating ft. Standing level after perforating ft.

(10) WELL TESTS:

Was a pump test made? [] Yes [X] No If yes, by whom? Yield: gal./min. with ft. draw down after hrs. Temperature of water Was a chemical analysis made? [] Yes [X] No Was electric log made of well? [] Yes [X] No

(11) WELL LOG:

Table with columns: Total depth, Depth of completed well, Formation, Depth (ft.), and Material. Includes entries like Top Soil, Sandy Clay, Clay, Sand, Shale, Blue Clay, etc.

DTW = 170' 11-18-70 JD

Work started 1/28/61 19 Completed 2/18/61 19

WELL DRILLER'S STATEMENT:

This well was drilled under my jurisdiction and this report is true to the best of my knowledge and belief.

NAME Whitten Pumps, Inc. (Person, firm, or corporation) (Typed or printed) Address 1744 High Street Delano, California

[SIGNED] Will Driller License No. 148282 Dated 3/27/61

*The free Adobe Reader may be used to view and complete this form. However, software must be purchased to complete, save, and reuse a saved form.

File Original with DWR

State of California Well Completion Report

Refer to Instruction Pamphlet

No. e0094489

Page 1 of 3

Owner's Well Number

Date Work Began 03/18/2009 Date Work Ended 4/20/2009

Local Permit Agency Tulare County Environmental Health Services

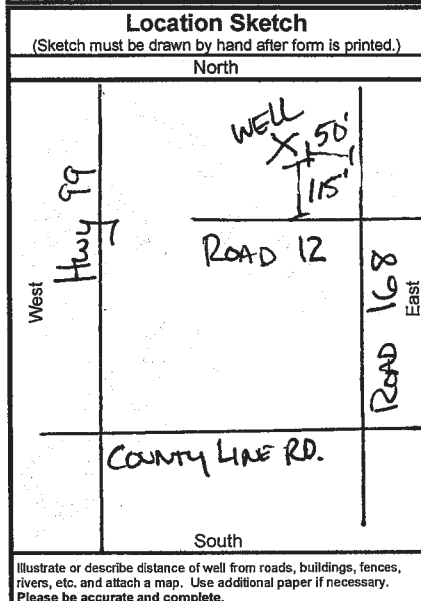
Permit Number 09-0120 Permit Date 3/9/09

DWR Use Only - Do Not Fill In	
24S126E-30	
State Well Number/Site Number	
Latitude	Longitude
APN/TRS/Other	

Geologic Log				
Orientation	<input checked="" type="radio"/> Vertical	<input type="radio"/> Horizontal	<input type="radio"/> Angle	Specify
Drilling Method	Reverse	Rotary	Drilling Fluid	Water
Depth from Surface		Description		
Feet	to Feet	Describe material, grain size, color, etc		
50	80	Sand Gravel		
80	120	Sand Gravel Clay		
120	160	Sand		
160	280	Sand Clay		
280	360	Sand Gravel		
360	470	Sand Gravel Clay		
470	500	Clay		
500	550	Sand Clay		
550	640	Sand Gravel Clay		
640	770	Sand Clay		
770	820	Sand Gravel Clay		
820	1,190	Clay Sand		
1190	1,290	Clay		
1290	1,330	Sand Clay		
1330	1,410	Clay		
Total Depth of Boring		1410	Feet	
Total Depth of Completed Well		1150	Feet	

Well Owner	
Name	Dhillon Farms
Mailing Address	15676 County Line Rd.
City	Delano State CA Zip 93292

Well Location	
Address	N / W corner of Ave 12, Rd. 168
City	Delano County Tulare
Latitude	Deg. Min. Sec. N Longitude Deg. Min. Sec. W
Datum	Decimal Lat. Decimal Long.
APN Book	338 Page 080 Parcel 018
Township	24 S Range 26 E Section 30



Activity	
<input checked="" type="radio"/> New Well	
<input type="radio"/> Modification/Repair	
<input type="radio"/> Deepen	
<input type="radio"/> Other	
<input type="radio"/> Destroy	
<small>Describe procedures and materials under "GEOLOGIC LOG"</small>	
Planned Uses	
<input checked="" type="radio"/> Water Supply	
<input type="checkbox"/> Domestic <input type="checkbox"/> Public	
<input checked="" type="checkbox"/> Irrigation <input type="checkbox"/> Industrial	
<input type="radio"/> Cathodic Protection	
<input type="radio"/> Dewatering	
<input type="radio"/> Heat Exchange	
<input type="radio"/> Injection	
<input type="radio"/> Monitoring	
<input type="radio"/> Remediation	
<input type="radio"/> Sparging	
<input type="radio"/> Test Well	
<input type="radio"/> Vapor Extraction	
<input type="radio"/> Other	

Water Level and Yield of Completed Well			
Depth to first water	223	(Feet below surface)	
Depth to Static			
Water Level	223	(Feet)	Date Measured 04/18/2009
Estimated Yield *	1,500	(GPM)	Test Type Constant Rate
Test Length	12.0	(Hours)	Total Drawdown 166 (Feet)
*May not be representative of a well's long term yield.			

Casings										Annular Material			
Depth from Surface	Borehole Diameter	Type	Material	Wall Thickness	Outside Diameter	Screen Type	Slot Size	Depth from Surface	Fill	Description			
Feet	to Feet	(Inches)		(Inches)	(Inches)		if Any (Inches)	Feet to Feet					
0	50	42	Conductor	A53Grade B	.312	30		0	50	Cement	Annular Seal		
0	530	26	Blank	A53Grade B	.312	16		0	1,170	Filter Pack	4x16 SRI		
530	600	26	Ful Flo	Ful Flo A139	.312	16	Louver	0.090	1,170	Fill	Backfill		
600	620	26	StandardFlo	SF A139	.312	16	Louver						
620	640	26	Ful Flo	Ful Flo A139	.312	16	Louver	0.090					
640	680	26	Standard Flo	SF A139	.312	16	Louver						

Attachments	
<input type="checkbox"/>	Geologic Log
<input type="checkbox"/>	Well Construction Diagram
<input type="checkbox"/>	Geophysical Log(s)
<input type="checkbox"/>	Soil/Water Chemical Analyses
<input type="checkbox"/>	Other
Attach additional information, if it exists.	

Certification Statement	
I, the undersigned, certify that this report is complete and accurate to the best of my knowledge and belief	
Name	Bakersfield Well & Pump Co.
Person, Firm or Corporation	
7212 Fruitvale Ave. N	Bakersfield CA 93308
Address	City State Zip
Signed	7/9/2009
C-57 Licensed Water Well Contractor	Date Signed 440537
	C-57 License Number

THE RESOURCES AGENCY

DEPARTMENT OF WATER RESOURCES
WATER WELL DRILLERS REPORT

No. 49066

29/29-16

State Well No. _____
Other Well No. _____

Office of Intent No. 159690
Local Permit No. or Date 5/20/82

1) OWNER: Name Superior Farming Company
Address P.O. Box 9999
Bakersfield, CA Zip 93389
2) LOCATION OF WELL (See instructions):
County Tulare Owner's Well Number 010-13A
Well address if different from above SW corner of the NW 1/4
Township 24S Range 24E Section 16
Distance from lines, roads, railroads, fences, etc. 3 3/4 miles west of
Earlimart, CA and 1 1/2 miles south of the
Alpaugh-Ducor Road; Avenue 56.

(12) WELL LOG: Total depth 1405 ft. Depth of completed well 1382 ft.

from ft.	to ft.	Formation (Describe by color, character, size or material)
0	50	Conductor
50	70	70% sand, 30% clay
70	80	50% sand, 50% clay
80	90	Sand
90	130	Brown Clay
130	170	80% sand, 20% sandy brown clay
170	190	Hard brown clay
190	210	90% brown clay 20% sand
210	220	50% clay, 50% sand
220	230	Soft brown clay
230	240	Sandy gray clay
240	250	90% sand, 10% clay
250	260	50% sandy gray clay, 50% sand
260	270	70% sandy gray clay, 30% sand
270	280	50% sandy gray clay, 50% sand
280	350	Gray clay
350	360	Gray sandy clay
360	390	70% sandy blue clay, 30% sand
390	400	60% sandy gray clay, 40% fine sand
400	410	Sandy gray clay
410	420	80% sandy gray clay, 20% sand
420	440	100% gray clay
440	480	100% soft blue clay
480	490	50% gray clay, 50% sand
490	500	70% gray clay, 30% sand
500	510	100% soft blue clay
510	520	Hard blue clay
520	530	50% sand, 50% blue clay
530	540	100% fine sand
540	550	100% clay
550	560	70% sand, 30% clay
560	570	50% sand, 50% blue & gray clay
570	600	100% sand
600	610	100% brown clay
610	620	100% sand
620	630	95% brown & blue clay, 5% sand
630	650	100% brown & blue clay
650	660	70% soft brown clay, 30% sand

(3) TYPE OF WORK:
 New Well Deepening
 Reconstruction
 Reconditioning
 Horizontal Well
 Destruction (Describe destruction materials and procedures in Item 12)

(4) PROPOSED USE:
 Domestic
 Irrigation
 Industrial
 Test Well
 Stock
 Municipal
 Other

WELL LOCATION SKETCH

7) EQUIPMENT:

Motor	XX	Gravel Pack	XX
Sub	XX	Subsidiary or line	28"
Other		Length	1400

8) CASING INSTALLED:

From ft.	To ft.	Dia. in.	Casing or Wall	From ft.	To ft.	Sleeve size
0	640	16	5/16	640	760	3/32
760	780	12	5/16	Reduction & comp. sect.		
		12	5/16	780	1382	3/32

(9) WELL SEAL:

Has surface secondary seal provided? Yes No If yes, to depth 50 ft.
 Vent pipe sealed against polluting? Yes No Interval 40 ft.
 Method of sealing Bentonite Pellets

(10) WATER LEVELS:

Depth of first water, if known Unknown ft.
 Standing level after well completion 207 ft.

(11) WELL TESTS:

Has well test made? Yes No If yes, by whom? Driller
 Type of test Pump Bailer Air lift
 Depth to water at start of test 207 ft. At end of test 241 ft.
 Discharge 2500 gal/min after 12 hours. Water temperature N/A
 Chemical analysis made? Yes No If yes, by whom?
 As electric log made? Yes No If yes, attach copy to this report

WELL DRILLER'S STATEMENT:
 This well was drilled under my jurisdiction and this report is true to the best of my knowledge and belief.

SIGNED: Layne C. Knoll (Well Driller)
 NAME: Layne-Western Company, Inc.
 Address: P.O. Box 3216
 City: Bakersfield, CA Zip: 93385
 License No. 407409 Date of this report: July 6, 1982

TRIPPLICATE
Owner's Copy

STATE OF CALIFORNIA
WELL COMPLETION REPORT
Refer to Instruction Pamphlet

DWR USE ONLY - DO NOT FILL IN

Page of

Owner's Well No. 18E

No. **489856**

Date Work Began 7-15-91, Ended 7-17-91

Local Permit Agency Tulare

Permit No. 2 369745 Permit Date 7-12-91

STATE WELL NO./STATION NO.	
LATITUDE	LONGITUDE
APN/TRS/OTHER	

ORIENTATION (\angle) VERTICAL HORIZONTAL ANGLE (SPECIFY)
DEPTH TO FIRST WATER _____ (Ft.) BELOW SURFACE

WELL OWNER
Name Angiola Water Dist.
Mailing Address 10015 Yucca, 10015 Utica Ave.
CITY Corcoran, CA STATE _____ ZIP _____

DEPTH FROM SURFACE		DESCRIPTION <i>Describe material, grain size, color, etc.</i>
Ft.	to Ft.	
0	4	Top Soil
4	9	clay
9	15	sand
15	21	clay
21	37	sand
37	39	clay
39	42	sand
42	63	clay
63	74	sand
74	85	clay
85	91	sand
91	97	clay
97	101	sand
101	105	clay
105	125	sand
125	131	clay
131	142	sand
142	176	clay
176	196	sand
196	222	clay
222	228	sand
228	244	clay
244	250	sand
250	256	clay
256	262	sand
262	270	clay
270	274	sand
274	277	clay
277	281	sand
281	294	clay
294	298	sand
298	301	clay
301	310	sand
310	316	clay
316	336	sand
336	347	clay
347	355	sand
355	400	clay
400	408	sand
408	411	clay
411	426	sand
426	431	clay
431	435	sand
435	440	clay
440	452	sand
452	669	clay
669	716	sand
716	722	clay
722	731	sand
731	747	clay
747	765	sand
765	771	clay
771	775	sands
775	800	clay
800	807	sand
807	820	clay
820	825	sand
825	830	clay
830	852	sand
852	863	clay
863	868	clay

TOTAL DEPTH OF BORING 960 (Feet)
TOTAL DEPTH OF COMPLETED WELL 930 (Feet)

WELL LOCATION
Address Ave 112 1/2 mi W of Rd 56-200 ft S.
City Corcoran
County Tulare
APN Book Echoe Page 78 Parcel 233-240-03
Township 22S Range 23 E Section 26
Latitude _____ Longitude _____
DEG. MIN. SEC. DEG. MIN. SEC.

LOCATION SKETCH NORTH _____ SOUTH _____
WEST _____ EAST _____

ACTIVITY (\angle)
 NEW WELL
MODIFICATION/REPAIR
___ Deepen
___ Other (Specify) _____

___ DESTROY (Describe Procedures and Materials Under "GEOLOGIC LOG")
PLANNED USE(S) (\angle)
___ MONITORING
WATER SUPPLY
___ Domestic
___ Public
 Irrigation
___ Industrial
___ "TEST WELL"
___ CATHODIC PROTECTION
___ OTHER (Specify) _____

Illustrate or Describe Distance of Well from Landmarks such as Roads, Buildings, Fences, Rivers, etc.
PLEASE BE ACCURATE & COMPLETE.

DRILLING METHOD Reverse FLUID Natural
WATER LEVEL & YIELD OF COMPLETED WELL
DEPTH OF STATIC WATER LEVEL _____ (Ft.) & DATE MEASURED _____
ESTIMATED YIELD* _____ (GPM) & TEST TYPE _____
TEST LENGTH _____ (Hrs.) TOTAL DRAWDOWN _____ (Ft.)
* May not be representative of a well's long-term yield.

DEPTH FROM SURFACE Ft. to Ft.	BORE-HOLE DIA. (Inches)	CASING(S)					ANNULAR MATERIAL					
		TYPE (\angle)				MATERIAL/ GRADE	INTERNAL DIAMETER (Inches)	GAUGE OR WALL THICKNESS	SLOT SIZE IF ANY (Inches)	TYPE		
Blank	Screen	Conductor	Fill Pipe									CEMENT (\angle)
0-50	38			X		steel	30	1/4				Conductor
0-560	30	X				steel	16	5/16				5/16x4
560-580	30					Compression section	18/16	5/16				Tablets
580-930	30	X				louver	16	5/16	.070			5/16x4

- ATTACHMENTS (\angle)
- ___ Geologic Log
 - ___ Well Construction Diagram
 - ___ Geophysical Log(s)
 - ___ Soil/Water Chemical Analyses
 - ___ Other _____
- ATTACH ADDITIONAL INFORMATION, IF IT EXISTS.

CERTIFICATION STATEMENT

I, the undersigned, certify that this report is complete and accurate to the best of my knowledge and belief.

NAME Grabow Well Drilling Inc.
(PERSON OR FIRM OR CORPORATION) (PARTNER OR EMPLOYEE)

ADDRESS 12522 9th Ave. Hanford, CA 93230 CITY _____ STATE _____ ZIP _____

Signed _____ DATE SIGNED 8-1-91 289499 C-57 LICENSE NUMBER

Page _____ of _____
Owner's Well No. **18E Continued**
Date Work Began _____, Ended _____
Local Permit Agency _____
Permit No. _____ Permit Date _____

No. **489857**

DWR USE ONLY - DO NOT FILL IN

STATE WELL NO./STATION NO. _____

LATITUDE _____ LONGITUDE _____

APN/TRS/OTHER _____

GEOLOGIC LOG

WELL OWNER

ORIENTATION (∠) _____ VERTICAL _____ HORIZONTAL _____ ANGLE _____ (SPECIFY)

Name **Angiola Water Dist (continued)**

DEPTH TO FIRST WATER _____ (Ft.) BELOW SURFACE

Mailing Address _____

DEPTH FROM SURFACE	
Ft.	to Ft.

DESCRIPTION

Describe material, grain size, color, etc.

CITY _____ STATE _____ ZIP _____

Ft.	to Ft.	DESCRIPTION
863	868	sand
868	874	clay
874	879	sand
879	890	clay
890	902	sand
902	912	clay
912	920	sand
920	930	clay
930	938	sand
938	960	clay

WELL LOCATION

Address _____

City _____

County _____

APN Book _____ Page _____ Parcel _____

Township _____ Range _____ Section _____

Latitude _____ NORTH Longitude _____ WEST

DEG. MIN. SEC. DEG. MIN. SEC.

LOCATION SKETCH

ACTIVITY (∠)

WEST _____ NORTH _____ SOUTH _____

Illustrate or Describe Distance of Well from Landmarks such as Roads, Buildings, Fences, Rivers, etc.
PLEASE BE ACCURATE & COMPLETE.

NEW WELL

MODIFICATION/REPAIR

___ Deepen

___ Other (Specify) _____

DESTROY (Describe Procedures and Materials Under "GEOLOGIC LOG")

PLANNED USE(S)

(∠)

___ MONITORING

WATER SUPPLY

___ Domestic

___ Public

___ Irrigation

___ Industrial

___ "TEST WELL"

___ CATHODIC PROTECTION

___ OTHER (Specify) _____

DRILLING METHOD _____ FLUID _____

WATER LEVEL & YIELD OF COMPLETED WELL

DEPTH OF STATIC WATER LEVEL _____ (Ft.) & DATE MEASURED _____

ESTIMATED YIELD* _____ (GPM) & TEST TYPE _____

TEST LENGTH _____ (Hrs.) TOTAL DRAWDOWN _____ (Ft.)

* May not be representative of a well's long-term yield.

TOTAL DEPTH OF BORING _____ (Feet)

TOTAL DEPTH OF COMPLETED WELL _____ (Feet)

DEPTH FROM SURFACE	BORE-HOLE DIA. (Inches)	CASING(S)					MATERIAL / GRADE	INTERNAL DIAMETER (Inches)	GAUGE OR WALL THICKNESS	SLOT SIZE IF ANY (Inches)	DEPTH FROM SURFACE	ANNULAR MATERIAL			
		TYPE (∠)	CE-MENT (∠)	BEN-TONITE (∠)	FILL (∠)	FILTER PACK (TYPE/SIZE)									
Ft.	to Ft.	BLANK	SCREEN	CON-DUCTOR	FILL PIPE					Ft.	to Ft.				

ATTACHMENTS (∠)

- ___ Geologic Log
- ___ Well Construction Diagram
- ___ Geophysical Log(s)
- ___ Soil/Water Chemical Analyses
- ___ Other _____

ATTACH ADDITIONAL INFORMATION, IF IT EXISTS.

CERTIFICATION STATEMENT

I, the undersigned, certify that this report is complete and accurate to the best of my knowledge and belief.

NAME _____ (PERSON, FIRM, OR CORPORATION) (TYPED OR PRINTED),

ADDRESS _____ CITY _____ STATE _____ ZIP _____

Signed Debra E. Anderson DATE SIGNED _____ C-57 LICENSE NUMBER _____

22/23-23

CAL 17-54

U. S. DEPARTMENT OF THE INTERIOR
GEOLOGICAL SURVEY
WATER RESOURCES DIVISION

WELL SCHEDULE

CALIFORNIA

AREA: Palmdale

DATE: 12-11, 1957 Well No. 22/23-2341

Record by R. L. B. ... Other No. South Hill H 145

Source of data ... Other No. ...

1. Location: Map ... Photo 5-4522a

2. Owner South Hill Farms Address ...

Former owner ... Tenant ...

Driller ... Address ...

3. Topography Plain ; MP ... ft.

4. Altitude: Lsd 211 ft; how obtained ... ; MP ... ft.

5. Type: Dug, cable, rotary, auger, jet ... ; Finish ...

6. Depth: Rept. 178 1/2 ft; Meas. ... ft; Obstruction ... ft.

7. Casing: Diam. 1 1/2 in. to 5 1/2 ft; 12 in. to 17 1/2 ft. Type ...

Perforations ...

8. Aquifers ... Act 9, 1958

9. Water level 120.05 ft. Slidg: rept 12-11 1957 above 7.5 ft. Oil ... below ... ft. which is 1.0 ft above Lsd

Access on North side

10. Pump: Type ...; Dischg diam 10 in; length 25 ft

Power W S E 1100; HP 100; Meter No. 370917

11. Yield: Flow ... gpm; pump ... epm, meas, rept, est.

Drawdown ... ft after ... min pumpg. Specific cap. ... hrs

12. Use: Dom, Stock, PS, IRI, Ind, Irr, Obs, Destroyed, Unused, Test, ...

13. Quality ... Temp ... °F

Taste, odor, color ... Sampled ... 19...

14. Other data: log, analysis, water levels, electric log ...

15. Remarks: ...

Well No. 22/23-2341

AE

PLOTTED
FEB 1970

Well No. 22/23-2341

Location: ...

0.45 ft north and 90 ft west of SE corner sec. 33 mile

Remarks: ...

10-70 fld. chd. DTW-138' PERMISSION TO MEASURE PER FOR. WORKING LAND, WHO VERIFIED DEPTH, PERFS & APPROX. DATE DRILLED T.

motor *
1012417

24/24-4

LOCATION NOT CHECKED

DUPLICATE
File Original, Duplicate and Triplicate with the
REGIONAL WATER POLLUTION
CONTROL BOARD No. 5
(insert appropriate number)

WATER WELL DRILLERS REPORT
(Sections 7076, 7077, 7078, Water Code)

Do Not Fill In
No. 63276 4E2
State Well No. _____
Other Well No. 245/24E-4

STATE OF CALIFORNIA

2427

(1) OWNER:
Name John W. Oglesby
Address 516 West 4th.
Arvin, California

(2) LOCATION OF WELL:
County Tulare Owner's number, if any—
R. F. D. or Street No.
1/2 mile North of the town of
Allensworth and 300 ft. West of
Santa Fe Railway tracks.

(3) TYPE OF WORK (check):
New well Deepening Reconditioning Abandon
If abandonment, describe material and procedure in Item 11.

(4) PROPOSED USE (check):
Domestic Industrial Municipal
Irrigation Test Well Other
(5) EQUIPMENT:
Rotary
Cable
Dug Well

(6) CASING INSTALLED:
SINGLE DOUBLE
From ft. to ft. 1 1/2" diam. 1/4" wall
Top to 1,200 ft.
If gravel packed
Diameter of Bore 26" from ft. to ft.
Top to bottom
Type and size of shoe or well ring
Describe joint Butt welded
Size of gravel: 3/8"

(7) PERFORATIONS:
Type of perforator used Machine
Size of perforations 1/8 x 1 cc in., length, by in.
From ft. to ft. 798 ft. to 1,200 ft. 4 Perf. per row 18 Rows per ft.

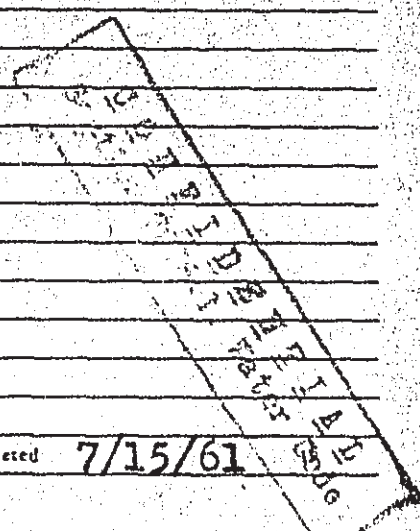
(8) CONSTRUCTION:
Was a surface sanitary seal provided? Yes No To what depth _____ ft.
Were any strata sealed against pollution? Yes No If yes, note depth of strata
From _____ ft. to _____ ft.
Method of Sealing _____

(9) WATER LEVELS:
Depth at which water was first found Unknown ft.
Standing level before perforating _____ ft.
Standing level after perforating _____ ft.

(10) WELL TESTS:
Was a pump test made? Yes No If yes, by whom?
Yield: _____ gal./min. with _____ ft. draw down after _____ hrs.
Temperature of water _____ Was a chemical analysis made? Yes No
Was electric log made of well? Yes No

(11) WELL LOG:
Total depth 1,200 ft. Depth of completed well 1,200 ft.
Formation: Describe by color, character, size of material, and structure.
0 to 35 Sandy Clay Top Soil
35 to 218 Clay
218 to 300 Sandy Clay
300 to 369 Clay
369 to 482 Shale
482 to 487 Sand
487 to 610 Clay
610 to 616 Hard Clay
616 to 630 Sandy Clay
630 to 638 Hard Clay
638 to 787 Clay
787 to 813 Shale
813 to 935 Clay
935 to 995 Sandy Clay
995 to 1015 Clay
1015 to 1025 Sand
1025 to 1089 Clay
1089 to 1104 Hard Shale
1104 to 1178 Clay
1178 to 1200 Shale

DTW = 166 - 11-5-70 JD



Work started 6/27/61 19 _____ Completed 7/15/61 19 _____

WELL DRILLER'S STATEMENT:
This well was drilled under my jurisdiction and this report is true to the best of my knowledge and belief.
NAME Whitten Pumps, Inc. (Typed or printed)
Address 1744 High Street
Delano, California
[SIGNED] [Signature] Well Driller
License No. 148282 Dated January 31, 19 62

24/23-31N1

ORIGINAL
File Original, Duplicate and Triplicate with the
REGIONAL WATER POLLUTION
CONTROL BOARD No. _____
(Insert appropriate number)

WATER WELL DRILLERS REPORT
(Sections 7076, 7077, 7078, Water Code)
THE RESOURCES AGENCY OF CALIFORNIA

Do Not Fill In
No. 118716

State Well No. _____
Other Well No. 245/23E-31N1

(1) OWNER:

Name Westgate Calif. Realty Co.
Address 1021 Sub. Term. Bldg.
417 S. Hill, Los Angeles, California

(2) LOCATION OF WELL:

County Tulare Owner's number, if any-- #20
R. F. D. or Street No.
SW Corner S 31, T24 S, R23 E

65' N & 85' E / 0 SW Cor.

(3) TYPE OF WORK (check):

New well Deepening Reconditioning Abandon
If abandonment, describe material and procedure in Item 11.

(4) PROPOSED USE (check):

Domestic Industrial Municipal
Irrigation Test Well Other

(5) EQUIPMENT:

Rotary
Cable
Dug Well

(6) CASING INSTALLED:

SINGLE DOUBLE
From 0 ft. to 1190 ft. 14" OD 1/4 Gage or Wall Diameter of Bore 25 1/2 ft. to 1190 ft. top to bottom
If gravel packed
Size of gravel: 1/4
Type and size of shoe or well ring
Describe joint Collared with fillet weld

(7) PERFORATIONS:

Type of perforator used Machine
Size of perforations .100" X 2 in., length, by 600 in.
From 490 ft. to 1190 ft. 2 Perf. per row 14 Rows per ft.

(8) CONSTRUCTION:

Was a surface sanitary seal provided? Yes No To what depth _____ ft.
Were any strata sealed against pollution? Yes No If yes, note depth of strata _____
From _____ ft. to _____ ft.
Method of Sealing _____

(9) WATER LEVELS:

Depth at which water was first found Unknown ft.
Standing level before perforating _____ ft.
Standing level after perforating _____ ft.

(10) WELL TESTS:

Was a pump test made? Yes No If yes, by whom?
Yield: _____ gal./min. with _____ ft. draw down after _____ hrs.
Temperature of water _____ Was a chemical analysis made? Yes No
Was electric log made of well? Yes No

(11) WELL LOG:

Total depth	ft.	Depth of completed well	ft.	Formation: Describe by color, character, size of material, and structure.
0	ft. to 4	ft.		top soil
4	" 92	"		sandy clay
92	" 304	"		sandy clay
304	" 680	"		sandy clay
680	" 684	"		sand
684	" 723	"		sandy clay
723	" 843	"		Sandy clay
843	" 873	"		clay
873	" 934	"		sandy clay
934	" 1055	"		hard shale
1055	" 1186	"		hard clay
1186	" 1190	"		hard shale

PRM 10/70 292' TS + JD

C. Clay = 381'

CONFIDENTIAL
Water Code Sec. 7060

Work started Sept. 7 19 66. Completed Sept. 19 19 66

WELL DRILLER'S STATEMENT:

This well was drilled under my jurisdiction and this report is true to the best of my knowledge and belief.

NAME Whitten Pumps, Inc. (Person, firm, or corporation) (Typed or printed)

Address 1744 Inyo Street
Delano, California

[SIGNED] [Signature] Well Driller
License No. 148282 Dated November 18, 19 66

24/23 22R2

ORIGINAL
File Original, Duplicate and Triplicate with the
REGIONAL WATER POLLUTION

WATER WELL DRILLERS REPORT

(Sections 7076, 7077, 7078, Water Code)

Do Not Fill In
No. 116291

CONTROL BOARD No. _____
(Insert appropriate number)

THE RESOURCES AGENCY OF CALIFORNIA

State Well No. 22R2
Other Well No. 24^S/23^E-22

(1) OWNER:

Name Alpaugh Irrigation District
Address P. O. Box 127
Alpaugh, California

(2) LOCATION OF WELL:

County Tulare Owner's number, if any—
R. F. D. or Street No. _____
Southeast corner sec 22
township 24S Range 23E
220' N of 75' N/O SE COR.

(3) TYPE OF WORK (check):

New well Deepening Reconditioning Abandon
If abandonment, describe material and procedure in Item 11.

(4) PROPOSED USE (check):

Domestic Industrial Municipal
Irrigation Test Well Other

(5) EQUIPMENT:

Rotary
Cable
Dug Well

(6) CASING INSTALLED:

SINGLE <input checked="" type="checkbox"/> DOUBLE <input type="checkbox"/>		Gage or Wall		Diameter of Bore		If gravel packed	
From	to	ft.	Diam.	ft.	ft.	ft.	ft.
0	500	16	1/4	25 1/2	from	to	
500	1200	14	1/4		top to bottom		
Type and size of shoe or well ring				Size of gravel:			
Describe joint <u>collared w/ fillet weld</u>							

(7) PERFORATIONS:

Type of perforator used	Size of perforations	in.	length, by	in.
machine	.100 x 2	6cc		
From 500 to 1200	ft. 2	Perf. per row	14	Rows per ft.
"	"	"	"	"
"	"	"	"	"
"	"	"	"	"
"	"	"	"	"

CAUTION:

Provided? Yes No To what depth _____ ft.
If yes, note depth of strata _____ ft.

(11) WELL LOG:

Total depth	ft.	Depth of completed well	ft.
1205		1205	
Formation: Describe by color, character, size of material, and structure.			
0	ft. to	4	ft. top soil
4	"	35	" sandy clay
35	"	78	" sandy clay
78	"	121	" sandy clay
121	"	329	" sandy clay
329	"	540	" sandy clay
540	"	664	" blue clay
664	"	874	" clay hard
874	"	900	" sandy clay
900	"	904	" sand
904	"	934	" clay
934	"	1058	" shale & clay
1058	"	1146	" hard shale
1146	"	1205	" blue sand

DTW = 244' 10/30/70 TS+JD

CONFIDENTIAL
Water Code Sec. 13752

Work started 10/31/66 Completed 11/14/66

WELL DRILLER'S STATEMENT:

This well was drilled under my jurisdiction and this report is true to the best of my knowledge and belief.

NAME Whitten Pumps, Inc.
(Person, firm, or corporation) (Typed or printed)
Address 1744 Inyo Street
Delano, California

[SIGNED] [Signature] Well Driller
License No. 148282 Dated 4/22/67, 19__

RECEIVED
SAN JOSE
APR 1967

24/23 22R2

ORIGINAL
File Original, Duplicate and Triplicate with the
REGIONAL WATER POLLUTION
CONTROL BOARD No. _____
(Insert appropriate number)

WATER WELL DRILLERS REPORT
(Sections 7076, 7077, 7078, Water Code)

Do Not Fill In
No. 116291

THE RESOURCES AGENCY OF CALIFORNIA

State Well No. 22R2
Other Well No. 245/23E-22

(1) OWNER:

Name Alpaugh Irrigation District
Address P. O. Box 127
Alpaugh, California

(2) LOCATION OF WELL:

County Tulare Owner's number, if any—
R. F. D. or Street No.
Southeast corner sec 22 23E 23E
township 24S Range 23E
220' N 75' N / O SE COR.

(3) TYPE OF WORK (check):

New well Deepening Reconditioning Abandon
If abandonment, describe material and procedure in Item 11.

(4) PROPOSED USE (check):

Domestic Industrial Municipal
Irrigation Test Well Other

(5) EQUIPMENT:

Rotary
Cable
Dug Well

(6) CASING INSTALLED:

SINGLE DOUBLE
From 0 ft. to 500 ft. Diam. 16" Gage or Wall 1/4"
500 " 1200 " 14 " 1/4 " top to bottom
16" OD to 14" OD
"Transition" Joint Slip jt.
Type and size of shoe or well ring Describe joint collared w/ fillet weld
If gravel packed Diameter of Bore 25 1/2 ft. to ft. Size of gravel:

(7) PERFORATIONS:

Type of perforator used machine
Size of perforations .100 x 2 in., length, by 6cc in.
From 500 ft. to 1200 ft. 2 Perf. per row 1 1/2 Rows per ft.

(8) CONSTRUCTION:

Was a surface sanitary seal provided? Yes No To what depth ft.
Were any strata sealed against pollution? Yes No If yes, note depth of strata
From ft. to ft.
Method of Sealing

(9) WATER LEVELS:

Depth at which water was first found unknown ft.
Standing level before perforating ft.
Standing level after perforating ft.

(10) WELL TESTS:

Was a pump test made? Yes No If yes, by whom?
Yield: gal./min. with ft. draw down after hrs.
Temperature of water Was a chemical analysis made? Yes No
Was electric log made of well? Yes No

(11) WELL LOG:

Total depth 1205 ft. Depth of completed well 1205 ft.
Formation: Describe by color, character, size of material, and structure.
0 ft. to 4 ft. top soil
4 " 35" sandy clay
35 " 78" sandy clay
78 " 121" sandy clay
121 " 329" sandy clay
329 " 540" sandy clay
540 " 664" blue clay
664 " 874" clay hard
874 " 900" sandy clay
900 " 904" sand
904 " 934" clay
934 " 1058" shale & clay
1058 " 1146" hard shale
1146 " 1205" blue sand

DTW = 244' 10/30/70 TS+JU

CONFIDENTIAL
Water Code Sec. 13753

Work started 10/31/66 19 Completed 11/14/66 19

WELL DRILLER'S STATEMENT:

This well was drilled under my jurisdiction and this report is true to the best of my knowledge and belief.

NAME Whitten Pumps, Inc.
(Person, firm, or corporation) (Typed or printed)
Address 174 1/2 Inyo Street
Delano, California

[SIGNED] *W. Whitten* Well Driller
License No. 148282 Dated 4/22/67 19

STATE OF CALIFORNIA
WELL COMPLETION REPORT
Refer to Instruction Pamphlet

DWR USE ONLY - DO NOT FILL IN

22S/23E-22 / 3

STATE WELL NO./ STATION NO.

LATITUDE LONGITUDE

APN/TRS/OTHER

Owner's Well No. 8104

No. **E072308**

Date Work Began 1/28/2008, Ended 2/1/2008

Local Permit Agency TULARE COUNTY HEALTH DEPT

Permit No. 07-0141 Permit Date 4/9/2007

GEOLOGIC LOG

ORIENTATION (✓)		DRILLING METHOD	FLUID WATER
<input checked="" type="checkbox"/> VERTICAL <input type="checkbox"/> HORIZONTAL <input type="checkbox"/> ANGLE _____ (SPECIFY)		<u>REVERSE</u>	<u>FLUID WATER</u>
DEPTH FROM SURFACE		DESCRIPTION	
Ft.	to Ft.	Describe material, grain, size, color, etc.	
0	5	CLAY TOP SOIL	
5	8	COARSE SAND	
8	12	SILTY BROWN CLAY	
12	16	COARSE SAND	
16	95	SILTY BROWN CLAY	
95	175	SILTY TAN CLAY WITH SAND	
175	285	SILTY BLUE GRAY CLAY WITH SAND	
285	350	SAND WITH SILTY BLUE GRAY CLAY STREAKS	
350	365	SILTY BLUE GRAY CLAY	
365	420	SAND WITH SILTY BLUE GRAY CLAY STREAKS	
420	435	SILTY BLUE GRAY CLAY	
435	458	SAND	
458	500	SILTY BLUE GRAY CLAY	
500	630	SOFT BLUE GRAY CLAY	
630	685	SAND WITH SILTY BLUE GRAY CLAY STREAKS	
685	740	SAND	
740	745	BLUE GRAY CLAY	
745	810	SAND	
810	865	SAND WITH BRITTLE BLUE GRAY CLAY STREAKS	
865	940	BLUE GRAY CLAY WITH SAND STREAKS	
940	995	SAND WITH BRITTLE BLUE GRAY CLAY STREAKS	
995	1035	SAND	
1035	1055	BLUE GRAY CLAY	
1055	1140	BLUE GRAY CLAY WITH SAND STREAKS	
1140	1196	SAND	
1196	1205	BLUE GRAY CLAY	
TOTAL DEPTH OF BORING <u>1090</u> (Feet)			
TOTAL DEPTH OF COMPLETED WELL <u>1050</u> (Feet)			

WELL OWNER

Name ANGIOLA WATER DISTRICT

Mailing Address 944 WHITLEY AVE
CORCORAN CA 93212

CITY STATE ZIP

WELL LOCATION

Address .15 MI NOF AVE 112 & 250 WOF HWY 43

City CA

County TULARE

APN Book 291 Page 070 Parcel 010

Township 22 S Range 23 E Section 22

Latitude _____

DEG. MIN. SEC. LOCATION SKETCH NORTH

DEG. MIN. SEC. ACTIVITY (✓)

NEW WELL

MODIFICATION/REPAIR
 Deepen
 Other (Specify) _____

DESTROY (Describe Procedures and Materials Under "GEOLOGIC LOG")

PLANNED USES (✓)

WATER SUPPLY
 Domestic Public
 Irrigation Industrial

MONITORING

TEST WELL

CATHODIC PROTECTION

HEAT EXCHANGE

DIRECT PUSH

INJECTION

VAPOR EXTRACTION

SPARGING

REMEDIATION

OTHER (SPECIFY) _____

WEST EAST

_____ SOUTH _____

Illustrate or Describe Distance of Well from Roads, Buildings, Fences, Rivers, etc. and attach a map. Use additional paper if necessary. PLEASE BE ACCURATE & COMPLETE.

WATER LEVEL & YIELD OF COMPLETED WELL

DEPTH TO FIRST WATER _____ (Ft.) BELOW SURFACE

DEPTH OF STATIC WATER LEVEL 320 (Ft.) & DATE MEASURED 4/19/2008

ESTIMATED YIELD * 1000 (GPM) & TEST TYPE _____

TEST LENGTH _____ (Hrs.) TOTAL DRAWDOWN 30 (Ft.)

May not be representative of a well's long-term yield.

DEPTH FROM SURFACE	BORE-HOLE DIA. (Inches)	CASING (S)					DEPTH FROM SURFACE	ANNULAR MATERIAL					
		TYPE (✓)				MATERIAL / GRADE		INTERNAL DIAMETER (Inches)	GAUGE OR WALL THICKNESS	SLOT SIZE IF ANY (Inches)	TYPE		
Ft.	to Ft.	BLANK	SCREEN	CON-DUCTOR	FILL PIPE		Ft.				to Ft.	CE-MENT (✓)	BEN-TONITE (✓)
0	360	28				ACCESS TB	2	SCH 40				SAND SLURRY	
0	400	28	✓			ASTM-135	16	.312			✓	SRI#8 SAND	
400	510	28	✓			ASTM-135	16	.375					
510	520	28				COMP SEC	16						
520	670	28	✓			ASTM-135	16	.312					
670	850	28	✓			DBL MILLSL	16	.312	.060				

ATTACHMENTS (✓)

- Geologic Log
- Well Construction Diagram
- Geophysical Log(s)
- Soil/Water Chemical Analysis
- Other _____

ATTACH ADDITIONAL INFORMATION, IF IT EXISTS.

CERTIFICATION STATEMENT

I, the undersigned, certify that this report is complete and accurate to the best of my knowledge and belief.

NAME EATON DRILLING CO.
(PERSON, FIRM, OR CORPORATION) (TYPED OR PRINTED)

20 WEST KENTUCKY AVE WOODLAND CA 95695
ADDRESS CITY STATE ZIP

Signed [Signature] DATE SIGNED 04/29/08 C57 A HIC - 13378
WELL DRILLER/AUTHORIZED REPRESENTATIVE DATE SIGNED C-57 LICENSE NUMBER

Owner's Well No. 8104

Date Work Began 1/28/2008, Ended 2/1/2008

Local Permit Agency TULARE COUNTY HEALTH DEPT

Permit No. 07-0141 Permit Date 4/9/2007

STATE OF CALIFORNIA
WELL COMPLETION REPORT
Refer to Instruction Pamphlet

No. **E072308**

DWR USE ONLY -- DO NOT FILL IN

22S/23E-22 13

STATE WELL NO./STATION NO.

LATITUDE LONGITUDE

APN/TRS/OTHER

GEOLOGIC LOG

WELL OWNER

ORIENTATION (✓)		DRILLING METHOD	FLUID	WATER
<input checked="" type="checkbox"/> VERTICAL <input type="checkbox"/> HORIZONTAL <input type="checkbox"/> ANGLE _____ (SPECIFY)		REVERSE		
DEPTH FROM SURFACE		DESCRIPTION		
Ft.	to Ft.	Describe material, grain, size, color, etc.		
0	5	CLAY TOP SOIL		
5	8	COARSE SAND		
8	12	SILTY BROWN CLAY		
12	16	COARSE SAND		
16	95	SILTY BROWN CLAY		
95	175	SILTY TAN CLAY WITH SAND		
175	285	SILTY BLUE GRAY CLAY WITH SAND		
285	350	SAND WITH SILTY BLUE GRAY CLAY STREAKS		
350	365	SILTY BLUE GRAY CLAY		
365	420	SAND WITH SILTY BLUE GRAY CLAY STREAKS		
420	435	SILTY BLUE GRAY CLAY		
435	458	SAND		
458	500	SILTY BLUE GRAY CLAY		
500	630	SOFT BLUE GRAY CLAY		
630	685	SAND WITH SILTY BLUE GRAY CLAY STREAKS		
685	740	SAND		
740	745	BLUE GRAY CLAY		
745	810	SAND		
810	865	SAND WITH BRITTLE BLUE GRAY CLAY STREAKS		
865	940	BLUE GRAY CLAY WITH SAND STREAKS		
940	995	SAND WITH BRITTLE BLUE GRAY CLAY STREAKS		
995	1035	SAND		
1035	1055	BLUE GRAY CLAY		
1055	1140	BLUE GRAY CLAY WITH SAND STREAKS		
1140	1196	SAND		
1196	1205	BLUE GRAY CLAY		
TOTAL DEPTH OF BORING 1090 (Feet)				
TOTAL DEPTH OF COMPLETED WELL 1050 (Feet)				

Name ANGIOLA WATER DISTRICT

Mailing Address 944 WHITLEY AVE
CORCORAN CA 93212

CITY STATE ZIP

WELL LOCATION

Address .15 MI NOF AVE 112 & 250' WOF HWY 43

City CA

County TULARE

APN Book 291 Page 070 Parcel 010

Township 22 S Range 23 E Section 22

Latitude _____

LOCATION SKETCH

NORTH

WEST EAST

SOUTH

Illustrate or Describe Distance of Well from Roads, Buildings, Fences, Rivers, etc. and attach a map. Use additional paper if necessary. PLEASE BE ACCURATE & COMPLETE.

ACTIVITY (✓)

NEW WELL

MODIFICATION/REPAIR

Deepen

Other (Specify) _____

DESTROY (Describe Procedures and Materials Under "GEOLOGIC LOG")

PLANNED USES (✓)

WATER SUPPLY

Domestic Public

Irrigation Industrial

MONITORING

TEST WELL

CATHODIC PROTECTION

HEAT EXCHANGE

DIRECT PUSH

INJECTION

VAPOR EXTRACTION

SPARGING

REMIEDIATION

OTHER (SPECIFY) _____

WATER LEVEL & YIELD OF COMPLETED WELL

DEPTH TO FIRST WATER _____ (Ft.) BELOW SURFACE

DEPTH OF STATIC WATER LEVEL 320 (Ft.) & DATE MEASURED 4/19/2008

ESTIMATED YIELD * 1000 (GPM) & TEST TYPE _____

TEST LENGTH _____ (Hrs.) TOTAL DRAWDOWN 30 (Ft.)

May not be representative of a well's long-term yield.

DEPTH FROM SURFACE	BORE-HOLE DIA. (Inches)	CASING (S)				MATERIAL / GRADE	INTERNAL DIAMETER (Inches)	GAUGE OR WALL THICKNESS	SLOT SIZE IF ANY (Inches)
		TYPE (✓)	BLANK	SCREEN	CON-DUCTOR				
850	940	28	✓			ASTM-135	16	.312	
940	960	28	✓			DBL MILLSL	16	.312	.060
960	990	28	✓			ASTM-135	16	.312	
990	1030	28	✓			DBL MILLSL	16	.312	.060
1030	1050	28	✓			ASTM-135	16	.312	

DEPTH FROM SURFACE	ANNULAR MATERIAL				
	TYPE				
Ft. to Ft.	CE-MENT (✓)	BEN-TONITE (✓)	FILL (✓)	FILTER PACK (TYPE/SIZE)	
0	480	✓			SAND SLURRY
480	1090			✓	SRI#8 SAND

- ATTACHMENTS (✓)**
- Geologic Log
 - Well Construction Diagram
 - Geophysical Log(s)
 - Soil/Water Chemical Analysis
 - Other _____
- ATTACH ADDITIONAL INFORMATION, IF IT EXISTS.

CERTIFICATION STATEMENT

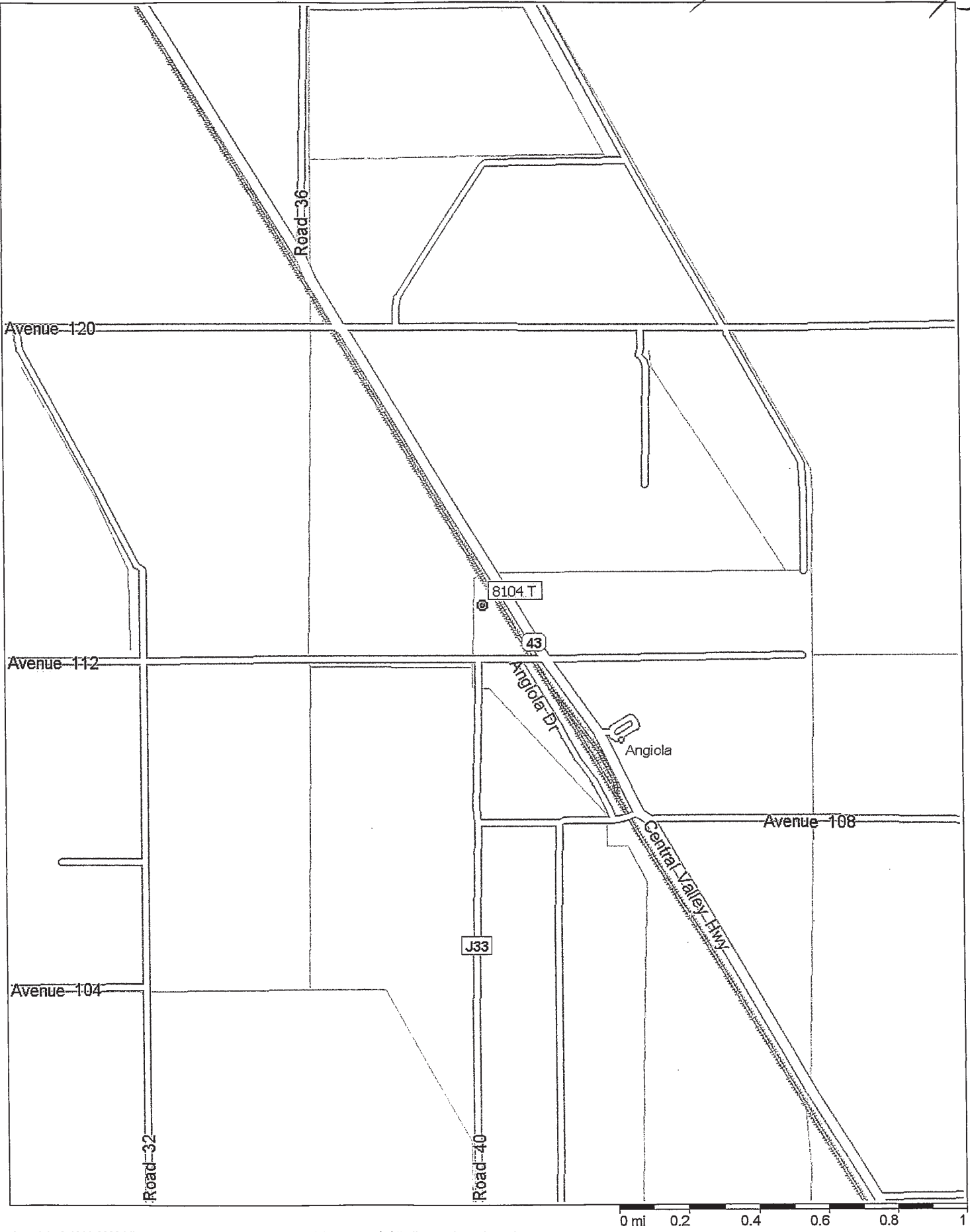
I, the undersigned, certify that this report is complete and accurate to the best of my knowledge and belief.

NAME EATON DRILLING CO.
(PERSON, FIRM, OR CORPORATION) (TYPED OR PRINTED)

20 WEST KENTUCKY AVE WOODLAND CA 95695
ADDRESS CITY STATE ZIP

Signed Mark Damion DATE SIGNED 04/29/08 C57 A HIC - 13378
WELL DRILLER/AUTHORIZED REPRESENTATIVE DATE SIGNED C-57 LICENSE NUMBER

22S/23E-22 3/3



W16

File Original with DWR

STATE OF CALIFORNIA WELL COMPLETION REPORT

DWR USE ONLY DC NOT FILL IN

Page 1 of 1

Owner's Well No. Well #16 or Layne Well #2

No. e077033

Date Work Began 5/8/08 Ended _____

Local Permit Agency Tulare County Env Health Services Div

Permit No. 08-0222 Permit Date 5/8/08

STATE WELL NO./STATION NO.	
LATITUDE	
LONGITUDE	
APN/TRS/OTHER	

GEOLOGIC LOG

WELL OWNER

ORIENTATION (X) VERTICAL HORIZONTAL ANGLE _____ (SPECIFY)

Name Angiola Water District

Mailing Address 944 Whitley Ave Ste A

Corcoran CA 93212

CITY STATE ZIP

Address Ave 112 & Rd 40

City Corcoran CA 93212

County Tulare County STATE ZIP

APN Book 311 Page 020 Parcel 010

Township 23S Range 23E Section 4

Latitude 35 57 26.38 NORTH Longitude 119 29 1.7 WEST

DEG. MIN. SEC. DEG. MIN. SEC.

LOCATION SKETCH NORTH ACTIVITY (X)

DRILLING METHOD Reverse Rotary FLUID _____

NEW WELL

MODIFICATION/REPAIR

Deepen

Other (Specify) _____

DESTROY (Describe Procedures and Materials Under "GEOLOGIC LOG")

PLANNED USES (X)

WATER SUPPLY

Domestic Public

Irrigation Industrial

MONITORING _____

TEST WELL _____

CATHODIC PROTECTION _____

HEAT EXCHANGE _____

DIRECT PUSH _____

INJECTION _____

VAPOR EXTRACTION _____

SPARGING _____

REMEDICATION _____

OTHER (SPECIFY) _____

WEST EAST

SOUTH

Illustrate or Describe Distance of Well from Roads Buildings, Fences, Rivers etc and attach map. Use additional paper if necessary. PLEASE BE ACCURATE & COMPLETE.

WATER LEVEL & YIELD OF COMPLETED WELL

DEPTH TO FIRST WATER Unknown (Ft.) BELOW SURFACE

DEPTH OF STATIC 321.93 (Ft.) & DATE MEASURED Late July through 8/1/08

WATER LEVEL _____

ESTIMATED YIELD 1685 (GPM) & TEST TYPE pump

TEST LENGTH 57 (Hrs.) TOTAL DRAWDOWN 163.56 (Ft.)

* May not be representative of a well's long-term yield.

DEPTH FROM SURFACE

FL to Ft.

60 : 260 sand, clay

260 : 300 clay, sand

300 : 310 clay, sand, little, gravel

310 : 320 clay, sand

320 : 1330 sand, clay

Describe material, grain size, color, etc.

TOTAL DEPTH OF BORING 1332 (Feet)

TOTAL DEPTH OF COMPLETED WELL 1312 (Feet)

DEPTH FROM SURFACE Ft. to Ft.	BORE-HOLE DIA. (inches)	CASING (S)				MATERIAL / GRADE	OUTSIDE DIAMETER (inches)	GAUGE OR WALL THICKNESS	SLOT SIZE IF ANY (Inches)	DEPTH FROM SURFACE Ft. to Ft.	ANNULAR MATERIAL			
		TYPE (-)	BLANK	SCREEN	CON-DUCTOR						FILL PIPE	TYPE		
0 : 40	36		X			Steel	30	.375		0 : 500	X			
0 : 870	26	X				Steel	16	.375		500 : 510				Hole Plug
870 : 910	26	X				Steel	16	.312	Full Flow .060	510 : <u>1312</u>			X	Gravel Pack 1/4 X 10
910 : 930	26	X				Steel	16	.375						
930 : 990	26	X				Steel	16	.312	VMS .060					
990 : 1044	26	X				Steel	16	.375						

ATTACHMENTS (X)

- Geologic Log
- Well Construction Diagram
- Geophysical Log(s)
- Soil/Water Chemical Analyses
- Other _____

ATTACH ADDITIONAL INFORMATION, IF IT EXISTS.

CERTIFICATION STATEMENT

1, the undersigned, certify that this report is complete and accurate to the best of my knowledge and belief.

Layne Christensen Company

NAME (PERSON, FIRM, OR CORPORATION) (TYPED OR PRINTED)

ADDRESS 11001 Etiwanda Ave Fontana CA 92337

Signed [Signature] CITY STATE ZIP

DRILLER AUTHORIZED REPRESENTATIVE DATE SIGNED 5/28/08 C-57 LICENSE NUMBER 510011

IF ADDITIONAL SPACE IS NEEDED, USE NEXT CONSECUTIVELY NUMBERED FORM

TRIPPLICATE
Owner's Copy

Page 1 of 3

Owner's Well No. G-17 = 6-28

Date Work Began 9/13/2007, Ended 10/9/2007

Local Permit Agency TULARE COUNTY

Permit No. 07-0438 Permit Date 9/11/2007

STATE OF CALIFORNIA

WELL COMPLETION REPORT

Refer to Instruction Pamphlet

No. **E054498**

DWR USE ONLY -- DO NOT FILL IN

STATE WELL NO./STATION NO.			
LATITUDE		LONGITUDE	
APN/TRS/OTHER			

GEOLOGIC LOG

DEPTH FROM SURFACE		DESCRIPTION <i>Describe material, grain, size, color, etc.</i>
Fl.	to Fl.	
0	10	SANDY BROWN CLAY
10	12	COARSE SAND
12	15	SANDY BROWN CLAY
15	34	SANDY BROWN CLAY & GRAVEL
34	41	COARSE SAND
41	50	BROWN CLAY
50	73	SAND
73	76	GRAVEL
76	85	CLAY
85	92	HARD CLAY
92	104	SOFT CLAY
104	116	SANDY HARD CLAY
116	124	SAND
124	136	HARD CLAY
136	141	SANDY CLAY
141	149	CLAY
149	158	SANDY CLAY
158	183	CLAY
183	194	SAND & GRAVEL
194	199	COARSE SAND
199	209	CLAY
209	235	SAND
241	268	SANDY CLAY
268	310	CLAY
310	332	SANDY CLAY
332	356	SAND & GRAVEL
356	365	SAND
365	371	CLAY
371	377	GRAVEL & COARSE SAND
377	384	CLAY

TOTAL DEPTH OF BORING 1120 (Feet)
TOTAL DEPTH OF COMPLETED WELL 1120 (Feet)

WELL OWNER

Name ANGIOLA WATER DIST.
Mailing Address 944 WHITLEY AVE. SUITE
CORCORAN CA 93212
CITY STATE ZIP

WELL LOCATION

Address RD 40 & AVE 112
City ANGIOLA CA
County TULARE
APN Book 291 Page 110 Parcel 003
Township 22 S Range 23 E Section 34
Latitude

<p>LOCATION SKETCH</p>	<p>DEG. MIN. SEC. DEG. MIN. SEC.</p> <p>ACTIVITY (✓)</p> <p><input checked="" type="checkbox"/> NEW WELL</p> <p>MODIFICATION/REPAIR</p> <p>— Deepen</p> <p>— Other (Specify)</p> <p>— DESTROY (Describe Procedures and Materials Under "GEOLOGIC LOG")</p> <p>PLANNED USES (✓)</p> <p>WATER SUPPLY</p> <p>— Domestic — Public-Industrial</p> <p><input checked="" type="checkbox"/> Irrigation</p> <p>MONITORING —</p> <p>TEST WELL —</p> <p>CATHODIC PROTECTION —</p> <p>HEAT EXCHANGE —</p> <p>DIRECT PUSH —</p> <p>INJECTION —</p> <p>VAPOR EXTRACTION —</p> <p>SPARGING —</p> <p>REMEDIATION —</p> <p>OTHER (SPECIFY) —</p>
	<p>Illustrate or Describe Distance of Well from Roads, Buildings, Fences, Rivers, etc. and attach a map. Use additional paper if necessary. PLEASE BE ACCURATE & COMPLETE.</p>

WATER LEVEL & YIELD OF COMPLETED WELL

DEPTH TO FIRST WATER _____ (Fl.) BELOW SURFACE
DEPTH OF STATIC WATER LEVEL _____ (Fl.) & DATE MEASURED _____
ESTIMATED YIELD * _____ (GPM) & TEST TYPE _____
TEST LENGTH _____ (Hrs.) TOTAL DRAWDOWN _____ (Fl.)
May not be representative of a well's long-term yield.

DEPTH FROM SURFACE	BORE-HOLE DIA. (Inches)	CASING (S)				MATERIAL / GRADE	INTERNAL DIAMETER (Inches)	GAUGE OR WALL THICKNESS	SLOT SIZE IF ANY (Inches)
		TYPE (✓)	BLANK	SCREEN	CONDUCTOR FILL PIPE				
0	50	44"				STEEL	36"	5/16"	
0	760	30"	✓			STEEL	18"	3/8"	
760	762	30"	✓			STEEL	18" - 16"	3/8"	
762	1122	28"	✓			STEEL	16"	3/8"	.050 SLO

DEPTH FROM SURFACE	ANNULAR MATERIAL TYPE					
		FL. TO FL.	CE-MENT (✓)	BEN-TONITE (✓)	FILL (✓)	FILTER PACK (TYPE/SIZE)
0	50		✓			SIX SACK
0	700				✓	1/4 X #8
700	1120				✓	6 x 16 / 1/4 # 1

ATTACHMENTS (✓)

- Geologic Log
- Well Construction Diagram
- Geophysical Log(s)
- Soil/Water Chemical Analysis
- Other _____

CERTIFICATION STATEMENT

I, the undersigned, certify that this report is complete and accurate to the best of my knowledge and belief.

NAME MYERS BROS. WELL DRILLING, INC.
(PERSON, FIRM, OR CORPORATION) (TYPED OR PRINTED)

8650 E. LACEY BLVD. HANFORD CA 93230-4844
ADDRESS CITY STATE ZIP

Signed [Signature] DATE SIGNED 10/12/07 548214
WELL DRILLER/AUTHORIZED REPRESENTATIVE C-57 LICENSE NUMBER

TRIPPLICATE
Owner's Copy

STATE OF CALIFORNIA
WELL COMPLETION REPORT

DWR USE ONLY -- DO NOT FILL IN

Page 2 of 3

Refer to Instruction Pamphlet

Owner's Well No. G-17

No. **E054498**

Date Work Began 9/13/2007, Ended 10/9/2007

STATE WELL NO./STATION NO.	
LATITUDE	LONGITUDE
APN/TRS/OTHER	

Local Permit Agency TULARE COUNTY

Permit No. 07-0438 Permit Date 9/11/2007

GEOLOGIC LOG

DEPTH FROM SURFACE		DESCRIPTION <i>Describe material, grain, size, color, etc.</i>
Fl.	to Fl.	
384	399	COARSE SAND & GRAVEL
399	411	SANDY CLAY
411	416	SAND
416	436	CLAY
436	455	COARSE SAND
455	482	SANDY CLAY
482	547	CLAY
547	553	SAND
553	594	CLAY
594	607	SANDY CLAY
607	663	CLAY
663	672	SANDY CLAY
672	718	CLAY
718	740	SANDY CLAY
740	786	SAND
786	810	SANDY CLAY
810	826	CLAY
826	847	SAND
847	861	COARSE SAND
861	884	SANDY CLAY
884	903	CLAY
903	941	SAND
941	960	CLAY
960	987	COARSE SAND
987	1004	SANDY CLAY
1004	1011	SAND
1011	1025	COARSE SAND
1025	1041	CLAY
1041	1058	SAND
1058	1064	CLAY

ORIENTATION (✓) VERTICAL HORIZONTAL ANGLE _____ (SPECIFY)
 DRILLING METHOD REVERSE FLUID _____
 TOTAL DEPTH OF BORING 1120 (Feet)
 TOTAL DEPTH OF COMPLETED WELL 1120 (Feet)

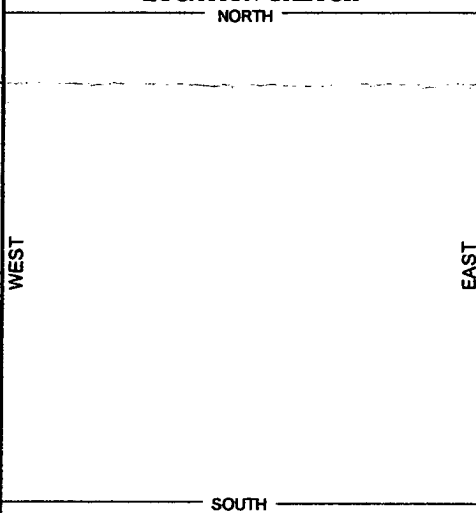
WELL OWNER

Name ANGIOLA WATER DIST.
 Mailing Address 944 WHITLEY AVE. SUITE
CORCORAN CA 93212
 CITY STATE ZIP

WELL LOCATION

Address RD 40 & AVE 112
 City ANGIOLA CA
 County TULARE
 APN Book 291 Page 110 Parcel 003
 Township 22 S Range 23 E Section 34
 Latitude _____

LOCATION SKETCH



Illustrate or Describe Distance of Well from Roads, Buildings, Fences, Rivers, etc. and attach a map. Use additional paper if necessary. PLEASE BE ACCURATE & COMPLETE.

- ACTIVITY (✓)
 NEW WELL
 MODIFICATION/REPAIR
 Deepen
 Other (Specify) _____
 DESTROY (Describe Procedures and Materials Under "GEOLOGIC LOG")
 PLANNED USES (✓)
 WATER SUPPLY
 Domestic Public
 Irrigation Industrial
 MONITORING _____
 TEST WELL _____
 CATHODIC PROTECTION _____
 HEAT EXCHANGE _____
 DIRECT PUSH _____
 INJECTION _____
 VAPOR EXTRACTION _____
 SPARGING _____
 REMEDIATION _____
 OTHER (SPECIFY) _____

WATER LEVEL & YIELD OF COMPLETED WELL

DEPTH TO FIRST WATER _____ (FL) BELOW SURFACE
 DEPTH OF STATIC WATER LEVEL _____ (FL) & DATE MEASURED _____
 ESTIMATED YIELD * _____ (GPM) & TEST TYPE _____
 TEST LENGTH _____ (Hrs.) TOTAL DRAWDOWN _____ (FL)
 * May not be representative of a well's long-term yield.

DEPTH FROM SURFACE Fl. to Fl.	BORE-HOLE DIA. (Inches)	CASING (S)				MATERIAL / GRADE	INTERNAL DIAMETER (Inches)	GAUGE OR WALL THICKNESS	SLOT SIZE IF ANY (Inches)
		TYPE (✓)	BLANK	SCREEN	CON-DUCTOR FILL PIPE				
0 : 50	44"				STEEL	36"	5/16"		
0 : 760	30"	✓			STEEL	18"	3/8"		
760 : 762	30"	✓			STEEL	18" - 16"	3/8"		
762 : 1122	28"	✓			STEEL	16"	3/8"	.050 SLO	

DEPTH FROM SURFACE Fl. to Fl.	ANNULAR MATERIAL			
	CE-MENT (✓)	BEN-TONITE (✓)	FILL (✓)	FILTER PACK (TYPE/SIZE)
0 : 50	✓			SIX SACK
0 : 700			✓	1/4 X #8
700 : 1120			✓	6 x 16 / 1/4 # 1

ATTACHMENTS (✓)

- Geologic Log
- Well Construction Diagram
- Geophysical Log(s)
- Soil/Water Chemical Analysis
- Other _____

ATTACH ADDITIONAL INFORMATION, IF IT EXISTS.

CERTIFICATION STATEMENT

I, the undersigned, certify that this report is complete and accurate to the best of my knowledge and belief.
 NAME MYERS BROS. WELL DRILLING, INC.
 (PERSON, FIRM, OR CORPORATION) (TYPED OR PRINTED)
8650 E. LACEY BLVD. HANFORD CA 93230-4844
 ADDRESS CITY STATE ZIP
 Signed _____ DATE SIGNED 10/12/07 548214
 WELL DRILLER/AUTHORIZED REPRESENTATIVE DATE SIGNED C-57 LICENSE NUMBER

TRIPPLICATE
Owner's Copy

Page 3 of 3

Owner's Well No. G-17

Date Work Began 9/13/2007, Ended 10/9/2007

Local Permit Agency TULARE COUNTY

Permit No. 07-0438

Permit Date 9/11/2007

STATE OF CALIFORNIA

WELL COMPLETION REPORT

Refer to Instruction Pamphlet

No. **E054498**

DWR USE ONLY — DO NOT FILL IN

STATE WELL NO./STATION NO.

LATITUDE LONGITUDE

APN/TRS/OTHER

GEOLOGIC LOG

WELL OWNER

ORIENTATION (✓) VERTICAL HORIZONTAL ANGLE _____ (SPECIFY)

DRILLING METHOD **REVERSE** FLUID _____

DEPTH FROM SURFACE

Fl.	to	Fl.	DESCRIPTION
1064	1081		COARSE SAND
1081	1100		SANDY CLAY
1100	1118		SAND
1118	1120		CLAY

Describe material, grain, size, color, etc.

TOTAL DEPTH OF BORING 1120 (Feet)

TOTAL DEPTH OF COMPLETED WELL 1120 (Feet)

Name ANGIOLA WATER DIST.

Mailing Address 944 WHITLEY AVE. SUITE
CORCORAN CA 93212

CITY STATE ZIP

WELL LOCATION

Address RD 40 & AVE 112

City ANGIOLA CA

County TULARE

APN Book 291 Page 110 Parcel 003

Township 22 S Range 23 E Section 34

Latitude _____

LOCATION SKETCH

NORTH

WEST EAST

ACTIVITY (✓)

NEW WELL

MODIFICATION/REPAIR
 Deepen
 Other (Specify)

DESTROY (Describe Procedures and Materials Under "GEOLOGIC LOG")

PLANNED USES (✓)

WATER SUPPLY
 Domestic Public
 Irrigation Industrial

MONITORING _____

TEST WELL _____

CATHODIC PROTECTION _____

HEAT EXCHANGE _____

DIRECT PUSH _____

INJECTION _____

VAPOR EXTRACTION _____

SPARGING _____

REMEDICATION _____

OTHER (SPECIFY) _____

Illustrate or Describe Distance of Well from Roads, Buildings, Fences, Rivers, etc. and attach a map. Use additional paper if necessary. PLEASE BE ACCURATE & COMPLETE.

WATER LEVEL & YIELD OF COMPLETED WELL

DEPTH TO FIRST WATER _____ (FL) BELOW SURFACE

DEPTH OF STATIC _____

WATER LEVEL _____ (FL) & DATE MEASURED _____

ESTIMATED YIELD * _____ (GPM) & TEST TYPE _____

TEST LENGTH _____ (Hrs.) TOTAL DRAWDOWN _____ (FL.)

May not be representative of a well's long-term yield.

DEPTH FROM SURFACE	BORE HOLE DIA. (Inches)	CASING (S)				
		TYPE (✓)	MATERIAL / GRADE	INTERNAL DIAMETER (Inches)	GAUGE OR WALL THICKNESS	SLOT SIZE IF ANY (Inches)
0	50	44"	✓	STEEL	36"	5/16"
0	760	30"	✓	STEEL	18"	3/8"
760	762	30"	✓	STEEL	18" - 16"	3/8"
762	1122	28"	✓	STEEL	16"	3/8" .050 SLO

DEPTH FROM SURFACE	ANNULAR MATERIAL TYPE			
	FL	to	FL	FILTER PACK (TYPE/SIZE)
0	50		✓	SIX SACK
0	700		✓	1/4 X #8
700	1120		✓	6 x 16 / 1/4 # 1

- ATTACHMENTS (✓)**
- Geologic Log
 - Well Construction Diagram
 - Geophysical Log(s)
 - Soil/Water Chemical Analysis
 - Other _____
- ATTACH ADDITIONAL INFORMATION, IF IT EXISTS.

CERTIFICATION STATEMENT

I, the undersigned, certify that this report is complete and accurate to the best of my knowledge and belief.

NAME MYERS BROS. WELL DRILLING, INC.

(PERSON, FIRM, OR CORPORATION) (TYPED OR PRINTED)

8650 E. LACEY BLVD. HANFORD CA 93230-4844

ADDRESS CITY STATE ZIP

Signed _____ DATE SIGNED 10/12/07 548214

WELL DRILLER/AUTHORIZED REPRESENTATIVE C-57 LICENSE NUMBER

STATE OF CALIFORNIA
WELL COMPLETION REPORT
Refer to Instruction Pamphlet

DWR USE ONLY - DO NOT FILL IN

Page 1 of 2

Owner's Well No. 3 / E-22 No. e0078570

Date Work Began 5/19/08 Ended 10/3/08

Local Permit Agency Tulare County Environmental Health Division

Permit No. 08-0248 Permit Date 5/19/08

STATE WELL NO./STATION NO.	
LATITUDE	LONGITUDE
APN/TRS/OTHER	

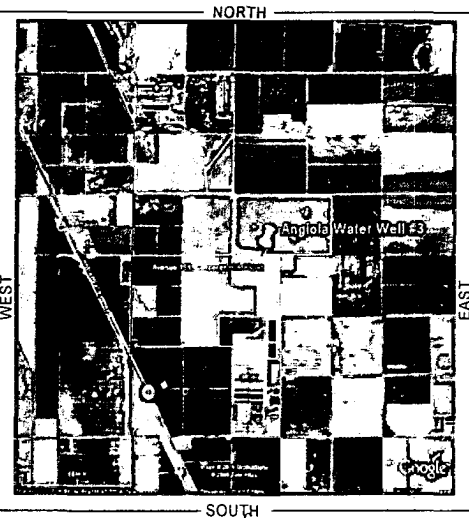
GEOLOGIC LOG

WELL OWNER

ORIENTATION (X)	<input checked="" type="checkbox"/> VERTICAL	<input type="checkbox"/> HORIZONTAL	ANGLE _____ (SPECIFY)
DEPTH FROM SURFACE	DRILLING METHOD	Reverse Rotary	FLUID _____
FL to Ft.	DESCRIPTION		
	Describe material, grain size, color, etc.		
40 - 60	Sand, pebbles		
60 - 360	Sand		
360 - 370	Sand, little clay		
370 - 380	Sand, Clay		
380 - 390	Sand, little clay		
390 - 720	Sand, little clay		
720 - 880	Clay, sand		
880 - 1010	Sand, Clay		
1010 - 1150	Clay, sand		

Name Angiola Water District
Mailing Address 944 Whitley Ave Ste A
Corcoran Ca 93212
CITY STATE ZIP
Address 1.8 Mi E Hwy 43 off Ave 108
City Corcoran Ca 93212
County Tulare County STATE ZIP
APN Book 293 Page 230 Parcel 01
Township 22S Range 23E Section 25
Latitude 35 59 8.66 NORTH Longitude 119 26 30.18 WEST
DEG. MIN. SEC. DEG. MIN. SEC.

LOCATION SKETCH



ACTIVITY (X)

NEW WELL
 MODIFICATION/REPAIR

— Deepen
— Other (Specify)

DESTROY (Describe Procedures and Materials Under "GEOLOGIC LOG")

PLANNED USES (X)

WATER SUPPLY

Domestic Public
 Irrigation Industrial

MONITORING
TEST WELL
CATHODIC PROTECTION
HEAT EXCHANGE
DIRECT PUSH
INJECTION
VAPOR EXTRACTION
SPARGING
REMEDICATION - OTHER (SPECIFY)

Illustrate or Describe Distance Of Well from Roads Buildings, Fences, Rivers etc and attach map. Use additional paper if necessary. PLEASE BE ACCURATE & COMPLETE.

WATER LEVEL & YIELD OF COMPLETED WELL

DEPTH TO FIRST WATER Unknown (Ft.) BELOW SURFACE

DEPTH OF STATIC WATER LEVEL 328.95 (Ft.) & DATE MEASURED 9/30/08-10/3/08

ESTIMATED YIELD 2075 (GPM) & TEST TYPE Step and constant pump

TEST LENGTH 35 (Hrs.) TOTAL DRAWDOWN 74.08 (Ft.)

* May not be representative of a well's long-term yield.

TOTAL DEPTH OF BORING 1160 (Feet)
TOTAL DEPTH OF COMPLETED WELL 1140 (Feet)

DEPTH FROM SURFACE Ft. to Ft.	BORE-HOLE DIA. (inches)	CASING (S)						DEPTH FROM SURFACE Ft. to Ft.	ANNULAR MATERIAL			
		TYPE (-)	MATERIAL / GRADE	OUTSIDE DIAMETER (inches)	GAUGE OR WALL THICKNESS	SLOT SIZE IF ANY (Inches)	CE- MENT (X)		BEN- TONITE (X)	FILL (X)	FILTER PACK (TYPE/SIZE)	
0 - 40	40		Steel	30	.375		0 - 500	X			8 Sac Sand Slurry	
0 - 640	26	X	Steel	16	.375		500 - 510				Hole Plug	
640 - 700	26	X	Steel	16	.312	.060 Full Flow	510 - 1140			X	1/4 x 10 Greenfield Gravel Pack	
700 - 720	26	X	Steel	16	.375							
720 - 800	26	X	Steel	16	.312	.060 Full Flow						
800 - 860	26	X	Steel	16	.375							

ATTACHMENTS (X)

- Geologic Log
- Well Construction Diagram
- Geophysical Log(s)
- Soil/Water Chemical Analyses
- Other _____

CERTIFICATION STATEMENT

I, the undersigned, certify that this report is complete and accurate to the best of my knowledge and belief.

Layne Christensen Company

NAME (PERSON, FIRM, OR CORPORATION) (TYPED OR PRINTED)

ADDRESS 11001 Etiwanda Ave Fontana Ca 92337
CITY STATE ZIP

Signed [Signature] DATE SIGNED 10/7/08 C-57 LICENSE NUMBER 510011
WELL DRILLER AUTHORIZED REPRESENTATIVE

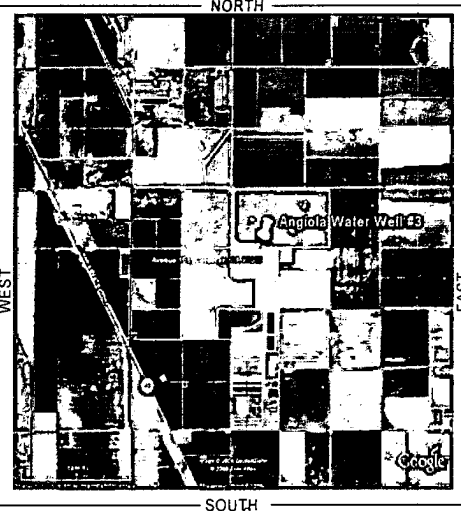
ATTACH ADDITIONAL INFORMATION, IF IT EXISTS.

STATE OF CALIFORNIA WELL COMPLETION REPORT

Refer to Instruction Pamphlet

DWR USE ONLY - DO NOT FILL IN	
STATE WELL NO./STATION NO.	
LATITUDE	LONGITUDE
APN/TRS/OTHER	

Page 2 of 2
 Owner's Well No. 3 / E-22 No. e0078570
 Date Work Began 5/19/08 Ended 10/3/08
 Local Permit Agency Tulare County Environmental Health Division
 Permit No. 08-0248 Permit Date 5/19/08

GEOLOGIC LOG	WELL OWNER
ORIENTATION (<input checked="" type="checkbox"/>) VERTICAL <input type="checkbox"/> HORIZONTAL <input type="checkbox"/> ANGLE _____ (SPECIFY) DRILLING METHOD <u>Reverse Rotary</u> FLUID _____ DESCRIPTION _____ Describe material, grain size, color, etc.	Name <u>Angiola Water District</u> Mailing Address <u>944 Whitley Ave Ste A</u> City <u>Corcoran</u> Ca <u>93212</u> STATE ZIP WELL LOCATION Address <u>1.8 Mi E Hwy 43 off Ave 108</u> City <u>Corcoran</u> Ca <u>93212</u> STATE ZIP County <u>Tulare County</u> APN Book <u>293</u> Page <u>230</u> Parcel <u>01</u> Township <u>22S</u> Range <u>23E</u> Section <u>25</u> Latitude <u>35 59 8.66</u> NORTH Longitude <u>119 26 30.18</u> WEST DEG. MIN. SEC. DEG. MIN. SEC.
DEPTH FROM SURFACE _____ FL to Ft. _____	LOCATION SKETCH 
TOTAL DEPTH OF BORING <u>1160</u> (Feet) TOTAL DEPTH OF COMPLETED WELL <u>1140</u> (Feet)	ACTIVITY (<input checked="" type="checkbox"/>) <input type="checkbox"/> NEW WELL <input type="checkbox"/> MODIFICATION/REPAIR _____ Deepen _____ Other (Specify) _____ _____ DESTROY (Describe Procedures and Materials Under "GEOLOGIC LOG") PLANNED USES (<input checked="" type="checkbox"/>) WATER SUPPLY <input checked="" type="checkbox"/> Domestic _____ Public <input checked="" type="checkbox"/> Irrigation _____ Industrial MONITORING _____ TEST WELL _____ CATHODIC PROTECTION _____ HEAT EXCHANGE _____ DIRECT PUSH _____ INJECTION _____ VAPOR EXTRACTION _____ SPARGING _____ REMEDIATION - OTHER (SPECIFY) _____
WATER LEVEL & YIELD OF COMPLETED WELL DEPTH TO FIRST WATER <u>Unknown</u> (Ft.) BELOW SURFACE DEPTH OF STATIC WATER LEVEL <u>328.95</u> (Ft.) & DATE MEASURED <u>9/30/08-10/3/08</u> ESTIMATED YIELD <u>2075</u> (GPM) & TEST TYPE <u>Step and constant pump</u> TEST LENGTH <u>35</u> (Hrs.) TOTAL DRAWDOWN <u>74.08</u> (Ft.) * May not be representative of a well's long-term yield.	

DEPTH FROM SURFACE Ft. to Ft.	BORE-HOLE DIA. (inches)	CASING (S)							DEPTH FROM SURFACE Ft. to Ft.	ANNULAR MATERIAL TYPE				
		BLANK	SCREEN	CONDUIT	DUCTOR	FILL PIPE	MATERIAL / GRADE	OUTSIDE DIAMETER (inches)		GAUGE OR WALL THICKNESS	SLOT SIZE IF ANY (Inches)	CE-MENT (X)	BEN-TONITE (X)	FILL (X)
860 to 900	26	X					Steel	16	.312	.060 Full Flow				
900 to 940	26	X					Steel	16	.375					
940 to 960	26	X					Steel	16	.312	.060 Full Flow				
960 to 1020	26	X					Steel	16	.375					
1020 to 1120	26	X					Steel	16	.312	.060 Full Flow				
1120 to 1140	26	X					Steel-sump	16	.375					

ATTACHMENTS (<input checked="" type="checkbox"/>)	CERTIFICATION STATEMENT
<input checked="" type="checkbox"/> Geologic Log <input checked="" type="checkbox"/> Well Construction Diagram <input type="checkbox"/> Geophysical Log(s) <input type="checkbox"/> Soil/Water Chemical Analyses <input type="checkbox"/> Other _____	1, the undersigned certify that this report is complete and accurate to the best of my knowledge and belief. <p style="text-align: center;">Layne Christensen Company</p> NAME (PERSON, FIRM OR CORPORATION) (TYPED OR PRINTED) <u>11001 Etiwanda Ave</u> ADDRESS Fontana Ca 92337 CITY STATE ZIP Signed <u>[Signature]</u> DATE SIGNED <u>10/7/08</u> C-57 LICENSE NUMBER <u>510011</u> WELL DRILLER AUTHORIZED REPRESENTATIVE

Owner's Well No. E-21

Date Work Began 10/27/2007, Ended 11/16/2007

Local Permit Agency TULARE COUNTY

Permit No. 07-0479

Permit Date 10/2/2007

STATE OF CALIFORNIA
WELL COMPLETION REPORT
Refer to Instruction Pamphlet

No. **E062799**

DWR USE ONLY -- DO NOT FILL IN

STATE WELL NO./STATION NO.

LATITUDE LONGITUDE

APN/TRS/OTHER

GEOLOGIC LOG

ORIENTATION (✓)		DRILLING METHOD	FLUID	DESCRIPTION
<input checked="" type="checkbox"/> VERTICAL <input type="checkbox"/> HORIZONTAL <input type="checkbox"/> ANGLE _____ (SPECIFY)		<u>REVERSE</u>		<i>Describe material, grain, size, color, etc.</i>
DEPTH FROM SURFACE	Ft. to Ft.			
0	10	SANDY BROWN CLAY		
10	13	MEDIUM SAND		
13	28	SANDY BROWN CLAY		
28	37	MEDIUM SAND		
37	50	SANDY BROWN CLAY		
50	67	CLAY		
67	94	FINE SAND		
94	107	CLAY		
107	111	SAND		
111	146	CLAY		
146	164	SANDY CLAY		
164	192	SAND		
192	207	SANDY CLAY		
207	239	SAND		
239	268	CLAY		
268	304	SANDY CLAY		
304	309	SAND		
309	332	CLAY		
332	351	SAND		
351	356	SANDY CLAY		
356	401	SAND		
401	426	SANDY CLAY		
426	447	SAND		
447	454	CLAY		
454	470	SAND		
470	492	SANDY CLAY		
492	596	CLAY		
596	616	SANDY CLAY		
616	633	CLAY		
633	643	SAND		
TOTAL DEPTH OF BORING <u>1220</u>		(Feet)		
TOTAL DEPTH OF COMPLETED WELL <u>1200</u>		(Feet)		

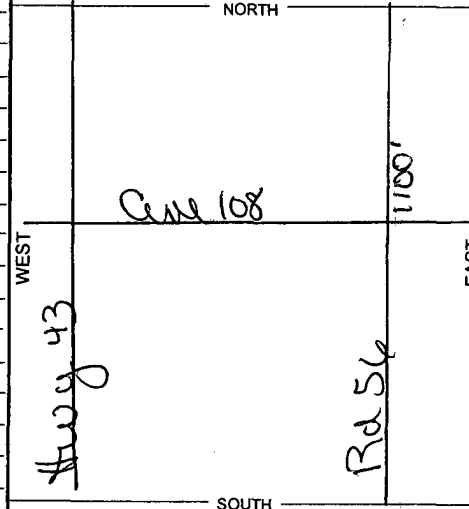
WELL OWNER

Name ANGIOLA WATER DIST.
Mailing Address 944 WHITLEY AVE. SUITE
CORCORAN CA 93212
CITY STATE ZIP

WELL LOCATION

Address AVE 108. & HWY 43
City ANGIOLA CA
County TULARE
APN Book 293 Page 230 Parcel 001
Township 22 S Range 23 E Section 25
Latitude _____

LOCATION SKETCH



ACTIVITY (✓)

NEW WELL
MODIFICATION/REPAIR
 Deepen
 Other (Specify)

DESTROY (Describe Procedures and Materials Under "GEOLOGIC LOG")

PLANNED USES (✓)

WATER SUPPLY
 Domestic Public
 Irrigation Industrial

MONITORING
TEST WELL
CATHODIC PROTECTION
HEAT EXCHANGE
DIRECT PUSH
INJECTION
VAPOR EXTRACTION
SPARGING
REMEDIATION
OTHER (SPECIFY) _____

Illustrate or Describe Distance of Well from Roads, Buildings, Fences, Rivers, etc. and attach a map. Use additional paper if necessary. PLEASE BE ACCURATE & COMPLETE.

WATER LEVEL & YIELD OF COMPLETED WELL

DEPTH TO FIRST WATER _____ (Ft.) BELOW SURFACE

DEPTH OF STATIC

WATER LEVEL _____ (Ft.) & DATE MEASURED _____

ESTIMATED YIELD * _____ (GPM) & TEST TYPE _____

TEST LENGTH _____ (Hrs.) TOTAL DRAWDOWN _____ (Ft.)

May not be representative of a well's long-term yield.

DEPTH FROM SURFACE	BORE-HOLE DIA. (Inches)	CASING (S)							
		TYPE (✓)	MATERIAL / GRADE	INTERNAL DIAMETER (Inches)	GAUGE OR WALL THICKNESS	SLOT SIZE IF ANY (Inches)			
Ft. to Ft.		BLANK	SCREEN	CONDUCTOR	FILL PIPE				
0	50	44"					STEEL	34"	5/16"
0	640	28"	✓				STEEL	16"	3/8"
640	1200	28"	✓				STEEL	16"	5/16" .060 DBL

DEPTH FROM SURFACE	ANNULAR MATERIAL			
	TYPE			
Ft. to Ft.	CE-MENT (✓)	BEN-TONITE (✓)	FILL (✓)	FILTER PACK (TYPE/SIZE)
0	50	✓		SIX SACK
0	600		✓	1/4
600	1220		✓	6 X 16

ATTACHMENTS (✓)

- Geologic Log
- Well Construction Diagram
- Geophysical Log(s)
- Soil/Water Chemical Analysis
- Other _____

ATTACH ADDITIONAL INFORMATION, IF IT EXISTS.

CERTIFICATION STATEMENT

I, the undersigned, certify that this report is complete and accurate to the best of my knowledge and belief.

NAME MYERS BROS. WELL DRILLING, INC.

(PERSON, FIRM, OR CORPORATION) (TYPED OR PRINTED)

8650 E. LACEY BLVD.

HANFORD

CA

93230-4844

ADDRESS

CITY

STATE

ZIP

Signed _____

WELL DRILLER/AUTHORIZED REPRESENTATIVE

11/26/07

DATE SIGNED

548214

C-57 LICENSE NUMBER

Owner's Well No. E-21

Date Work Began 10/27/2007, Ended 11/16/2007

Local Permit Agency TULARE COUNTY

Permit No. 07-0479

Permit Date 10/2/2007

STATE OF CALIFORNIA
WELL COMPLETION REPORT

Refer to Instruction Pamphlet

No. **E062799**

DWR USE ONLY -- DO NOT FILL IN

STATE WELL NO./STATION NO.

LATITUDE LONGITUDE

APN/TRS/OTHER

GEOLOGIC LOG

ORIENTATION (✓)		DRILLING METHOD	FLUID	DESCRIPTION
<input checked="" type="checkbox"/> VERTICAL <input type="checkbox"/> HORIZONTAL <input type="checkbox"/> ANGLE _____ (SPECIFY)		<u>REVERSE</u>	_____	Describe material, grain, size, color, etc.
DEPTH FROM SURFACE	Ft. to Ft.			
643	668	SANDY CLAY		
668	677	CLAY		
677	694	SAND		
694	703	CLAY		
703	716	SANDY CLAY		
716	738	SAND		
738	743	CLAY		
743	760	SANDY CLAY		
760	794	SAND		
794	799	CLAY		
799	811	SANDY CLAY		
811	863	SAND		
863	882	CLAY		
882	910	SAND		
910	932	CLAY		
932	941	SAND		
941	962	SANDY CLAY		
962	991	SAND		
991	1002	CLAY		
1002	1013	SANDY CLAY		
1013	1018	CLAY		
1018	1026	SAND		
1026	1063	SANDY CLAY		
1063	1091	SAND		
1091	1099	CLAY		
1099	1126	SAND		
1126	1150	CLAY		
1150	1164	SANDY CLAY		
1164	1176	SAND		
1176	1220	CLAY		
TOTAL DEPTH OF BORING <u>1220</u> (Feet)				
TOTAL DEPTH OF COMPLETED WELL <u>1200</u> (Feet)				

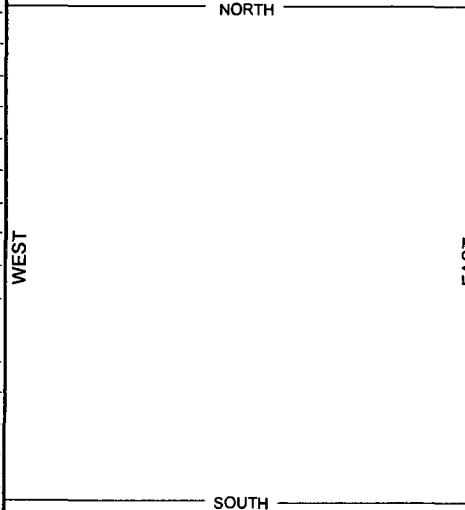
WELL OWNER

Name ANGIOLA WATER DIST.
 Mailing Address 944 WHITLEY AVE. SUITE
CORCORAN CA 93212
 CITY STATE ZIP

WELL LOCATION

Address AVE 108. & HWY 43
 City ANGIOLA CA
 County TULARE
 APN Book 293 Page 230 Parcel 001
 Township 22 S Range 23 E Section 25
 Latitude _____

LOCATION SKETCH



DEG. MIN. SEC. DEG. MIN. SEC.

ACTIVITY (✓)

NEW WELL

MODIFICATION/REPAIR

— Deepen

— Other (Specify) _____

— DESTROY (Describe Procedures and Materials Under "GEOLOGIC LOG")

PLANNED USES (✓)

WATER SUPPLY

— Domestic Public

Irrigation Industrial

MONITORING _____

TEST WELL _____

CATHODIC PROTECTION _____

HEAT EXCHANGE _____

DIRECT PUSH _____

INJECTION _____

VAPOR EXTRACTION _____

SPARGING _____

REMEDIATION _____

OTHER (SPECIFY) _____

WATER LEVEL & YIELD OF COMPLETED WELL

DEPTH TO FIRST WATER _____ (Ft.) BELOW SURFACE

DEPTH OF STATIC WATER LEVEL _____ (Ft.) & DATE MEASURED _____

ESTIMATED YIELD * _____ (GPM) & TEST TYPE _____

TEST LENGTH _____ (Hrs.) TOTAL DRAWDOWN _____ (Ft.)

May not be representative of a well's long-term yield.

DEPTH FROM SURFACE	BORE-HOLE DIA. (Inches)	CASING (S)					ANNULAR MATERIAL							
		TYPE (✓)	MATERIAL / GRADE	INTERNAL DIAMETER (Inches)	GAUGE OR WALL THICKNESS	SLOT SIZE IF ANY (Inches)	TYPE	CEMENT	BENTONITE	FILL	FILTER PACK (TYPE/SIZE)			
0	50	44"					STEEL	34"	5/16"					
0	640	28"	✓				STEEL	16"	3/8"					SIX SACK
640	1200	28"	✓				STEEL	16"	5/16"	.060 DBL				1/4
														6 X 16

ATTACHMENTS (✓)

- Geologic Log
- Well Construction Diagram
- Geophysical Log(s)
- Soil/Water Chemical Analysis
- Other _____

ATTACH ADDITIONAL INFORMATION, IF IT EXISTS.

CERTIFICATION STATEMENT

I, the undersigned, certify that this report is complete and accurate to the best of my knowledge and belief.

NAME MYERS BROS. WELL DRILLING, INC.
 (PERSON, FIRM, OR CORPORATION) (TYPED OR PRINTED)

8650 E. LACEY BLVD. HANFORD CA 93230-4844
 ADDRESS CITY STATE ZIP

Signed _____ 11/26/07 548214
 WELL DRILLER/AUTHORIZED REPRESENTATIVE DATE SIGNED C-57 LICENSE NUMBER

Appendix C

Groundwater Level Field Measurement Form



Field Groundwater Level Measurements

Well Name/ Number:	Checked By:
Project:	Field Personnel:

Well Name/Owner	Date	Time	Reference Point Elevation (ft)	Depth To Groundwater (ft)	Groundwater Elevation (ft)	Instrument Type

Appendix D

Chalk/Tape Groundwater Level Measurement



Appendix E

Quality Assurance Project Plan



ELEMENT 1: TITLE AND APPROVAL SHEETS**Draft Tule Basin Water Quality Coalition**

Surface Water and Groundwater Monitoring Plan
Quality Assurance Program Plan

Revision

July 1, 2019

Approvals

R.L. Schafer, RCE, RAE Tule Basin Water Quality Coalition Program Coordinator	Date
---	------

David De Groot, RCE 4Creeks, Inc. Project Manager, Technical Lead	Date
---	------

Michelle Parker R.L Schafer & Associates Quality Assurance Manager, Laboratory Coordinator	Date
--	------

Belinda C. Vega, Laboratory Director BSK Associates Laboratory Program Manager	Date
--	------

Draft Tule Basin Water Quality Coalition

Surface Water Monitoring Plan
Quality Assurance Program Plan

Revision
July 1, 2019

Approvals, cont.

David Sholes, Non-Point Source/AG Planning Date
California Regional Water Quality Control Board
QAPP Review

Renee Spears, Quality Assurance Officer Date
State Water Resources Control Board
QAPP Review

Element 2: TABLE OF CONTENTS

ELEMENT 1: TITLE AND APPROVAL SHEETS.....	1
ELEMENT 2: TABLE OF CONTENTS	3
ELEMENT 3: DISTRIBUTION LIST.....	6
ELEMENT 4: PROJECT ORGANIZATION.....	8
ELEMENT 5: PROBLEM DESCRIPTION AND BACKGROUND	13
ELEMENT 6: PROJECT DESCRIPTION.....	21
ELEMENT 7: QUALITY OBJECTIVES AND CRITERIA.....	27
ELEMENT 8: SPECIAL TRAINING NEEDS / CERTIFICATIONS	32
ELEMENT 9: DOCUMENTS AND RECORDS.....	33
ELEMENT 10: SAMPLING PROCESS DESIGN.....	36
ELEMENT 11: SAMPLING METHODS – ADD SOP FOR SUPPLY WELL SAMPLING.....	43
ELEMENT 12: SAMPLE HANDLING AND CUSTODY.....	48
ELEMENT 13: ANALYTICAL METHODS AND FIELD MEASUREMENTS	50
ELEMENT 14: QUALITY CONTROL	63
ELEMENT 15: INSTRUMENT/EQUIPMENT TESTING, INSPECTION, AND MAINTENANCE	67
ELEMENT 16: INSTRUMENT/EQUIPMENT CALIBRATION AND FREQUENCY.....	69
ELEMENT 17: INSPECTION / ACCEPTANCE OF SUPPLIES AND CONSUMABLES.....	70
ELEMENT 18: NON-DIRECT MEASUREMENTS	70
ELEMENT 19: DATA MANAGEMENT	71
ELEMENT 20: ASSESSMENT AND RESPONSE ACTIONS.....	72
ELEMENT 21: REPORTS TO MANAGEMENT	73
ELEMENT 22: DATA REVIEW, VERIFICATION AND VALIDATION.....	74
ELEMENT 23: VERIFICATION AND VALIDATION METHODS.....	75
ELEMENT 24: RECONCILIATION WITH USER REQUIREMENTS.....	76
ELEMENT 25: DEFINITIONS.....	77

TABLES

Table 1: MRP Chemistries and BPOs for Tulare Lake Basin Surface Waters
Table 2: MRP Chemistries and BPOs for Tulare Lake Basin Ground Waters
Table 3: Coalition Sampling Points – Data Evaluation Criteria
Table 4: Data Quality Objectives
Table 5: Coalition Surface Water Sampling Point Coordinates
Table 6: Method Preservation, Storage and Holding Time Requirements
Table 7: Standard Operating Procedures
Table 8: Methods, Reporting Limits and Detection Limits
Table 9: Laboratory Method QC Criteria
Table 10: Required Quality Control by Method
Table 11: BSK Field Instrumentation
Table 12: TBWQC Field Instrumentation
Table 13: Laboratory Instrumentation

FIGURES

- Figure 1: Organizational Chart
- Figure 2: Tule Basin Water Quality Coalition Boundary Map
- Figure 3: Deer Creek at Road 120 Site Map
- Figure 4: Deer Creek at Road 176 Site Map
- Figure 5: Deer Creek at Road 248 Site Map
- Figure 6: Porter Slough near Road 192 Site Map
- Figure 7: Tule River at North Fork Road 144 Site Map
- Figure 8: Tule River at Road 92 Site Map
- Figure 9: GQTMP Well Network

APPENDICES

Appendix A: Sample Forms

- A.1: Chain of Custody
- A.2: Surface Water Field Sample Collection Logs
- A.3: Supply Well Field Sample Collection Logs
- A.3: Data Completeness Worksheet (Example)
- A.4: Field and Transport Worksheet (Example)

Appendix B: Standard Operating Procedures (Proprietary, excluded from public release)

- B.1: BSK Associates Standard Operating Procedures*
 - B.1.1 Ammonia by Gas Diffusion, Automated Phenate
 - B.1.2 Anions by Ion Chromatography
 - B.1.3 Carbamates by LC-MS/MS
 - B.1.4 Glyphosate by HPLC, Post Column Derivatization
 - B.1.5 Metals by ICP-MS
 - B.1.6 Metals by ICP-AES
 - B.1.7 Metals (Total Recoverable) Preparation
 - B.1.8 o-Phosphate and Phosphorus by Ascorbic Acid Reduction
 - B.1.9 Paraquat by SPE, HPLC-UV
 - B.1.10 Multi-tube Fermentation for Total and Fecal Coliform, and E. coli
 - B.1.11 Nitrogen, Organophosphorus and Pyrethroid Pesticides by GC-MS
 - B.1.12 Organochlorine Pesticides by GC-ECD
 - B.1.13 Solids by Gravimetric Determination
 - B.1.14 Turbidity by Nephelometry
 - B.1.15 Complex Calculations (Hardness)
 - B.1.16 Total and Dissolved Organic Carbon by TOC Analyzer
 - B.1.17 Alkalinity by PC Titrate
 - B.1.18 Field Sampling from Streams, Rivers and Canals
 - B.1.19 Safety for Stream and Canal Sampling

B.2: Aquatic Bioassay Consulting Laboratory Standard Operating Procedures

- B.2.1 Chronic Toxicity (Algae)
- B.2.2 Acute Toxicity (Water Flea)
- B.2.3 Acute Toxicity (Fathead Minnow)
- B.2.4 Sediment Toxicity (*Hyalella azteca*)

B.3: Pacific EcoRisk Laboratory Standard Operating Procedures

- B.3.1 Chronic Toxicity (Algae)
- B.3.2 Acute Toxicity (Water Flea)
- B.3.3 Acute Toxicity (Fathead Minnow)
- B.3.4 Sediment Toxicity (*Hyalella azteca*)

Appendix C: Certifications

- C.1: BSK Associates ELAP and NELAP Certificates
- C.2: ABC Laboratory ELAP Certificate
- C.3: PER Laboratory ELAP and NELAP Certificates

Appendix D: Quality Assurance Manuals (Proprietary, excluded from public release)

- D.1: BSK Associates Quality Assurance Manual (QAM)
- D.2: ABC Laboratory Quality Assurance Manual (QAM)
- D.3: PER Laboratory Quality Assurance Manual (QAM)

ELEMENT 3: DISTRIBUTION LIST

Coalition Contacts:

R.L. Schafer
Tule Basin Water Quality Coalition
2904 W. Main Street
Visalia, CA 93291
559-627-2948
rschafer@rlsmap.com

David De Groot
4Creeks, Inc.
324 S. Sante Fe, Suite A
Visalia, CA 93292
(559) 802-3052
davidd@4-creeks.com

Laboratory Contacts:

BSK Associates
Belinda C. Vega
Laboratory Director
1414 Stanislaus
Fresno, CA 93706
559-497-2888 x 133
mvega@bskassociates.com

BSK Associates
Michael Ng
Quality Assurance Manager
1414 Stanislaus
Fresno, CA 93706
559-497-2888 x 118
mng@bskassociates.com

BSK Associates
Stephane Maupas
Project Management Supervisor
1414 Stanislaus
Fresno, CA 93706
559-497-2888 x 212
smaupas@bskassociates.com

QAPP Recipients

Patrick Pulupa
Executive Officer
Central Valley Regional Water Quality Control Board
11020 Sun Center Drive, Suite 200
Rancho Cordova, CA 95670

Clay Rodgers
Central Valley Regional Water Quality Control Board
Fresno Office
1685 E Street
Fresno, CA 93706

R.L. Schafer
2904 W. Main Street
Visalia, CA 93291

4 Creeks
324 S. Sante Fe, Suite A
Visalia, CA 93292

BSK Associates
1414 Stanislaus Street
Fresno, CA 93706

ELEMENT 4: PROJECT ORGANIZATION

Personnel

R.L. Schafer Program Lead Tule Basin Water Quality Coalition

Mr. Schafer graduated from the University of South Dakota, School of Mines and Technology in 1951, attended graduate school in the University of California and is a registered civil engineer in six states. Mr. Schafer specializes in water rights, hydrology, hydraulics & hydrography, water distribution systems, canals, pipelines and related structures; domestic water systems; well construction and equipment; drainage systems and flood control works. Mr. Schafer also directs land development projects, subdivisions of properties, topographic and boundary surveys and mapping thereof. Mr. Schafer has over 55 years of professional civil engineering experience representing private sector clients and numerous public districts in the San Joaquin Valley. Mr. Schafer has served as the Watermaster/Secretary of the Tule River Association since 1962, is a member of the Tulare County Water Commission, the Coordinator of the Tule Basin Water Quality Coalition, and is currently coordinating the formation and implementation of the Sustainable Groundwater Management Act in the Tule Sub-Basin.

David De Groot Project Manager, Technical Lead 4Creeks, Inc.

Mr. De Groot graduated from Calvin College located in Grand Rapids, Michigan with his B.S. in Civil Engineering and is a registered civil engineer in the State of California. Mr. De Groot specializes in agriculture and water resource engineering, including hydrology, hydraulics, water distribution systems, canals, pipelines, waste management systems, irrigation systems, dairy design, and environmental permitting for agriculture and water related projects. Mr. De Groot has 13 years of professional engineering experience and represents many private clients and public districts within the Central Valley of California. Mr. De Groot is the Assistant Watermaster of the Tule River Association since 2009 and is the Technical Lead of the Tule Basin Water Quality Coalition.

Michelle Parker QA Manager, Laboratory Coordinator R.L. Schafer & Associates

Mrs. Parker has served as the Executive Assistant to R. L. Schafer and Office Manager of R. L. Schafer & Associates for 25 years, Treasurer of the Tule River Association with the responsibility for the preparation of all reports for the Tule River, along with preparation of

the Tule River Association Annual Reports. Mrs. Parker also serves as the Treasurer, Enrollment Administrator and Quality Assurance Manager for the Tule Basin Water Quality Coalition. As the QA Manager for the Coalition, Ms. Parker has the responsibility for maintaining and distributing the official approved QAPP.

**Belinda C. Vega, Laboratory Director
Program Manager, BSK Associates**

Ms. Vega is the Laboratory Director of BSK Associates' (**BSK**) analytical laboratory in Fresno, CA. Ms. Vega received her B.S. in Environmental Resources Engineering from Humboldt State University and has been with BSK Associates since 2018. Prior to working with BSK, Ms. Vega served as the V.P. of Operations for Torrent Laboratory. She has also served as General Manager for Test America and President of EMLab P&K. For the purposes of this QAPP, Ms. Vega will act as the Program Manager for the sampling and analytical services performed in accordance with this QAPP. Ms. Vega's responsibility in this role will be to understand the plan requirements and work in conjunction with the Coalition contacts to ensure those requirements are met by the primary and subcontract laboratories.

**Michael Ng, Quality Assurance Manager
QA Manager, BSK Associates**

Mr. Ng is the Quality Assurance (**QA**) Manager at BSK's Fresno Analytical Laboratory (BSK Labs). Mr. Ng received his M.S. Chemistry from California State University, Los Angeles, and has over 30 years of experience in environmental laboratory industry. He will be acting in the role of quality assurance to ensure that all data produced by BSK are of a known and documented quality, consistent with standard industry practices and the State's Environmental Laboratory Accreditation Program. Mr. Ng will be the primary point of contact for all matters related to the laboratory quality system and data quality concerns.

**Stephane Maupas, Project Management and Acquisition Manager
Project Manager, BSK Associates**

Mr. Maupas is the Project Management and Acquisition Manager at BSK's Fresno Analytical Laboratory (BSK Labs). Mr. Maupas received his B.S. Chemistry from California Polytechnic State University, San Luis Obispo, and has over 20 years of experience in environmental laboratory industry. He will be acting in the role of Laboratory Project Manager to ensure that each sampling and analytical event is performed in accordance with program requirements. Mr. Maupas will be the primary point of contact for the Coalition personnel, coordinating the field sampling events and analytical testing required by each monitoring event.

Contracted Laboratories

The **COALITION** has contracted with the following laboratories for chemical testing, toxicity testing, and sampling services. Sub-contracting laboratories are mentioned under each primary laboratory.

BSK Associates (**BSK**)

Fresno Analytical Laboratory
1414 Stanislaus St
Fresno, CA 93706
(559) 497-2888
(559) 485-6935 fax
www.bskassociates.com

BSK provides testing services for the chemistry and microbiology samples for Tule Basin Water Quality Coalition as well as the sampling services at all surface water monitoring sites.

Aquatic Bioassay and Consulting (**ABC**)

29 N. Olive St.
Ventura, CA 93001
(805) 643-5621
(805) 643-2930 fax
www.aquaticbioassay.com

ABC will provide the aquatic toxicity testing for the Coalition. ABC has been providing this service for the COALITION over the last several years either directly or indirectly when the district was part of the former Southern San Joaquin Valley Water Quality Coalition. ABC will serve in a subcontract role (**SUBCONTRACT LABORATORY**) to BSK.

In the event that BSK determines that the service provided by the SUBCONTRACT LABORATORY is inadequate to meet the data quality or scheduling needs of the COALITION, BSK may elect to redirect the aquatic toxicity testing to an alternate provider, namely, Pacific EcoRisk Laboratory. Similar to ABC Laboratory, Pacific EcoRisk is California ELAP certified and can perform aquatic toxicity testing that meets the data quality objectives of this QAPP.

Pacific EcoRisk Environmental Consulting and Testing (**PER**)

2250 Cordelia Road
Fairfield, CA 94534
(707) 207-7760
(707) 207-7916 fax
www.pacificcorisk.com

Should it become necessary to utilize any other subcontract laboratories other than ABC and PER, BSK will inform the COALITION as to the need for the change and provide a

letter for submission to the Regional Board to document the necessary deviation from the QAPP and to identify the new subcontract laboratories.

Laboratories used by the Coalition will be certified at a minimum under the California Environmental Laboratory Accreditation Program (**ELAP**). The laboratories listed in the QAPP will meet all Quality Assurance and Control requirements provided in this document. The selection of sub-contractors by a contracted lab must first be approved by the Coalition, and such sub-contractors must abide by the conditions set forth by the Regional Board and this QAPP document.

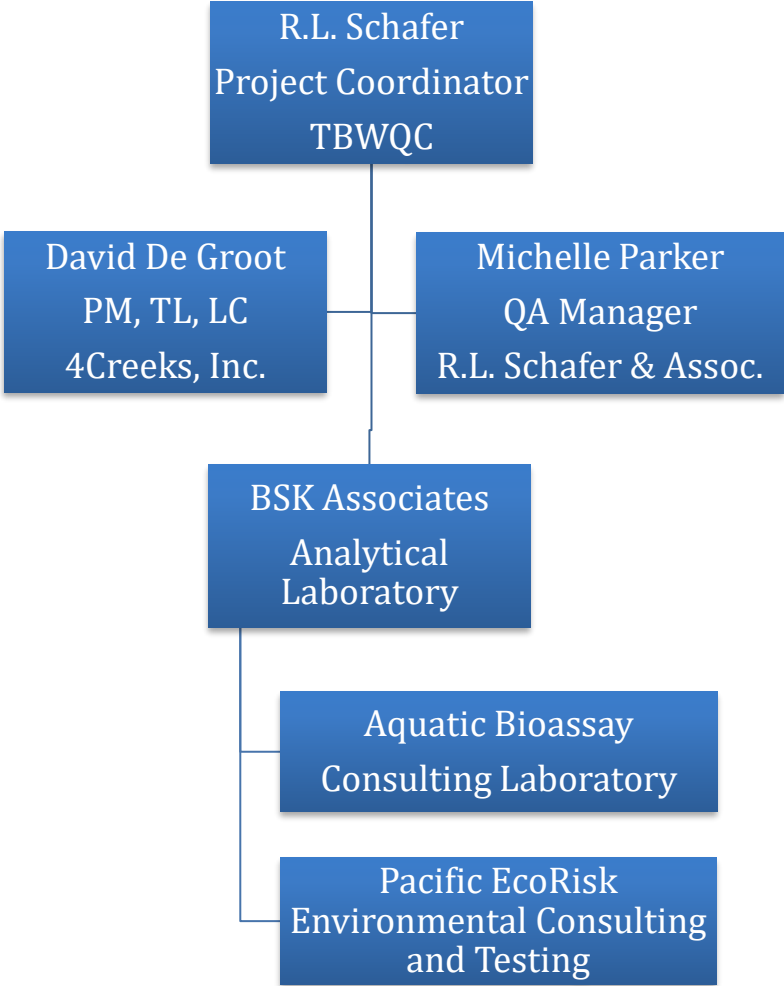


Figure 1. Organizational Chart

ELEMENT 5: PROBLEM DESCRIPTION AND BACKGROUND

Introduction

It is known that some waters of the State are negatively impacted by discharges from agricultural lands. Said discharges are likely to contain applied pesticides or chemical fertilizers that negatively impact the water quality and ecosystems present within the receiving waters. The TBWQC has conducted chemical and physical parameter testing of surface waters since 2004 on representative waterways within its boundaries, initially as part of the now dissolved Southern San Joaquin Valley Water Quality Coalition (SSJVWQC) and are currently under the California Regional Water Quality Control Board General Order R5-2013-0120.

The hydrology of the Coalition is one where surface water supplies are frequently limited, and when available in the case of Tule River, are only released from Success Reservoir to satisfy irrigation demands or flood-control. Groundwater is used by landowners where surface delivery infrastructure does not exist or when the public districts are unable to deliver irrigation water on the farmer's irrigation schedule.

This Plan is designed to monitor the constituents in Waters of the State, determine exceedances (if any), trace the source, under the Surface Water Monitoring Plan and the Groundwater Quality Trend Monitoring Workplan of the TBWQC, alter the Management Practices used to reduce/eliminate the exceedance. The Plan is further designed to provide groundwater quality (constituent) analyses as required by Order R5-2013-0120.

Project Objectives

In accordance with the requirements of the California Water Code, the Irrigated Lands Regulatory Program's Monitoring and Reporting Program Plan (MRP), the General Order objectives are to (1) categorize the current condition of the water of the state within the jurisdictional boundaries of the Coalition, (2) to identify any potential sources of pollutants that may contribute to the degradation of the water of the State, and, if identified, (3) to prevent further degradation (if any) of such water of the State as may be caused by irrigated agriculture through the implementation, where feasible, of management plans that prevent future negative impacts and eventual recovery of the waters to acceptable conditions that are protective of the identified beneficial uses.

Approaches Used

To achieve these objectives, the Coalition has implemented a Surface Water Monitoring Plan (SWMP) and a Groundwater Quality Trend Monitoring Workplan (GQTMW) with selected representative monitoring sites/wells within the TBWQC. Testing is done for physical and chemical constituents related to agricultural practices common to the region surrounding the monitoring site.

Surface water monitoring consists of monthly collection of samples at sites within natural channels that represent the beginning of irrigated agriculture, location of historic gaging stations, downstream of all sources of flow entering the waterway and other general conditions. When water is not present at the surface water sampling sites, monthly photo documentation of the monitoring sites are conducted. To maximize the occasions for surface water samples, Coalition personnel will monitor both the local agricultural irrigation schedules and the regional weather forecasts. During periods of active irrigation, regular stream flows or significant precipitation, the Coalition will conduct its monitoring events, but at the least monthly.

Groundwater monitoring consists of annual collection of samples from wells that are chosen to reflect the quality, as determined by the Coalition's Groundwater Quality Trend Monitoring Workplan (GQTMW) that employs wells in the upper most zone of first encountered groundwater as described in the Irrigated Lands Regulatory Program's MRP. Depth to groundwater measurements wells are conducted twice per year: during the Spring, normally during February for seasonal high data; and during the Fall, normally in October, for seasonal low data.

Regulatory Information

The Coalition covers essentially the center of the Tulare Lake Basin. The State has recognized that the conditions present within this Basin are distinctly different from the conditions found in the San Joaquin or Sacramento River Basins, and that the Tulare Lake Basin is closed and isolated from the San Joaquin-Sacramento River delta under normal hydrologic circumstances. As such, a separate basin plan was developed to address the Tulare Lake Basin.

Table 1 and Table 2 provide the Basin Plan Objectives (BPO) for surface water and groundwater, respectively, of the Tulare Lake Basin, as well as the spectrum of chemistries tested under the current monitoring and reporting program (MRP). Some of the BPO's for water quality are derived from standards in Title 22 of the California Code of Regulation. Many of the constituents listed do not have official numerical limits in place, although the interpretation of the narrative would lead to a zero tolerance.

Table 1: MRP Chemistries Tested for and BPOs for Tulare Lake Basin Surface Waters

CONSTITUENT	BASIN PLAN OBJECTIVE	UNITS	CONSTITUENT	BASIN PLAN OBJECTIVE	UNITS
Field Measurements			Pesticides and 303(d) Parameters		
Flow	-	cfs	2,4-D Acids & Salts	0.45	ug/L
EC	700	umhos/cm	Acetamiprid	0.01	ug/L
Temperature	Variable	°C	Aldicarb	3	ug/L
pH	6.5 – 8.3	pH units	Atrazine	1	ug/L
Dissolved Oxygen	5-7 (W/C)	mg/L	Azinphos-methyl	0.01	ug/L
			Captan	0.01	ug/L
Drinking Water			Carbaryl	2.53	ug/L
E. Coli	235	MPN/100mL	Carbofuran	0.5	ug/L
TOC	NA	mg/L	Chloropicrin	8.5	ug/L
			Chlorothalonil	0.025	ug/L
General Physical			Chlorpyrifos	0.015	ug/L
Hardness	NA	mg/L	Clothianidin	0.01	ug/L
TSS	NA	mg/L	Cyanazine	1	ug/L
Turbidity	Variable	NTU	DDD	0.001	ug/L
			DDE	0.001	ug/L
Metals			DDT	0.001	ug/L
Arsenic	10	ug/L	Demeton-s	NA	ug/L
Arsenic (Dissolved)	150	ug/L	Diazinon	0.1	ug/L
Boron	700	ug/L	Dichlorvos	0.085	ug/L
Cadmium	Variable	ug/L	Dicofol	NA	ug/L
Copper	Variable	ug/L	Dieldrin	0.056	ug/L
Lead	Variable	ug/L	Dimethoate	1	ug/L
Molybdenum	10	ug/L	Disulfoton	0.05	ug/L
Nickel	Variable	ug/L	Diuron	2	ug/L
Selenium	5	ug/L	Endrin	0.036	ug/L
Zinc	Variable	ug/L	Glyphosate	700	ug/L
			Imidacloprid	0.002	ug/L
Nutrients			Linuron	1.4	ug/L
Ammonia-N	0.025	mg/L	Malathion	0.1	ug/L
Nitrate-N	10	mg/L	Mancozeb	1	ug/L
Nitrite-N	1	mg/L	Methamidophos	0.35	ug/L
Orthophosphate-P	NA	mg/L	Methidathion	0.7	ug/L
			Methiocarb	5	ug/L
Water Toxicity			Methomyl	0.52	ug/L
Ceriodaphnia dubia			Methoxychlor	0.03	ug/L
Pimephales promelas			Methyl Parathion	0.08	ug/L
Selenastrum capricornutum			Molinate	13	ug/L
Sediment Toxicity					
Hyalella azteca					

CONSTITUENT	BASIN PLAN OBJECTIVE	UNITS	CONSTITUENT	BASIN PLAN OBJECTIVE	UNITS
Pesticides and 303(d) Parameters			Pesticides and Sediment Parameters		
Norflurazon	0.011	ug/L	Bifenthrin	-	ng/g
Oryzalin	0.3	ug/L	Chlorpyrifos	-	ng/g
Oxamyl	50	ug/L	Cyfluthrin	-	ng/g
Oxyfluorfen	0.003	ug/L	Cypermethrin	-	ng/g
Paraquat	3.2	ug/L	Esfenvalerate	-	ng/g
Paraquat Dichloride	0.19	ug/L	Fenpropathrin	-	ng/g
Pendimethalin	0.07	ug/L	Lambda cyhalothrin	-	ng/g
Phorate	0.7	ug/L	Permethrin	-	ng/g
Phosmet	140	ug/L	Piperonyl Butoxide	-	ng/g
Pyraclostrobin	0.0029	ug/L			
Pyrethrins	0.1	ug/L			
Pyridaben	0.01	ug/L			
Simazine	4	ug/L			
Tebuconazole	0.0102	ng/L			
Thiobencarb	3.1	ng/L			
Trifluralin	5	ug/L			
Ziram	1	ug/L			

Table 2: MRP Chemistries Tested for and BPOs for Tulare Lake Basin Ground Waters

CONSTITUENT	BASIN PLAN OBJECTIVE	UNITS
Field Measurements		
EC	900-1,600	umhos/cm
Temperature	Variable	°C
pH	6.5 - 8.3	pH units
Dissolved Oxygen	5-7 (W/C)	mg/L
Inorganic Chemicals		
Nitrate as Nitrogen (N)	10	mg/L
Total Dissolved Solids (TDS)	500-1,000	mg/L
General Minerals		
Anions		
Carbonate (as CaCO ₃)	NA	mg/L
Bicarbonate (as CaCO ₃)	NA	mg/L
Chloride	500	mg/L
Sulfate	500	mg/L
Cations		
Boron	NA	ug/L
Calcium	NA	mg/L
Sodium	NA	mg/L
Magnesium	NA	mg/L
Potassium	NA	mg/L

Program Background

Surface Water Monitoring

The requirement for a comprehensive testing program as part of the Agricultural Discharge Waiver (now Irrigated Lands Regulatory Program) was put in place July 2003 with the installation of a new discharge waiver. The program was revised in January 2008 to incorporate additional requirements for the selection of sample sites and the development of management plans, if triggered. Most recently, a new order (R5-2013-0120) adopted by the RWQCB in September 2013 for the Tulare Lake Basin which has led to the dissolution of the SSJWQC and the establishment of numerous coalitions, each focus on those concerns specific to the subbasin of the former combined coalitions.

Limited laboratory testing (water column toxicity) along with physical parameter measurements (dissolved oxygen [DO], electrical conductivity [EC], pH, and temperature)

were started on a systematic schedule in 2004. The water column toxicity tests included an evaluation of algae growth (*Selenastrum capricornutum*), fathead minnow (*Pimephales promelas*), and water flea (*Ceriodaphnia dubia*) survival. Each represents an important step in the aquatic food chain and when combined with the physical parameters, would be indicative of some form of water contamination. The laboratory test results for exceedances were transmitted to the Regional Board as an indicator of whether an exceedance existed in the Waters of the State within the Coalition.

Starting in June 2006, the testing of surface waters was expanded to include general chemistry (dissolved metals), nutrients, and pesticides that the Regional Board felt were important, and were consistent with other testing done under the Surface Water Ambient Monitoring Program (SWAMP). The surface water monitoring program was revised in 2008 to give the Coalitions greater flexibility in selecting the sampling sites, frequency of sampling, and constituents tested for as long as each change from the previous program could be adequately justified. Sampling of surface waters was increased to once per month for all monitoring sites. Reporting requirements under the program were also adjusted to quarterly reports of accumulated data (in a SWAMP compatible format) and one annual report of the data collected instead of two reports per year. The increased frequency of data reporting was to help the Regional Board see trends sooner, and the single report by the Coalitions was to help reduce costs.

The annual testing of surface waters was categorized as either Assessment or Core monitoring, with differing requirements for each. Surface water monitoring assessment sites are those sites that are new to the program and thus have no historical data associated with them.

Surface water monitoring core sites are those with historical data and are used for the monitoring of trends within the waterways of the Coalition. Both type of sites are monitored intensely for a one-year period, then only lightly sampled (lower chemistry test requirements) for the following two years, unless problems are detected during the first year.

A third type of surface water monitoring site to be monitored is a Special Project Monitoring Site, where research into a specific question is undertaken. Once sufficient data has been collected at such a site, it can be discontinued if no issues were identified.

Groundwater Quality Trend Monitoring

Previous to the implementation of the IRLP, monitoring of groundwater quality was performed under two Regional Water Quality Control Board programs: the Dairy General Order R5-2007-0035 adopted in May of 2007, and the individual Waste Discharge Requirements (WDR); along with two State Water Resources Control Board programs for the Division of Drinking Water and the Groundwater Ambient Monitoring and Assessment Program (GAMA), expanded in 2007. With the adoption of the ILRP General Order R5-2013-0120 by the RWQCB in September 2013, monitoring of waters of the State was expanded to include the determination of groundwater quality through the evaluations consisting of 1)

Groundwater Quality Assessment Report (GAR), 2) Management Practice Evaluation Program (MPEP), and 3) Groundwater Quality Trend Monitoring Program (GQTMP).

The purpose of the GAR was to provide a technical basis for the scope and level of effort for implementation of the of the General Order's groundwater monitoring and implementation provisions, accomplished by an assessment of all available, applicable, and relevant data and information to determine the high and low vulnerability areas where discharges from irrigated lands may result in groundwater quality degradation. At a minimum, the GAR is required to be reviewed and updated by the Coalition on a 5-year basis incorporating new information and data. The GAR provides the necessary foundation for design of the MPEP and GQTMP and identifies the areas where a GQTMP must be implemented. In January of 2016 the TBWQC received conditional approval on the Coalition's GAR.

The purpose for developing the MPEP was to evaluate the effectiveness of current agricultural management practices for protection of groundwater quality, consistent with the General Order requirements. The TBWQC elected to participate in the group option for developing the Management Practice Evaluation Workplan required under the General Order. The participants of the group plan include all of the Coalitions within the Tulare Lake Basin.

The GAR's initial groundwater assessment is the basis for development of the GQTMP. With the findings and data gaps identified in the GAR the TBWQC developed their Groundwater Quality Trend Monitoring Workplan (GQTMW) to further investigate the conditions of the existing groundwater quality and develop a plan for determining trends in groundwater quality for evaluation of the effects of irrigated agriculture on groundwater quality. The TBWQC received conditional approval from the Regional Board on their Groundwater Quality Trend Workplan in September 2018.

Beginning in the Fall of 2018, the TBWQC was required to begin collecting groundwater quality samples from the monitoring network included in the GQTMW and annually in the summer thereafter. Constituents required to be sampled for annually by the MRP consist of field-tested physical parameters (electrical conductivity [EC], pH, dissolved oxygen [DO], temperature) and laboratory tested inorganic chemicals (nitrate as nitrogen). In addition to the annually tested constituents, the MRP requires laboratory tested constituent of total dissolved solids [TDS], general mineral anions (carbonate, bicarbonate, chloride and sulfate) and cations (boron, calcium, sodium, magnesium and potassium) be tested initially and once every 5 years thereafter.

Decisions Made with Information Obtained from Monitoring

The purpose of any testing program is to detect a constituent exceedance in the waters of the State as the first step. The second step is to evaluate the seriousness of the detection. Once detection has been made, the approach of the Coalition is to trace the constituent exceedance to its potential source. This includes a physical survey of the

waterway for possible points of entry of applied irrigation waters (pipes, culverts, canal gates), evaluation and documentation of cropping patterns, and the eventual tracking of the application with the local agricultural commissioner. Once the likely source of the constituent exceedance has been identified, contact with the suspected grower(s) would begin so as to prevent future occurrences. A wide range of options are available, including improved irrigation waters management, changes in chemicals applied, changes in application methods, or any other procedure that would prevent the offsite movement of the detected constituent.

The data from the individual surface water and groundwater sampling points will be assessed according to the following beneficial use criteria:

Table 3: Coalition Sampling Points – Data Evaluation Criteria

Site name	Beneficial Use
Deer Creek at Road 120	Freshwater Habitat
Deer Creek at Road 176	Freshwater Habitat
Deer Creek at Road 248	Freshwater Habitat
Porter Slough near Road 192	Freshwater Habitat
Tule River at North Fork Road 144	Freshwater Habitat
Tule River at Road 92	Freshwater Habitat
White River at Road 208	Freshwater Habitat
GQTMP Supply Wells	Municipal & Domestic Supply

ELEMENT 6: PROJECT DESCRIPTION***Surface Water Sample Sites Description***

The Coalition has identified seven natural channel locations where surface monitoring will be conducted under the monitoring program. The locations and schedule were identified as being the most representative of the surface waters within the Coalition boundaries. For additional details concerning the choice of the individual monitoring locations and schedule, please refer to the TBWQC Surface Water Monitoring Plan (8/4/14) and the associated addendum (2/9/15).

The monitoring locations are as follows:

1. Deer Creek At Road 120 – Pixley, CA Site Description

The Deer Creek at Road 120 station is located approximately 3.5 miles southwest of Pixley, CA. The land use surrounding this location is predominantly irrigated agriculture, ranging between different row crops and permanent crops. The station is located within the Pixley Irrigation District.

2. Deer Creek At Road 176 – Pixley, CA Site Description

The Deer Creek at Road 176 station, a stream gaging station, located approximately 6 miles southeast of Pixley, CA. The land use surrounding this station is predominantly irrigated agriculture, consisting of permanent crops and limited row crops. This station is located within the Saucelito Irrigation District.

3. Deer Creek At Road 248 – Terra Bella, CA Site Description

The Deer Creek at Road 248 station is located where the foothills of the Sierra Nevada Mountains meet the flat lands of the basin, approximately 2.5 miles northeast of Terra Bella, CA. At this location, the land use is primarily range land for cattle grazing. This location is not within an Irrigation District boundary.

4. Porter Slough Near Road 192 – Porterville, CA Site Description

The Porter Slough Near Road 192 monitoring station is located approximately 4.5 miles northwest of the City of Porterville. Porter Slough is a natural distributary of the Tule River with the head works approximately 2.5 miles downstream of Success Dam. The Porter Slough channel traverses 12 miles through the City of Porterville and Porterville Irrigation District prior to terminating into a Lower Tule River Irrigation District (LTRID) canal. The sampling point is located within Porter Slough upstream of the discharge into the LTRID canal. This monitoring station is located within the Porterville Irrigation District.

5. Tule River At Road 144 (North Fork) – Woodville, CA Site Description

The Tule River at Road 144 station is located approximately 3.5 northwest of Woodville, CA. The Tule River bifurcates at Road 192 into North and South Fork channels.

Downstream on the South Fork at Road 168, the South Fork further bifurcates into a Middle Fork and South Fork. At Road 144, the South Fork and Middle Fork rejoin as the South Fork and at Road 104 the South Fork and North Fork rejoin back into one main Tule River channel that continues to the Tulare Lake Bed. The Tule River at Road 144 monitoring site is located along the North Fork of the Tule River, just downstream of where a LTRID canal discharges CVP water from the Friant-Kern Canal into the Tule River. The land uses surrounding this station are predominantly agriculture, ranging from row crops to different permanent crops and is located in the northern central portion of Lower Tule River Irrigation District (LTRID).

6. Tule River At Road 92 - Tipton, CA Site Description

The Tule River at Road 92 station is located approximately 4 miles northwest of Tipton, CA. The Tule River at Road 92 station is located downstream of where the North Fork, Middle Fork, and South Fork all merge together forming a single Tule River Channel to the Tulare Lake Bed. This station is surrounded by irrigated agriculture of row crops and several permanent crops within the LTRID.

7. White River At Road 208 - Earlimart, CA Site Description

The White River at Road 208 station is located approximately 4 miles southwest of Ducor, CA. The monitoring station is located above the beginning of irrigated agriculture with the land use below this station planted predominantly with various permanent crops. The station is located within the Delano Earlimart Irrigation District (DEID).

Maps and coordinates of the sample site locations are included in Element 10 (Sampling Process Design / Monitoring Points).

Groundwater Sample Sites Description

An initial goal of the selection of groundwater sampling sites was to identify existing irrigation/domestic wells of first encountered groundwater that have adequate physical information to ensure the trends analyzed over time are reliable. The spatial coverage for the selection from existing groundwater wells of the monitoring well network is proposed to be four wells per township with one well for each nine square miles of the Township. In addition, for each “selected” well, a back-up or “secondary” well will be identified and utilized in case the selected well is damaged or is no longer in production. During the initial field verification and monitoring, the selected well will be included in the program to establish baseline groundwater depth and quality data. After the initial monitoring, only the selected well will be sampled annually. If the selected well is damaged permanently or is no longer in use, a replacement for the selected or secondary well will be identified at that time. The TBWQC covers in whole or in part twenty-nine (29) townships, identified as follows:

1. Township 21 South, Range 25 East
2. Township 22 South, Range 25 East
3. Township 23 South, Range 25 East

4. Township 23 South Range 23 East; those four townships include the communities of Tipton, Pixley, Earlimart and Alpaugh
5. Township 20 South, Range 27 East
6. Township 21 South, Range 27 East
7. Township 23 South, Range 27 East
8. Township 24 South, Range 27 East; those four townships cover the City of Porterville and the communities of Strathmore, Terra Bella, Ducor and Richgrove
9. Township 21 South, Range 26 East; covers the communities of Woodville and Poplar
10. Township 24 South, Range 24 East; covers the small community of Allensworth
11. Township 24 South, Range 25 East; covers urban sprawl of the community of Earlimart
12. Township 24 South, Range 26 East
13. Township 21 South, Range 28 East
14. Township 21 South, Range 29 East
15. Township 22 South, Range 28 East
16. Township 22 South, Range 27 East
17. The portion of the Tule Basin in Township 20 South, Range 26 East
18. Township 22 South, Range 26 East
19. Township 23 South, Range 26 East
20. The portion of Township 25 South, Range 26 East; covered by the Delano-Earlimart Irrigation District in Kern County
21. The portion of Township 21 South, Range 23 East
22. Township 22 South, Range 23 East
23. Township 24 South, Range 23 East
24. Township 21 South, Range 24 East
25. Township 22 South, Range 24 East
26. Township 23 South, Range 24 East
27. Township 23 South, Range 28 East
28. Township 24 South, Range 28 East
29. The portion of Township 22 South, Range 29 East

Map of the Tule Basin Water Quality Coalition Boundary is included in Element 10.

Summary of Work Performed for Surface Water and Groundwater Sampling

Sampling Procedures for Surface Water

The following is a description of the surface water sampling techniques to be used under this QAPP. The basic processes used to collect samples will remain unchanged from the previous MRP/QAPP although incorporation of the frequency of monitoring will require a more real-time determination of the sampling windows. Sampling, site photographs and reports will continue on a monthly basis for each surface water monitoring site.

Prior to the sampling event, physical parameter equipment will be recalibrated using known laboratory standards and according to the manufacturer's instructions. This equipment includes pH meters, EC meters, and DO meters. Known standards are brought to the field to recheck the calibration (pH, EC) at each site prior to sample collection.

Field samples of the water are collected in bottles provided by the laboratory (chemistry) or in one-gallon amber jugs specially purchased for the sampling event (water column toxicity). The containers are marked with site identification description, date and time of collection along with any preservative added by the lab on water resistant labels. Photo documentation is performed at each surface monitoring site each month.

Glass bottles are wrapped to prevent breakage during transport to the collection sites, and after collection, "blue" or gel ice packs are placed with the samples to reduce the sample temperature as low as possible in the field. Once all sampling points are collected, the samples will be transported to a location where they will be repacked for transportation to the laboratory. Samples will then be packed in "wet" ice and delivered to the laboratory on the same day of collection. The samples are packed with sufficient ice to lower the sample temperature to $\leq 6^{\circ}\text{C}$ but not frozen.

Chains of custody are filled out with matching information (sample ID, sample date and time, site, and tests required) and are given to either the courier or the lab representative when the samples change hands.

The hold time for the water column toxicity samples is 36 hours, and the samples are shipped no later than the morning after collection. Ice levels are rechecked prior to shipment.

Sampling Procedures for Groundwater

The physical parameter equipment shall be calibrated at the beginning and once during each sampling day in accordance with the equipment manufacturer's specifications, as outlined in the instruction manual for the EC meter used. This equipment includes pH meter, EC meter, and DO meter.

Water supply wells shall be sampled by purging the well for a period of time adequate to purge the pump riser pipe. If the well is currently pumping, the sample may be taken

without purging the well. Water samples shall then be collected from the discharge point nearest the well head. Samples shall be collected directly into laboratory-prepared bottles. Samples may not be taken from any location after any treatment of the water for domestic use, such as from a faucet within the house.

Field measurements of temperature, pH, dissolved oxygen (DO), Electrical Conductivity (EC), will be conducted and recorded of aliquots of groundwater and not determined in the laboratory. Field water quality measurements and instrument calibration details will be recorded on the Well Sampling Record.

Efforts will be made to handle, store, and transport supplies and samples safely. Exposure to dust, direct sunlight, high temperature, adverse weather conditions, and possible contamination shall be avoided. Immediately following collection, samples shall be placed in a clean chest that contains ice or “blue” ice, and transported to the subcontracted laboratory as soon as practical. Samples should be chilled at 4°C to prevent degradation.

After samples have been collected and labeled, they shall be maintained under chain-of-custody procedures. These procedures document the transfer of custody of samples from the field to the laboratory. Each sample sent to the laboratory for analysis shall be recorded on a Chain of Custody record, which will include instructions to the laboratory for analytical services.

If the samples are to be left at a BSK sample drop-off location, the original chain-of-custody shall be sealed inside a plastic bag within the ice chest, and the chest shall be sealed with custody tape which has been signed and dated by the last person listed on the chain-of-custody. The laboratory shall sign as a receiver once samples are received.

Analytical Procedures

Once received by the laboratory, the samples will be checked for temperature and preservation requirements. Bottles will be inspected for integrity and any deviations noted as part of the sample conditions on receipt documentation. Any anomalies will be communicated to the Project Coordinator and corrective actions taken as required. At a minimum, the discrepancies will be noted as part of the Case Narrative included with the laboratory results.

Samples will be processed according to the test methods required by the General Order. All laboratory data will undergo a tertiary review process to ensure that the data meets the requirements of the method and the data quality objectives of the Order. The Laboratory Project Manager will create the Certificate of Analysis (Report). A case narrative will be written to identify any anomalies, QC failures or other material issues that do not meet the quality objectives of the Order.

A preliminary report will be provided to the Coalition within ten (10) business days of sample collection, and will include all partial laboratory results that are reviewed and

completed by then. The preliminary and final reports will be sent via email to the Project Coordinator and QA Manager.

Finally, the laboratory will prepare the required electronic data deliverables (EDD) as required by the MRP of the Order. Prior to delivery to the Project Coordinator, the laboratory personnel will evaluate the EDD using the SWAMP data integrity validation program as provided by the California Environmental Data Exchange Network (CEDEN) for surface water analysis results or the GeoTracker Electronic Submittal of Information (ESI) "Check EDD" tool for groundwater analysis results. Any critical failures observed will be addressed and the EDD will be reevaluated. Once complete with no critical errors, the EDD will be sent to the Project Lead along with a copy of the error log returned by the CEDEN or GeoTracker validation program.

Resource and Time Constraints

There are no significant resource constraints associated with the Surface Water Monitoring Plan (SWMP) or the Groundwater Quality Trend Monitoring Workplan (GQTMW). Both the Coalition and the laboratories have adequate resources to effectively perform the tasks required under the Plan and the General Order.

The responsibility of surface water sampling will be that of the primary laboratory, BSK. BSK has offices in the Fresno and Bakersfield areas. The Fresno location will be the primary respondent and operate as the base for crew and the sample receiving location. Multiple personnel will be trained on the sample collection procedures to ensure that BSK can respond to the sampling events with a minimal amount of notification. In the event of a scheduling conflict, staff from BSK's Bakersfield location will be dispatched to collect samples for the Coalition.

Coalition staff is responsible for collecting groundwater samples and have multiple staff members stationed in Visalia trained to use field instruments and procedures required for sample collection. The Fresno-based laboratory has extensive equipment and personnel to accommodate the water quality analysis workload generated under the SWMP and GQTMW.

Time represents the most significant restraint for both surface water and groundwater monitoring. The sample collection will require the close coordination of both Coalition and Laboratory personnel. Coalition personnel will closely monitor both the scheduled irrigation program and the regional weather forecast as well as sample date coordination with well owners to ensure a timely notification of sampling requirements. Laboratory and Coalition personnel will have the required water sampling equipment and materials (e.g. field instruments, sample containers, ice chests, etc.) on hand as a matter of practice to minimize the time requirements for the commencement of field sampling. The primary laboratory, BSK has a sample drop-off location in Visalia that facilitates the transportation of samples.

ELEMENT 7: QUALITY OBJECTIVES AND CRITERIA

The primary goal of any sampling and analyses program is to produce data that is of known and documented quality and is suitable for its intended use. The data generated under the TBWQC's SWMP and GQTMP will be used to make decisions regarding water quality in the Coalition, ensuring the preservation of the environment and the protection of human health. To that end, the data quality objectives set forth in the SWMP and GQTMW are established to ensure that (1) the collection of samples are representative of the environmental conditions associated with agricultural activities, that (2) the samples are handled and processed in a manner consistent with the requirements of the methods used and the practices set forth in this QAPP, and that (3) the data generated from the project are of sufficient quality to make sound decisions regarding the impact of agricultural activities on the waters of the State.

Performance Criteria Goals

The success of any given monitoring event will be determined based on the characteristic of completeness. The quality of completeness is a function of the number of successful checks or evaluations made on a project versus the total number of observations made. The overall completeness goal for each monitoring event is 90%. A discussion of completeness for both the sampling and the analytical portions of the SWMP and the GQTMW will follow below.

Quantitation Limits

The data generated as part of the SWMP and the GQTMW must be at a level of sensitivity low enough to detect and quantify constituents of concern at levels needed for preservation of the environment and human health. With that, the majority of the chemical testing is done to the parts-per-billion level.

Chemistry

The laboratory will establish reporting limits (RLs) at a level at or below the requirements of the General Order. These RLs will be based on a calibration point at or below the equivalent sample concentration. The laboratory will not report any value below the RL without qualification as an estimated value. All reported results will be bracketed by a calibration point.

To determine the low value at which the laboratory can detect the presence of a target analyte, the laboratory will conduct a Method Detection Limit (MDL) study in accordance with the procedure set forth in 40 CFR Part 136 Appendix B. This value is the lowest concentration at which the lab can state the compound is present with 99% confidence that it is truly non-zero.

Some methods are not amenable to conducting method detection limits studies. These methods are identified in Table 8 with a “-“ in the column labeled MDL. This table reflects the MDLs in existence at the time this QAPP is approved. As per the requirements of the Order, the MDLs will be regenerated or verified by the laboratory at least every two years or when a material change is made in the method or equipment used to generate the original MDL study.

To provide the program with the most sensitive data possible but with the statistical confidence that a result is not a false positive, the laboratory will report results that exist between the MDL and the RL. As these values are outside of the calibration range of the equipment used, there exists some uncertainty as to the accuracy of the result return. For values reported between the MDL and RL, the laboratory will identify these as estimated values by applying a qualifier to indicate the uncertainty of the measurement (e.g. “J-Flagged”).

Toxicity

Water toxicity tests will be considered significant at the 95% level of significance. TIEs will not be initiated until 50% survival or below is reported. Phase I TIE testing, along with a retest of the failed test, will begin as quickly as practical by the laboratory.

Table 8 summarizes the analytes, ILRP PQLs, method detection limits and reporting limits for this project.

Quality Control Measurements

Every effort will be made to provide quality from both the field sampling activities and from the fixed facility laboratory activities. Field and laboratory personnel are trained on proper sampling and analysis techniques appropriate to the tasks performed. All activities will be performed in accordance with established standard operating procedures (SOPs). See the Table 6 for listing of the applicable SOPs.

The results of the field and analytical activities will be gauged on a number of characteristics. Those characteristics are:

1. **Representativeness**. The monitoring sites selected for the SWMP and GQTMP by the Coalition will be indicative of the water quality within the Tule Basin. The surface water monitoring sites selected by the Coalition reflect the quality of the flows into and out of the Coalition. Samples will be collected based on real-time assessments of water flows, including those associated with storm events. Samples will be handled to ensure they maintain the conditions at they exist in the field and will be released to the laboratory in a timely manner to ensure that hold times are met.

The monitoring sites selected for the GQTMW by the Coalition must be consistent with and indicative of the water quality relevant to irrigated agriculture. The groundwater

monitoring wells selected by the Coalition represent both high and low vulnerability areas, as well as areas contributing significant recharge to urban and rural communities where groundwater serves as a significant source of supply. Groundwater sampling will be collected on an annual basis. Samples will be handled to ensure they maintain the conditions at they exist in the field and will be released to the laboratory in a timely manner to ensure that hold times are met.

2. Comparability. All samples are to be collected in the same manner, from approximately the same location at each monitoring site. All conditions will be maintained as consistent as possible to ensure that testing performed across multiple monitoring events is comparable with variation only due to field conditions. Furthermore, tests used by the laboratory will be in accordance with the General Order requirements to ensure comparability to historical data generated for each of the sampling locations.
3. Sensitivity, Contamination, Accuracy, Recovery and Precision is determined based on the performance of the method on one or more quality control indicators.

Sensitivity is an assessment of the ability of the method to detect the analytes of interest at levels that are significant to the Plan. Numerous factors can affect sample results such that the reporting limits would need to be elevated. These factors include dilutions due to target or non-target interferences, insufficient sample volumes, internal standard suppression, etc. Sensitivity will be assessed by comparing the Order required reporting limits to those actually observed for all samples.

Contamination is an assessment of the field and laboratory background by the examination of a blank matrix known to be free of contaminants. The blank matrix (Method Blank) is carried through the entire analytical process and then assessed for the presence of the target constituent. The presence of such constituents in the blank indicates that the field conditions or laboratory background may be responsible for the presence of a target constituent in the sample.

Accuracy is the ability of the method to generate a result within a prescribed range of its actual true value. For the test methods employed in this Plan, accuracy will be determined based on the use of a standard reference material (SRM) or Laboratory Control Sample (e.g. LCS, Blank Spike) that is free of interferences.

Recovery is the ability of the method to produce an accurate result given the potential interferences of a sample matrix. This is accomplished by fortifying a sample matrix with a small amount of the target compounds. The fortified matrix (or matrix spike [MS]) is carried through the analytical process to determine if the sample matrix somehow interferes with the method itself, either via suppression or enhancement of the matrix spike result.

Precision is the ability of the method to reproduce the same result within a prescribed acceptance range. For the test methods employed, precision will be assessed by the

analysis of a Laboratory Control Spike Duplicate, a Matrix Spike Duplicate or a Laboratory Sample Duplicate. The laboratory duplicate differs from a field duplicate in that the lab duplicate will be a secondary aliquot taken from the same container as the parent sample. A field duplicate is a second sample collected from the source and is treated as a separate unique sample that is “blind” to the laboratory.

4. **Completeness.** Completeness will be determined based on the measurement of the amount of valid data obtained per monitoring event (by site) versus the amount planned. The target of the Plan is to achieve 90 percent completeness at each event. Efforts to prevent sample loss include careful packaging of the sample for transport, and collection of adequate volumes for analysis, laboratory losses (errors, QC failures, and equipment failure). The laboratory shall determine the volumes required for the tests requested, and it is assumed that this final volume contains sufficient surplus to account for laboratory issues. As such, they have specified or provided the necessary containers for the sampling collection process.

Completeness will be determined at two levels: Field and Transport, and Laboratory with levels reported within each quarterly report. As BSK does the surface water sampling for the Coalition, the calculation of completeness will be performed by them. The following describes the Completeness calculation to be used.

Field and Transport completeness will include: completion of the site inspection report elements as specified on the Field Data Sheet, results of field instrument calibration checks, actual test results for physical parameters, completion of the Chain of Custody with the requested analyte list with no broken sample containers, and all samples received within temperature requirements. Chain of Custody forms (Appendix A.1) are provided by the lab and are pre-populated to include the analyses requested as determined by the Core vs. Assessment sampling schedule. The samples are inspected prior to packing with ice for breakage. Bottle counts are done when the labels are affixed to the containers. The Field and Transport evaluation program ends with the signed Chain of Custody, the reporting of the conditions of the samples as they are unpacked by the lab. Laboratory failures (e.g. breakage of sample container, samples received out of hold time, temperature exceedance, etc.) will be documented. All other measures beyond this point are associated with the Laboratory Completeness assessment.

Photo documentation shall constitute 100 percent Completeness for those times when no sample water is available at surface water monitoring sites.

The logbook sheets used for documentation of the Field and Transport portion of the monitoring event is included in Appendix A.2. An example of the spreadsheet used for the determination of the Field and Transport completeness is provided in Appendix A.4.

Completeness for the Field and Transport activities will be determined based on the number of assessment points satisfying the expected criteria versus the total number assessed per sample site (22 individual assessment criteria per location).

Laboratory Completeness is achieved via an exhaustive examination of the results of both, field samples and the quality control indicators for each of the laboratory analyses. The laboratory completeness assessment is based on the characteristics of laboratory data listed above: sensitivity, contamination, accuracy, recovery and precision.

Completeness for the Laboratory activities will be determined based on the number of sample results that are not materially impacted by data quality issues. The calculation is the number of unaffected sample results versus the total number of data points generated for the sampling event.

An example of the spreadsheet used in the determination of Laboratory Completeness is included in Appendix A.3.

Table 4: Data Quality Objectives -

Measurement or Analysis Type	Sensitivity	Contamination	Accuracy	Recovery	Precision	Completeness
Physical Parameters (EC, pH, DO, temp)	X		X		X	X
Toxicity	X	X	X	NA	X	X
Pathogens	X	X			X	X
Nutrients/Anions	X	X	X	X	X	X
Carbonate/Bicarbonate Alkalinity	X	X	X		X	X
TDS	X	X	X		X	X
TSS	X	X			X	X
Metals	X	X	X	X	X	X
Carbamates	X	X	X	X	X	X
Organochlorines	X	X	X	X	X	X
Organophosphates	X	X	X	X	X	X
Pyrethroids	X	X	X	X	X	X
Herbicides	X	X	X	X	X	X

ELEMENT 8: SPECIAL TRAINING NEEDS / CERTIFICATIONS

As of this time, there are no Coalition staff members with specialized training in chemistry or laboratory procedures, outside of the coursework taken as part of their general educational curriculum. BSK personnel involved in the project have been performing sample collection procedures for many years and are familiar with the maintenance and calibration of the equipment used and the sampling techniques involved. Technical questions are fielded by the contracted labs and their sampling crew.

BSK's Quality Assurance Manager is responsible for the oversight of training. The QA Manager will ensure that adequate training is provided to the laboratory personnel on the requirements of this Program. The training will consist of both written review and hands-on training, all documented and contained within the Laboratory's record keeping system. The training files are maintained by the Laboratory's Quality Assurance Department.

BSK's field technicians undergo initial training and annual refresher training thereafter on proper sample collection techniques for both water and sediment. Initial training consists of a review and acknowledgement of understanding of the laboratory's standard operating procedure on sample collection. This is followed by hands on sample collection working in conjunction with one of BSK's experienced samplers. This hands-on training will continue until the trainer witnesses and documents the satisfactory understanding demonstration of proper technique. Once the Field Technician has demonstrated sufficient knowledge and understanding of the project, the training will be documented and included in the laboratory's training records. The field technicians are trained according to the following SOPs: Field Sampling from Streams, Rivers and Canals (SR-SP-0015), and Safety for Stream and Canal Sampling (SF-SP-0010).

Coalition field technicians undergo an initial training on proper sample collection techniques for groundwater wells. Initial training consists of a review and acknowledgement of understanding of standard operation procedures on groundwater sample collection. This followed by a hands-on sample collection working in conjunction with one of BSK's experienced samplers. This hands-on training will continue until the trainer witnesses and documents the satisfactory understanding demonstration of proper techniques.

BSK's Project Manager will undergo initial training on the details of the QAPP and other project requirements. The training will be conducted by the Laboratory Program Manager or his designee. The training will consist of a reading of the QAPP and a follow up review with the Project Manager. Following this training, the first work order will be reviewed by the Project Manager as well, both on the initial receipt of samples and also at the time of reporting. This final stage of training will include a review of the final work product, the case narrative, the field logs and any other program requirements associated with the QAPP. Once the BSK Project Manager has demonstrated sufficient knowledge and understanding of the project, the training will be documented and included in the laboratory's training records.

ELEMENT 9: DOCUMENTS AND RECORDS

Record keeping is a critical component to any research project. The data collected by the Coalition is maintained in multiple locations. Each lab is required to maintain a copy of the data for a specified period of time according to each laboratory's standard record retention requirements.

Record Handling

Copies of the data submitted by the labs to the Coalition are kept at the Coalition office in electronic and, where necessary, hardcopy format. Additional copies of the data are submitted to the Regional Board along with the quarterly and annual reports. Copies of this data are kept at the local Board office in Fresno, the Regional Board office in Rancho Cordova (and at the Coalition's office).

Data is submitted to the Coalition by the BSK Laboratory in PDF format, and stored electronically. This is more efficient than paper copies of the reports, given the voluminous amounts of data generated. CD's containing the data are routinely made and stored in a secure manner.

Data submission is to be in a CEDEN and GeoTracker ESI compatible excel spreadsheet, for SWAMP and GQTMP respectively, prepared by the individual laboratories (in addition to the additional data formats submitted), which will be combined into a single spreadsheet for submission to the Regional Board. Staff at the Regional Board will be responsible for the upload of data into the CEDEN database. Coalition staff will be responsible for the upload of data into the GeotTracker ESI database,

Data collected and held by the Coalition will be stored for a minimum of seven years at the Coalition office. How long the data submitted to the Regional Board is held is unknown. The Laboratories will store the raw data in both hardcopy and electronic format in accordance with their respective record retention requirements. For CA ELAP certified laboratories – a required credential for this program – laboratories are required to maintain all records for a minimum of five years. Sufficient records must be maintained to allow complete reconstruction of the data.

Documents retained by the Coalition may include: paper copies of the field data sheets, executed Chains of Custody, purchase orders for lab services, and printed copies of the Chemistry, Microbiology and Water Column Toxicity results. All of which are also backed up electronically.

Each data submission to the Regional Board will be a standalone file stored electronically with the Coalition. Once SWAMP analysis results are submitted and accepted by the Regional Board, the data will be integrated into the CEDEN database as maintained by the Central Valley Regional Data Center (CV RDC). GQTMP analyses results will be submitted to the Regional Board through the GeoTracker ESI system.

The QAPP, will be submitted to the Regional Board in the form of a CD. Two versions will be submitted, one containing proprietary information regarding chemical testing and the other for public viewing. They will be clearly labeled. A paper copy of each version will be provided to the Regional Board for review on request.

Once the QAPP is approved by the Regional Board and signed by all required parties, an official copy will be maintained and controlled by the Coalition Quality Assurance Manager. The QA Manager will be responsible for distributing the official copy to the recipient list specified in Element 3. Due to its size, the official copy will be distributed via CD, sent either through mail (or similar delivery) or hand delivered to each recipient's location. In the event of a change in the QAPP, the QA Manager will be responsible for ensuring the timely delivery of the latest revision.

Report Format

Reports for the Chemistry, Microbiology and Water Column Toxicity will be provided in a manner consistent with this QAPP required content.

Documentation of the field activities will include copies of field logs with anomalies noted, results for field measurements, executed chains of custody, and any additional forms, records, or logs that contain information critical to the quality of the data obtained from the sampling event.

Analytical Reports or Certificates of Analysis will contain the following information:

- a. Project Name
- b. Sample Description
- c. Sample Date and Time of Collection
- d. Collection Technique (e.g. grab, composite)
- e. Sample Type (e.g. field sample, field blank, field duplicate)
- f. Preparation and Test Method
- g. Parameter
- h. Result
- i. Dilution Factor
- j. Reporting and Detection Limit
- k. Units
- l. Date / Time Prepared and Analyzed
- m. Data Qualifies
- n. Quality Control Data including Blanks, Spikes, Duplicates, Surrogates
- o. Case Narrative explaining all data anomalies or deficiencies
- p. Chain of Custody
- q. Sample Conditions on Receipt Summary
- r. Subcontract Reports

Record Distribution

The Project QA Manager will have the responsibility of ensuring that the stakeholders have the current version of all relevant documentation including the QAPP. The QA Manager will issue control copies of the current QAPP to each QAPP recipient listed in Element 3 of this QAPP. On a change or revision, the QA Manager will retract the old version of the document and replace with the most current version. The same process will be used for all other documents required by this Plan.

ELEMENT 10: SAMPLING PROCESS DESIGN

Sampling will be conducted according to the schedule mandated within the MRP, with visits of all surface water monitoring sites on a monthly basis and groundwater monitoring of wells on an annual basis. The date for the surface water sampling event is held open with Coalition as the presence of water at each sampling location is uncertain. This allows the contracted lab to work with the Coalition staff to determine the appropriate date for surface water sampling collection to maximize the collection of a sample at a time of water flow. The groundwater sample collection will be conducted during the summer months of each year.

Surface Water Sampling Process Design

The sampling design is to test for the specified chemistries at each of the identified surface water monitoring sites, thus creating defined areas that can be easily addressed should detection occur. Modifications to the list of tested chemistries are planned once cropping patterns and pesticide usages are analyzed.

The SWMP study design is a simple one because of the nature of the waterways involved. Nearly all of the river and creek systems within the Tulare Lake Basin have been optimized for irrigation deliveries. The flow in the Tule River below Success Dam is controlled by the Army Corps of Engineers, while Deer Creek and White River are smaller watersheds and uncontrolled streams. The Plan is designed to detect any occurrence of chemical contamination of these waterways, and then to trace the source. The method for the connection of any chemical contamination to its source and, ultimately, the management practices or runoff related events are outlined in the SWMP.

All surface water monitoring sites listed within the MRP will be visited during each month. It is anticipated that several of the sampling sites will only require photo documentation for the majority of the sample dates. This is due to infrequent flow in the waterway. Specific sampling points at each location have been identified and the rationale for each point is detailed in the SWMP.

Should a site become inaccessible due to field conditions that prevent a Coalition or Laboratory representative to safely access the site, the condition of the site will be documented and the sampling site revisited as soon as conditions allow. This documentation will be included with the report submitted for the follow up (or make up) sampling event. Resampling due to accessibility problems will be addressed on a case by case basis and coordinated between the contract Laboratory and the Coalition. However, as noted in the SWMP, part of the rationale for the selection of the sampling points was the reliability of each to be accessible at all but the most extreme conditions.

However, in some cases, resampling may not be an option due to inclement weather or some other water management constraint. In the event that it is determined a surface water sample must be collected, the specific sampling point may need to be modified. The Coalition Program Manager and Technical Lead will make the determination if this

modification is required. If so, the Program Manager will have the responsibility of informing the Board of the modified sampling point and the rationale for doing so.

The occurrence of an exceedance at any of the surface water monitoring sites will trigger a review of the possible sites where the detected chemical could have been used. Also, a physical survey may be undertaken to determine where the chemical could have entered into the waterway. The exact course of action will depend upon the chemistry detected, and the conditions that were present when the sample was collected.

One or more of the surface water sampling sites may be wet during the full course of the year. For these samples, a full set of chemical tests (as specified by the MRP) will be analyzed during the first year of the program. Samples will be grab samples of ambient water.

A duplicate sample will be randomly collected from those sites with water present. However, given that some sites are more likely to be dry a portion of the year, those sites having water most of the year will likely be disproportionately chosen during most sampling events for the field duplicate. One duplicate will be collected for each event.

The only sources of natural variation within the testing program are the EC values. These sources of variation are natural, and as such, uncontrollable.

No known sources of bias exist within the testing program. Field instruments, which could be considered a source of bias, are constantly checked for calibration against known standards and rechecked at the field during the course of the day. The laboratories constantly recalibrate their instrumentation as per method, so that source of variation is minimized as well, the resultant data having no more variation than that inherently contained within the test methods employed.

Surface water sampling points for the coalition are identified in Table 5.

Table 5: Coalition Surface Water Sampling Point Coordinates

Site name	CEDEN Code	Latitude	Longitude
Deer Creek at Road 120	558DCR120	35.912400	-119.303729
Deer Creek at Road 176	558DCR176	35.946256	-119.181017
Deer Creek at Road 248	558DCR248	35.9929	-119.017900
Porter Slough near Road 192	558SPR192	36.116285	-119.134132
Tule River at Plano Street Bridge	TBD	36.055865	-119.133987
Tule River at North Fork Road 144	558TRA144	36.129178	-119.246882
Tule River at Road 92	558TRAR92	36.092952	-119.366727
White River at Road 208	TBD	35.858597	-119.107887

All data collected as part of the sampling (pH, EC, temperature, turbidity, flow) will be considered critical to the program. All data will be used in the assessment of ambient conditions of the overall water quality. Field observations such as outside temperature, wind

directions, time of the day, etc. will be considered informational and not critical to the Plan. However, such observations should be documented as they may help explain any possible anomalies in the analytical data such as unexpected detections for parameters that are historically low or absent in the watershed.

The sampling schedule for each location is included in the SWMP.

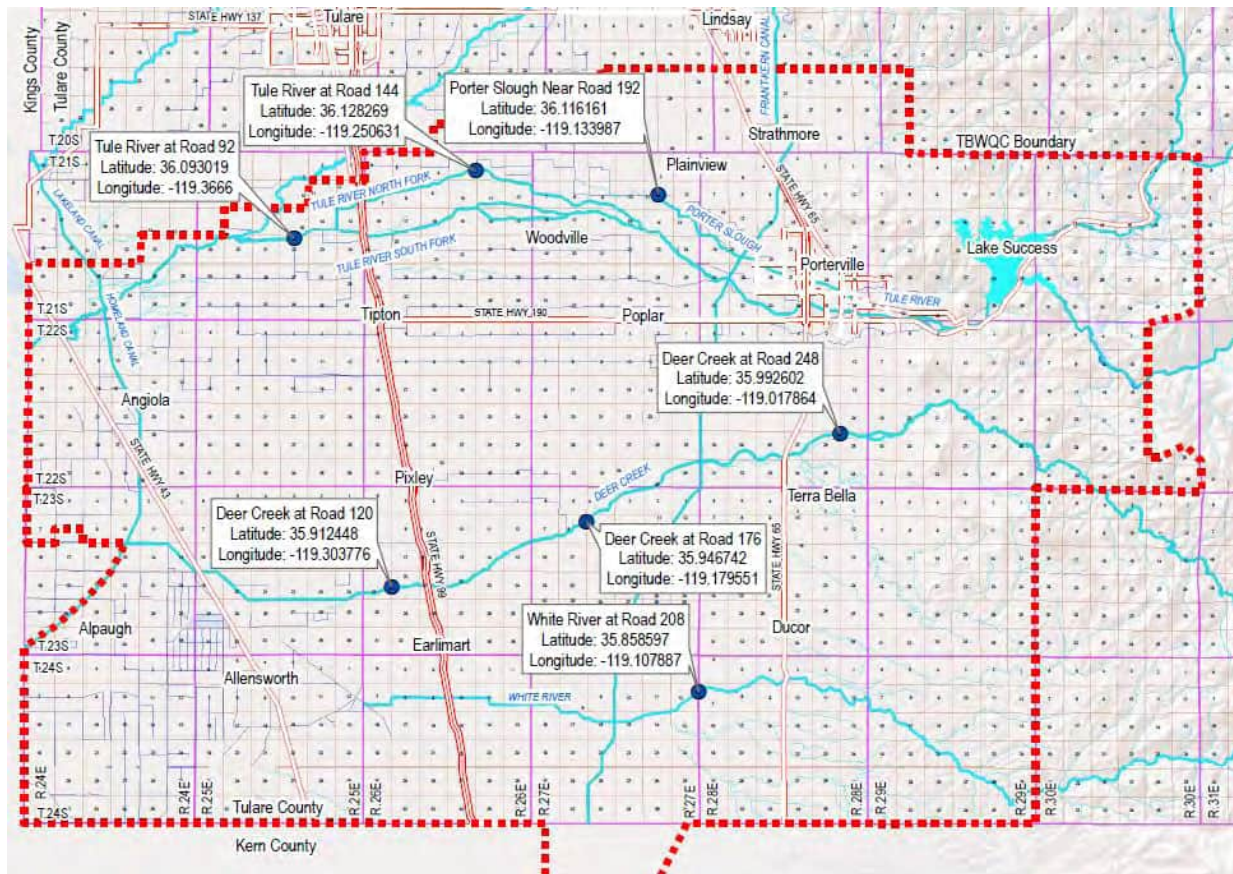


Figure 2: Tule Basin Water Quality Coalition Surface Water Monitoring Sites



Figure 3: Deer Creek at Road 120 Site Map



Figure 4: Deer Creek at Road 176 Site Map



Figure 5: Deer Creek at Road 248 Site Map



Figure 6: Porter Slough near Road 192 Site Map



Figure 7: Tule River at Plano Street Bridge Aerial Site Map



Figure 8: Tule River at North Fork Road 144 Site Map



Figure 9: Tule River at Road 92 Site Map

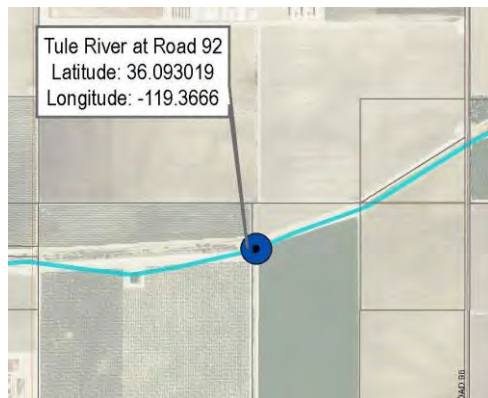


Figure 10: White River at Road 208 Site Map

Groundwater Sampling Process Design

The groundwater monitoring network as outlined in the GQTMW consists of sampling four wells per township, within both the High and Low Vulnerability areas within the TBWQC, provided, adequate existing wells are available. Domestic and shallow irrigation wells considered for the network are required to have permission from owners, be constructed in the upper most aquifer, with construction details, typically in the form of well completion reports.

Before wells are included in the monitoring program they must be reviewed and approved by the RWQCB to meet the requirements outlined in the MRP. Wells are presented to the RWQCB accompanied with GPS coordinates, well completion reports and construction details including: well depth, perforation intervals, seal information, and casing material.

The GQTMW for the TBWQC was designed in a two phased approach, see Figure 10. Phase 1 encompasses the township and ranges associated with disadvantaged communities (DACs) in the Coalition, with selection and monitoring of well beginning during the first year of the program (2018). Phase 2 makes up the remaining township and ranges within the Coalition and selection and monitoring of wells commencing in the second year (2019) of the program. In the third year of the program all wells will be sampled on the same schedule.

Wells in the GQTMW monitoring network will be sampled on an annual interval for a select group of water quality parameters and sampled every five years for a more extensive set of parameters. Monitoring includes field tested water quality parameters and laboratory analysis of nitrate as nitrogen and general minerals. Constituents and their frequency for analysis are outlined in the MRP.

Water samples shall be obtained from the wellhead, or as near the wellhead as possible, not from any point after the pressure tank. Samples shall not be collected from a

faucet inside the home. Wells without these physical capabilities for field sampling were not considered for the trend monitoring well, unless a spigot is installed at or near the wellhead.

If the well goes dry (Drought conditions), or if a well is not selected due to field conditions or access limitations, another well will be identified to replace the well that cannot or can no longer be used. The identification of the secondary well, should the selected well be abandoned, in the nine square mile areas of each township will allow time for identification of a replacement without a gap in data within the township. The Coalition Program Manager and Technical Lead will make the determination if a replacement is required. If so, the Program Manager will have the responsibility of informing the RWQCB of the replacement sampling well location and the rationale for doing so.

Wells used for the monitoring network are included in the GQTMW and periodic updates to network development will be provided to the RWQCB.

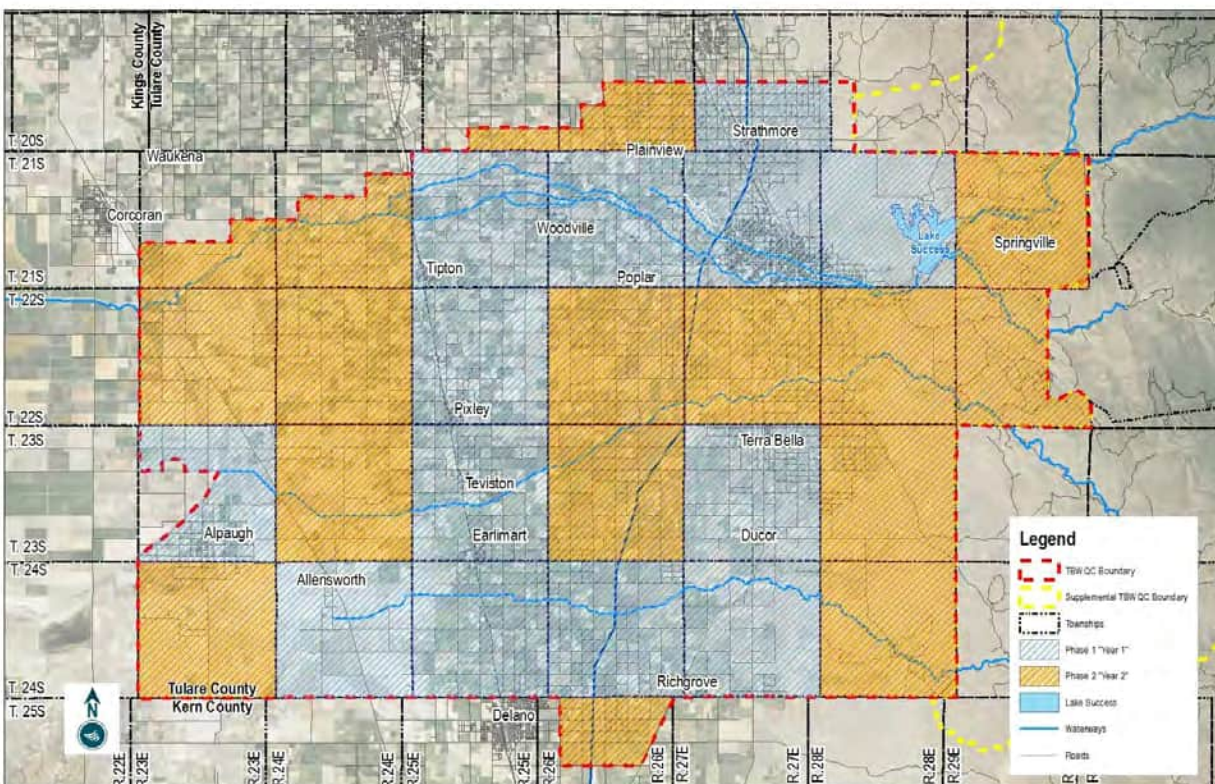


Figure 11: GQTMW Well Network

ELEMENT 11: SAMPLING METHODS

A more detailed description of the sample collection procedures are listed in the SOP in Appendix B.1. As part of the sample collection, photo documentation of the monitoring site will occur. Field technicians will photo log the location, both upstream and downstream of the sampling point as well as the actual point of collection. GPS coordinates will be confirmed and if the point of collection changes, new GPS coordinates will be recorded. A change in the location will only occur on notification and approval of the Project Coordinator.

In the case that the sampling crew is responding to a stormwater event and cannot sample at the exact coordinates indicated in this QAPP, samples will be collected upstream and the Project Coordinator will be notified as soon as possible. Sample analysis will not begin until the location has been approved by the Project Coordinator or his designee. If there is a material difference in the location of actual collection versus the targeted location (>75 yds), the Coalition Project Coordinator will be responsible for notifying the RWQCB.

Safety precautions and procedures in the SOPs for *Field Sampling* must be followed by the sampling crew. Sampling cannot be conducted if the water conditions at the site are deemed hazardous or unsafe. The Project Coordinator will be notified as soon as possible when samplings cannot be performed.

General Sampling Requirements

For the **surface water** sample to be deemed acceptable, the following criteria must be met:

1. Water must be present at the sampling location.
2. The sampler must remain downstream of the sample bottle while the sample is being collected.
3. A delay between samples must occur to allow any disturbed sediment to clear the area of sample collection.
4. The Water Column Toxicity sample bottles should be rinsed with sample water before the final sample is collected.
5. The samples must be kept chilled prior to packing with ice for transport.

Unacceptable surface water samples would include samples from waters that are too shallow to completely submerge the sample container without excessive disturbance of the sediment.

For the **water supply well** sample to be deemed acceptable, the following criteria must be met:

1. Prior to collecting a water sample from a supply well, the water well shall be allowed to run for a period of time that is sufficient for water quality parameter readings for temperature, pH, EC, dissolved oxygen, and turbidity to stabilize to within 10 percent.
2. If the well is currently pumping, the sample may be taken without purging the well.
3. Water samples shall be collected from the discharge point nearest the well head.
4. Samples shall be collected directly into laboratory-prepared bottles. and shall not be taken from a location after treatment of the water for domestic use.
5. The samples must be kept chilled prior to packing with ice for transport.

Surface Water Sediment Sample Collection Requirements

Sediment samples are considered acceptable if the depth of the sediment collected does not exceed 1 inch or 2.5 cm (per method). The sediment must be collected within a reasonable distance of the water collection site, and in sufficient volume to perform an adequate analysis.

Unacceptable sediment samples are those collected from depths in excess of 1 inch or 2.5 cm, from distances too far away from the monitoring site (potentially representing different conditions than those present when water samples are collected), and samples of insufficient volume. Failure to transport the sample at controlled temperatures would also constitute an unacceptable sample.

As a safety precaution, sediment collection should only be performed in a shallow, slow flowing stream or canal waterway, where the water is between a minimal surface flow of a few inches to a maximum depth that is below the height of the sampler's knee. The stream or canal flow must be slow flowing of less than one foot per second. Sampling attempted in conditions exceeding these limitations must be conducted with special safety harness, retrieval gear or rescue apparatus.

Sample Collection Volumes

The volume of collected samples are designated by the contracted laboratory to allow for sufficient volume to test, plus additional volume for retesting in the event of laboratory errors (spillage, instrument failure, operator error). Breakage, unfortunately, cannot be anticipated once the sample is delivered to the lab, so no contingency plan is available for such an occurrence. The only recourse is to fully duplicate all samples, which is impractical for all concerned.

Sample Collection Procedures

Pre-Collection

The sequence of events for a sampling event is as follows:

1. Several days before the event, all bottles are collected and labeled for the event. They are then packed into labeled ice chests for transport.
2. The day before the event, the calibration of the field instruments is performed according to manufacturer specifications. Adequate supplies of standard solutions are placed within the field equipment box for instrumentation checks while at the monitoring sites. Battery issues with field instruments are addressed at this time.
3. The day of the sample, chests are loaded into the vehicle along with a chest filled with frozen “blue ice” sample temperature maintaining blocks.

During Collection

Once at a site, the sequence is as follows:

1. One team member begins the filling out of the sample sheet for the site (field sheet and chain of custody), and takes a photo of the site. The monitoring site where the sample is collected does not change from event to event so the GPS coordinates remain the same from event to event. The names of the sampling crew are recorded on the sample sheet.
2. Ice chests to be used at the site are carried from the vehicle to the sample site.
3. Date, sampler, and time of sample are recorded on the bottles within the chests.
4. Field instruments are checked against the standard solutions (pH and EC) where appropriate, and the data recorded.
5. Field sampling technician will don powder free, nitrile gloves to guard against contamination.
6. If entry into the water is required, field technician approaches the sampling point from downstream to minimize the chance of sediment in the collection field. If sediment is materially disturbed, the zone must be allowed to clear before collecting a sample. **(surface water sampling)**
7. Samples will be taken with a large carboy to minimize the number of bottles carried into the water body. Once filled, the contents of the carboy will be transferred into the actual preserved sample containers.
8. After all bottles have been filled, a fresh sample is analyzed for field parameters: pH, EC, temperature and dissolved oxygen. The stream velocity is also measured and recorded on the field log for surface water sampling.
9. Water samples are collected until all bottles are filled. Care is exercised to repack the bottles to prevent breakage.
10. If a duplicate sample is to be collected at the site, steps 5 – 9 are repeated.
11. Site photos are taken, with photos of the sampling point, upstream and downstream. **(surface water sampling)**
12. “Blue” or gel ice is placed in the chests once they are carried back to the vehicle.

Following Collection

After the samples are returned to the office, and offloaded from the vehicle, cubed ice is packed into the chests (blue ice is removed). Chemical test samples are then transported to the lab. Water Column Toxicity samples are stored within the office for transport the next morning if the sampling crew returns too late in the day to package and ship to the aquatic toxicity laboratory.

The Laboratory will provide additional sample containers for the Field Duplicate and Site Specific QC (MS/MSDs). The laboratory will identify the bottles by location and by sample type (Dup, MS/MSD). It is critical that the sampling crew fill ALL bottles provided in the manner specified by the laboratory. Failure to fill all containers may result in insufficient quality control data to meet the project data quality objectives.

There is limited sampling equipment required for the collection of both aqueous and sediment samples. For the aqueous samples, a large 3-L carboy is the only container that may be reused between sampling location. To that end, the carboy will be triple rinsed between sampling locations using 300mL of laboratory grade deionized water. The use of any detergent as a cleansing agent could be problematic given the low reporting limit requirements of the program. Once triple rinsed, the carboy will be sealed and remain closed until the next sampling location. Prior to collection at the next site, the carboy shall be rinsed under the above matrix prior to collecting any samples.

Alternatively, the Laboratory may elect to use virgin bottleware for the collection of samples. If so, no decontamination procedures are required. Additional carboys and any other sampling devices will be carried in the event that there is a problem with the carboy or other device that might be shared between locations.

For the sediment samples, the trowel or large scoop is the only device that may be in contact with each sample. Therefore, after use it will be first rinsed with water from the stream where the sample was collected. This is done to remove any remaining solids. It will then be triple rinsed with deionized water, stored in a clean Zip-lock bag and kept sealed till the next sampling site. Once at the next location, it will be rinsed in the river or stream prior to the collection of the next sample.

Post Collection Handling

Transport represents the greatest risk to the sample once collected, and every effort shall be made to package the samples in protective materials. Glass containers are wrapped in “bubble-wrap” both before and after sample collection. Care is exercised when placing the “blue-ice” temperature control materials within the ice chests after the sample is collected, to prevent breakage. Travel speeds on unimproved roads are also limited.

Water Column Toxicity samples are collected in 1-gallon cubitainer jugs, with 6 gallons of sample per site. Each jug is rinsed using sample water prior to filling with the final sample. Headspace is left at top of bottle to reduce risk of bottle breakage at lab.

As stated in the SOP section (Appendix B.1), the field instruments are rinsed in distilled water after the second (duplicate) reading, and stored within the instrument case. The pH meter is returned to a container containing pH 7 solution for transport.

Problems are always unforeseen. Barring a technical failure in the field instrumentation or an accident during or between the sampling events, most anticipated issues can be dealt with in a manner that will not substantially affect data usability. However, technical failures will result in the loss of all data generated by the field instrument from the point of failure on due to the need to return the instrument to the manufacturer for repairs. Battery issues are eliminated by inspecting the instrument during calibration and by maintaining backup supplies for field activities.

Automobile accidents or the dropping of a sample container are by nature unpredictable.

Access restrictions to the monitoring site are likely to be rare, and corrected (if practical) by hiking to the site.

Sufficient staff exists to cover a sampling event in the event of scheduling conflict or illness.

The only samples that require homogenization are the sediment samples, which are collected across the entire main waterway. Individual containers of approximately 1L will be collected with a sufficient number filled to cover all the testing required including the Toxic Identification Evaluation (TIE) if required. Once transported back to the Laboratory, all individual containers will be emptied and combined into a single sample. The sample will be homogenized in a large stainless steel container and once thoroughly mixed, returned to the original containers. These individual containers will then be distributed to the primary contract Laboratory as well as any subcontract laboratories.

ELEMENT 12: SAMPLE HANDLING AND CUSTODY

Samples are to be collected only in containers provided by the laboratory. Substitute containers are strictly forbidden as the integrity of such containers would be unknown. Any alternative containers provided to the laboratory will be rejected unless otherwise authorized in writing by the Project Coordinator and Program QA Manager.

Using the correct container is critical as each test method has specific preservation requirements. Samples are preserved to ensure that the condition of the sample at the time of analysis is consistent with the conditions as it existed in the field. The laboratory uses a variety of conditions to inhibit bacterial growth that would degrade target analytes, to prevent certain constituents from precipitating and falling out of solution, to prevent oxidation/reduction of the various constituents, and to prevent parameters from evolving off as a gas. The preservation technique and storage requirements for each test method are listed in Table 6.

Once collected, each sample and analysis has a finite amount of time before it must be prepared or analyzed. If the time period (known as the holding time) expires, the results may be considered invalid and would normally be a cause for rejection of the subsequent data. The holding times for each test method are listed in the following Table 6.

Table 6: Method Preservation, Storage and Holding Time Requirements

Parameter	Preservative	Container	Storage	Hold Time to Prepare	Hold Time to Analyze
Ammonia/Ammonium	H ₂ SO ₄	Plastic	<6°C	28 Days	-
Carbamates	None	Clear Glass	<6°C	7 Days	40 Days
Carbonate/Bicarbonate	None	Plastic	<6°C	-	14 Days
Glyphosate	Na ₂ S ₂ O ₃	Amber Glass	<6°C	14 Days	-
Hardness (Calc)	HNO ₃	Plastic	Ambient	-	180 Days
Herbicides	None	Amber Glass	<6°C	7 Days	40 Days
Metals	HNO ₃	Plastic	Ambient	-	180 Days
Metals (Dissolved)	None	Plastic	Ambient	-	180 Days
Nitrate, Nitrite	None	Plastic	<6°C	-	48 Hours
OCl Pesticides	None	Amber Glass	<6°C	7 Days	40 Days
OP Pesticides	None	Amber Glass	<6°C	7 Days	40 Days
o-Phosphate	None	Plastic	<6°C	-	48 Hours
Paraquat	Na ₂ S ₂ O ₃	Amber Plastic	<6°C	7 Days	21 Days
Pathogens	Na ₂ S ₂ O ₃	Acrylic	<6°C	8 Hours	-
Pyrethroids (Sediment)	None	Clear Glass	<6°C	14 Days	40 Days
Solids (TDS and TSS)	None	Plastic	<6°C	-	7 Days
TOC	H ₃ PO ₄	Clear Glass	<6°C	-	28 Days
Toxicity	Chilled to <6°C/wet ice	Plastic	<6°C	-	36 Hours
Triazine Pesticides	None	Amber Glass	<6°C	7 Days	40 Days
Turbidity	None	Plastic	<6°C	-	48 Hours

Samples are transported within ice chests that contain “blue ice” blocks to maintain low temperatures until the samples can be packed with wet ice. Glass bottles are wrapped in bubble wrap to prevent breakage (it also insulates the samples before they are packed in ice). Toxicity samples are repacked in ice (or have the levels checked) the next morning prior to transport.

Chains of custody forms are provided by the contracted lab and include all of the required information for the proper handling of the samples collected. As the sample passes from the control of one entity to another, the form is signed off by the responsible parties. Copies of the completed custody forms are provided with the final lab reports.

The Quality Assurance Manager and Laboratory Coordinators are responsible for the review and filing of the chains of custody forms.

Once at the lab, the condition of the samples is logged, with copies of the log appended to the lab report. Barcodes are attached to the samples and logged in a computerized tracking system.

Storage of the samples, once they are released to the lab, will be at the condition specified above. Any exceptions to the holding times listed above are noted in the laboratory report and are addressed on a case by case basis. Sample preservation is effectively handled by the chemistry lab as the bottles supplied are pre-treated with the proper preservation (if required, see above Table 6). Samples with pH preservation will be checked on receipt to verify that the sample has reached the proper pH. Any deviations from the method preservation requirements will be brought to the attention of the Project Lead. The laboratory will not proceed with the analysis of any improperly preserved samples without the approval of the Project Lead. Any samples analyzed that were not received under proper preservation will be noted in the report case narrative.

Records are maintained within the contracted lab that includes the checking in and out of samples during the analytical process as well as the disposal of samples following completion of the analytical process and archival. Samples are held under proper storage conditions until all analyses are conducted. Once complete, samples will be moved to a temporary archive where they await disposal. Samples are held by the laboratory for 60 days prior to being disposed.

ELEMENT 13: ANALYTICAL METHODS AND FIELD MEASUREMENTS**Standard Operating Procedures**

The contract laboratory utilizes a number of EPA or Standard Methods preparation and determinative methods. The laboratory has SOPs for each method employed as well as SOPs for the procedural activities in the laboratory. The following Table 7 lists the method specific SOPs for this project with the current revisions at the time of submittal of this QAPP. Laboratory SOPs are periodically reviewed and may be updated as necessary.

Table 7: Standard Operating Procedures

Parameter	Method Description	Doc ID	Rev. Date
Ammonia	Ammonia by Gas Diffusion and Automated Phenate	IO-SP-0036-01	1/16/15
Anions	Anions by Ion Chromatography	IO-SP-0085-03	12/18/17
Alkalinity	Alkalinity by PC-Titrate	IO-SP-0061-09	8/17/16
Glyphosate	Glyphosate by HPLC, Post Column Derivatization	OR-SP-0009-06	7/28/17
Hardness	Hardness by Calculation	IO-SP-0044-02	2/17/17
Metals	Metals by ICP-MS	MT-SP-0008-01	11/2/17
	Metals by ICP-AES	MT-SP-0007-01	11/6/17
	Total Recoverable Metals Preparation	MT-SP-0001-01	10/31/18
Ortho-Phosphate and Phosphorus	o-Phosphate and Phosphorus by Ascorbic Acid Reduction	IO-SP-0072-04	6/20/16
Paraquat	Paraquat by SPE, HPLC-UV	OR-SP-0011-06	5/25/17
Pathogens	Multi-Tube Fermentation for Total and Fecal Coliform, and E. Coli	WM-SP-0002-04	11/14/17
Pesticides – N,P, Pyrethroids	Nitrogen, Organophosphorous Pesticides	OR-SP-0034-02	2/17/17
	Pyrethroid Pesticides by GC/MS		
Pesticides – OCl	Organochlorine Pesticides by GC-ECD	OR-SP-0019-04	3/28/17
Solids (TDS and TSS)	Solids by Gravimetric Determination	IO-SP-0020-05	3/29/16
Total Organic Carbon	TOC by TOC analyzer (SM 5310C)	IO-SP-0067-07	12/18/17
Toxicity – Algae	Chronic toxicity	EPA-821-R-02-013	2002
Toxicity – Flea	Acute toxicity	EPA-821-R-02-012	2002
Toxicity - Minnow	Acute toxicity	EPA-821-R-02-012	2002
Toxicity - Hyalella	10 Day Sediment Survival and Growth	EPA-600-R-99-064	2000
	Test – Hyalella azteca		
Turbidity	Turbidity by Nephelometry	IO-SP-0029-04	4/20/15
Sample Collection	Field Sampling from Streams, Rivers and Canals	SR-SP-0015-01	6/8/16
Sample Collection	Safety for Stream and Canal Sampling	SF-SP-0010-00	6/6/16

Copies of these SOPs can be found in Attachment B. These SOPs are considered proprietary information by the laboratory and will be redacted for the purpose of the public version of this QAPP.

Instrumentation

The contract laboratory will utilize a wide range of equipment in the performance of the analytical testing. While not exhaustive in content, the following list of equipment represents the minimal amount of instrumentation required to perform the testing under this Plan. The list does not indicate each individual piece of equipment as the laboratory maintains redundant equipment in many cases.

See Tables 11, 12 and 13 for a listing of field and laboratory instrumentation.

Field Monitoring

All field measurements will be performed at the time of sampling. There will be no *in situ* or continuous monitoring of field conditions at the specific monitoring sites. Any information about the conditions at the sampling points between sampling events would need to be inferred from other indirect sources such as water flows at points upstream or downstream or measurements made or samples collected and analyzed for other purposes. Otherwise, there are no other requirements for the deployment, maintenance, calibration or storage of related data for field equipment.

Method and Instrument Performance Criteria

The contract laboratory performs testing for several watersheds in support of their ILRP monitoring requirements. The test methods employed have been tailored to meet the requirements of this Plan to ensure compliance with the General Order, WDR and QAPP guidelines. All methods utilized are based on approved, standardized methods. There are no other “in-house” or non-standardized methods used for this Plan.

The contract laboratory will observe the following list of performance criteria for the testing done in support of this Plan.

Quantitation and Detection Limits

Table 8: Methods, Reporting Limits and Detection Limits

Constituent	ILRP PQL	BSK Reporting Information			
		RL	MDL ¹	Units	Method
Physical Parameters					
Flow	1	-	-	cfs	Field
pH	0.1	0.1	-	pH Units	Field
EC	100	5	-	umhos/cm	Field
DO	0.1	0.1	-	mg/L	Field
Temp	0.1	-	-	°C	Field
Turbidity	1	0.1	-	NTU	SM 2130B
TDS	-	10	-	mg/L	SM 2540C
TSS	10	10	-	mg/L	SM 2540D
Hardness as CaCO ₃	10	0.41	-	mg/L	SM 2340B
TOC	-	0.5	0.086	mg/L	SM 5310C
Percent Solids / Moisture	-	0.1	-	%	SM 2540B
Pathogens					
Fecal Coliform	2	1.8	-	MPN/100mL	SM 9221E
E. coli	2	1.8	-	MPN/100mL	SM 9221F
Water Column Toxicity					
Algae	NA	NA	NA	Cell/mL, % Growth	EPA 821-R-02-013
Water Flea	NA	NA	NA	% Survival	EPA 821-R-02-012
Fathead Minnow	NA	NA	NA	% Survival	EPA 821-R-02-012
Sediment Toxicity					
Hyalella azteca	NA	NA	NA	% Survival	EPA 600-R-99-064
Carbamates					
Aldicarb	0.5	0.4	0.017	ug/L	EPA 8321A
Carbaryl	0.5	0.1	0.022	ug/L	EPA 8321A
Carbofuran	0.5	0.1	0.021	ug/L	EPA 8321A
Methiocarb	0.5	0.4	0.014	ug/L	EPA 8321A
Methomyl	0.5	0.1	0.018	ug/L	EPA 8321A
Thiobencarb	-	0.5	0.0065	ug/L	EPA 8270C
Oxamyl	0.5	0.4	0.021	ug/L	EPA 8321A
Organochlorines					
DDD	0.02	0.01	0.00072	ug/L	EPA 8081A
DDE	0.01	0.01	0.00061	ug/L	EPA 8081A
DDT	0.01	0.01	0.0007	ug/L	EPA 8081A
Dicofol	0.1	0.1	0.015	ug/L	EPA 8270C
Dieldrin	0.01	0.01	0.00097	ug/L	EPA 8081A

		BSK Reporting Information			
Constituent	ILRP PQL	RL	MDL ¹	Units	Method
Endrin	0.01	0.01	0.00081	ug/L	EPA 8081A
Methoxychlor	0.05	0.01	0.00091	ug/L	EPA 8081A
Toxaphene	-	0.5	0.035	ug/L	EPA 8081A
Organophosphates					
Azinphos-methyl (Guthion)	0.1	0.1	0.032	ug/L	EPA 8270C
Chlorpyrifos	0.015	0.015	0.0029	ug/L	EPA 8270C
Diazinon	0.02	0.02	0.0036	ug/L	EPA 8270C
Dichlorvos	0.1	0.1	0.0048	ug/L	EPA 8270C
Dimethoate	0.1	0.1	0.0075	ug/L	EPA 8270C
Demeton-S (Demeton [O,S])	0.1	0.1	0.025	ug/L	EPA 8270C or EPA 8321A
Disulfoton	0.05	0.05	0.025	ug/L	EPA 8270C or EPA 8321A
Malathion	0.1	0.1	0.0046	ug/L	EPA 8270C
Methamidophos	0.2	0.2	0.022	ug/L	EPA 8270C or EPA 8321A
Methidathion	0.1	0.1	0.011	ug/L	EPA 8270C
methyl Parathion	0.1	0.1	0.003	ug/L	EPA 8270C
Phorate	0.2	0.1	0.0033	ug/L	EPA 8270C
Phosmet	0.2	0.2	0.03	ug/L	EPA 8270C
Herbicides					
Atrazine	0.5	0.5	0.029	ug/L	EPA 8270C
Simazine	0.5	0.5	0.024	ug/L	EPA 8270C
Cyanazine	0.5	0.5	0.036	ug/L	EPA 8270C
Diuron	0.5	0.4	0.022	ug/L	EPA 8321A
Molinate	-	0.5	0.0043	ug/L	EPA 8270C
Glyphosate	5	5	2.1	ug/L	EPA 547
Paraquat	0.5	0.4	0.21	ug/L	EPA 549.2
Linuron	0.5	0.4	0.014	ug/L	EPA 8321A
Trifluralin	0.05	0.05	0.0056	ug/L	EPA 8270C
Metals (Total /Dissolved)					
Arsenic	1	0.2	0.059	ug/L	EPA 200.8
Boron	10	10	4.6	ug/L	EPA 200.8
Cadmium	0.1	0.1	0.075	ug/L	EPA 200.8
Calcium	-	0.1	0.046	mg/L	EPA 200.7
Copper	0.5	1.1	0.49	ug/L	EPA 200.8
Lead	0.5	0.2	0.041	ug/L	EPA 200.8
Magnesium	-	0.1	0.046	mg/L	EPA 200.7
Molybdenum	1	0.5	0.32	ug/L	EPA 200.8
Nickel	1	1	0.20	ug/L	EPA 200.8

		BSK Reporting Information			
Constituent	ILRP PQL	RL	MDL ¹	Units	Method
Potassium	-	2	0.91	mg/L	EPA 200.7
Selenium	1	1	0.76	ug/L	EPA 200.8
Sodium	-	1	0.46	mg/L	EPA 200.7
Zinc	1	1	0.68	ug/L	EPA 200.8
Nutrients					
Nitrate-N	0.05	0.06	0.028	mg/L	EPA 300.0
Nitrite-N	0.05	0.05	0.020	mg/L	EPA 300.0
Ammonia	0.1	0.1	0.038	mg/L	EPA 350.1
Orthophosphate (as P)	0.01	0.01	0.0049	mg/L	SM 4500-P E
Phosphorus-P	-	0.01	0.0015	mg/L	SM 4500-P E
General Mineral					
Carbonate as CaCO ₃	-	3	-	mg/L	SM 2320B
Bicarbonate as CaCO ₃	-	3	-	mg/L	SM 2320B
Chloride	-	1	0.51	mg/L	EPA 300.0
Sulfate	-	1	0.40	mg/L	EPA 300.0
Pyrethroids / Chlorpyrifos					
Chlorpyrifos	-	10	0.36	ug/Kg	EPA 8270C
Bifenthrin	1.0	1.0	0.12	ug/Kg	EPA 8270C
Cyfluthrin	1.0	2.0	0.39	ug/Kg	EPA 8270C
Cypermethrin	1.0	2.0	0.54	ug/Kg	EPA 8270C
Deltamethrin	-	2.0	0.47	ug/Kg	EPA 8270C
Esfenvalerate (+Fenvalerate)	1.0	1.0	0.45	ug/Kg	EPA 8270C
Fenpropathrin	1.0	1.0	0.077	ug/Kg	EPA 8270C
Permethrin (cis-Permethrin)	1.0	1.0	0.11	ug/Kg	EPA 8270C
Lambda Cyhalothrin	1.0	1.0	0.062	ug/Kg	EPA 8270C
Piperonyl Butoxide	-	0.5	0.19	ug/Kg	EPA 8270C

1. The MDLs listed are those in existence at the time this QAPP was written. MDLs may change over time as the laboratory conducts ongoing studies due to changes in the method or equipment or is required to do so as per the SWAMP requirements.

Method Performance

The laboratory will observe the following method and instrument criteria for this project.

Table 9: Laboratory Method QC Criteria

Parameter	Calibration	Calibration Verification	Method Blank	Laboratory Control Spike (LCS)	LCS Duplicate	Matrix Spike (MS)	Matrix Spike Duplicate (MSD), Lab Duplicate	Field Duplicate	Surrogate Recovery
Ammonia	5 Pts Min. (Linear Fit, $R \geq 0.995$) 6 Pts Min. (Non-linear fit, $R^2 \geq 0.99$)	2 nd Source verification following calibration, %Diff \leq 10%, Continuing Verification every 10 field samples, %Diff \leq 10%	<RL	1 per batch of 20 samples, 90-110%	1 per batch of 20 samples, 20% RPD	1 per batch of 20 samples, 90-110%	1 per batch of 20 samples, 20% RPD	$\leq 25\%$ RPD	N/A
Carbamates	5 Pts Min. (Linear Fit, $R \geq 0.995$) 6 Pts Min. (Non-linear fit, $R^2 \geq 0.99$)	2 nd Source verification following calibration, %Diff \leq 10%, Continuing Verification every 10 field samples, %Diff \leq 10%	<MDL	1 per Batch of 20 Samples, 50-150%	1 per Batch of 20 Samples, 30% RPD	1 per Batch of 20 Samples, 50-150%	1 per Batch of 20 Samples, 30% RPD	$\leq 30\%$ RPD	Applied to all samples and QC, 50-150%
Glyphosate	5 Pts Min. (Linear Fit, $R \geq 0.995$) 6 Pts Min. (Non-linear fit, $R^2 \geq 0.99$)	2 nd Source verification following calibration, %Diff \leq 20%, Continuing Verification every 10 field samples, %Diff \leq 20%	<MDL	1 per batch of 20 samples, 70-130%	1 per Batch of 20 Samples, 30% RPD	1 per batch of 20 samples, 70-130%	1 per Batch of 20 Samples, 30% RPD	$\leq 30\%$ RPD	Applied to all samples and QC, 70- 130% Rec

Parameter	Calibration	Calibration Verification	Method Blank	Laboratory Control Spike (LCS)	LCS Duplicate	Matrix Spike (MS)	Matrix Spike Duplicate (MSD), Lab Duplicate	Field Duplicate	Surrogate Recovery
Hardness (Calc)	<i>Performed by Calculation. See Metals QC Criteria.</i>	<i>Performed by Calculation. See Metals QC Criteria.</i>	<RL	<i>Performed by Calculation. See Metals QC Criteria.</i>	<i>Performed by Calculation. See Metals QC Criteria.</i>	<i>Performed by Calculation. See Metals QC Criteria.</i>	<i>Performed by Calculation. See Metals QC Criteria.</i>	≤25% RPD	N/A
Herbicides	<i>5 Pts Min. (Linear Fit, R≥0.995 6 Pts Min. (Non-linear fit. R²≥0.99)</i>	<i>2nd Source verification following calibration, %Diff ≤ 30%, Continuing Verification every 20 field samples, %Diff ≤ 15%</i>	<MDL	<i>1 per Batch of 20 Samples, Rec Range Varies, Avg. Rec ± 3SD, See attached specification sheet</i>	<i>1 per Batch of 20 Samples, 30% RPD</i>	<i>1 per Batch of 10 Samples, Rec Range Varies, Avg. Rec ± 3SD, See attached specification sheet</i>	<i>1 per Batch of 20 Samples, 30% RPD</i>	≤30% RPD	<i>Applied to all samples and QC, Rec Range Varies, Avg. Rec ± 3SD, See attached specification sheet</i>
Metals	<i>Single Point calibration plus Calibration Blank, multi-point curves must be fit using Linear Regression, R≥0.995</i>	<i>2nd Source Verification following calibration, %Diff ≤ 10%, Reporting Limit Verification following calibration, %Diff ≤ 10%, Continuing Verification every 10 field samples, %Diff ≤ 10%</i>	<2.2x MDL	<i>1 per batch of 20 samples, 85-115%</i>	<i>1 per batch of 20 samples, 20% RPD</i>	<i>1 per batch of 20 samples, 70-130%</i>	<i>1 per batch of 20 samples, 20% RPD</i>	≤25% RPD	N/A

Parameter	Calibration	Calibration Verification	Method Blank	Laboratory Control Spike (LCS)	LCS Duplicate	Matrix Spike (MS)	Matrix Spike Duplicate (MSD), Lab Duplicate	Field Duplicate	Surrogate Recovery
Anions – Nitrate, Nitrite, Chloride, Sulfate	5 Pts Min. (Linear Fit, $R \geq 0.995$) 6 Pts Min. (Non-linear fit, $R^2 \geq 0.99$)	2 nd Source verification following calibration, %Diff \leq 10%, Continuing Verification every 10 field samples, %Diff \leq 10%	<RL	1 per batch of 20 samples, 90-110%	1 per batch of 20 samples, 20% RPD	1 per batch of 10 samples, 80-120%	1 per batch of 10 samples, 20% RPD	$\leq 25\%$ RPD	N/A
OCI Pesticides	5 Pts Min. (Linear Fit, $R \geq 0.995$) 6 Pts Min. (Non-linear fit, $R^2 \geq 0.99$)	2 nd Source verification following calibration, %Diff \leq 30%, Continuing Verification every 20 field samples, %Diff \leq 15%	<MDL	1 per Batch of 20 Samples, Rec Range Varies, Avg. Rec \pm 3SD, See attached specification sheet	1 per Batch of 20 Samples, 30% RPD	1 per Batch of 20 Samples, Rec Range Varies, Avg. Rec \pm 3SD, See attached specification sheet	1 per Batch of 20 Samples, 30% RPD	$\leq 30\%$ RPD	Applied to all samples and QC, Rec Range Varies, Avg. Rec \pm 3SD, See attached specification sheet
OP Pesticides	5 Pts Min. (Linear Fit, $R \geq 0.995$) 6 Pts Min. (Non-linear fit, $R^2 \geq 0.99$)	2 nd Source verification following calibration, %Diff \leq 30%, Continuing Verification every 20 field samples or 12 hours, %Diff \leq 20%	<MDL	1 per Batch of 20 Samples, Rec Range Varies, Avg. Rec \pm 3SD, See attached specification sheet	1 per Batch of 20 Samples, 30% RPD	1 per Batch of 20 Samples, Rec Range Varies, Avg. Rec \pm 3SD, See attached specification sheet	1 per Batch of 20 Samples, 30% RPD	$\leq 30\%$ RPD	Applied to all samples and QC, Rec Range Varies, Avg. Rec \pm 3SD, See attached specification sheet

Parameter	Calibration	Calibration Verification	Method Blank	Laboratory Control Spike (LCS)	LCS Duplicate	Matrix Spike (MS)	Matrix Spike Duplicate (MSD), Lab Duplicate	Field Duplicate	Surrogate Recovery
o-Phosphate	5 Pts Min. (Linear Fit, $R \geq 0.995$)	2 nd Source verification following calibration, %Diff \leq 15%, Continuing Verification every 10 field samples, %Diff \leq 10%	<RL	1 per batch of 20 samples, 90-110%	1 per Batch of 20 Samples, 20% RPD	1 per batch of 20 samples, 80-120%	1 per Batch of 20 Samples, 20% RPD	$\leq 25\%$ RPD	N/A
Phosphorus	5 Pts Min. (Linear Fit, $R \geq 0.995$)	2 nd Source verification following calibration, %Diff \leq 15%, Continuing Verification every 10 field samples, %Diff \leq 10%	<RL	1 per batch of 20 samples, 90-110%	1 per Batch of 20 Samples, 20% RPD	1 per batch of 20 samples, 80-120%	1 per Batch of 20 Samples, 20% RPD	$\leq 25\%$ RPD	N/A
Paraquat	5 Pts Min. (Linear Fit, $R \geq 0.995$) 6 Pts Min. (Non-linear fit, $R^2 \geq 0.99$)	2 nd Source verification following calibration, %Diff \leq 20%, Continuing Verification at the beginning of the run, every 8 hours or 20 samples minimally	<MDL	1 per batch of 20 samples, 70-130%	1 per Batch of 20 Samples, 30% RPD	1 per batch of 20 samples, 70-130%	1 per Batch of 20 Samples, 30% RPD	$\leq 30\%$ RPD	N/A

Parameter	Calibration	Calibration Verification	Method Blank	Laboratory Control Spike (LCS)	LCS Duplicate	Matrix Spike (MS)	Matrix Spike Duplicate (MSD), Lab Duplicate	Field Duplicate	Surrogate Recovery
Pathogens	N/A	thereafter, %Diff ≤ 20% N/A	<RL ¹	N/A ¹	N/A	N/A	N/A	≤25% RPD	N/A
Pyrethroids	5 Pts Min. (Linear Fit, R≥0.995) 6 Pts Min. (Non-linear fit, R ² ≥0.99)	2nd Source verification following calibration, %Diff ≤ 30%, Continuing Verification every 20 field samples or 12 hours, %Diff ≤ 20%	<MDL	1 per Batch of 20 Samples, Rec Range Varies, Avg. Rec ± 3SD, See attached specification sheet	1 per Batch of 20 Samples, 30% RPD	1 per Batch of 20 Samples, Rec Range Varies, Avg. Rec ± 3SD, See attached specification sheet	1 per Batch of 20 Samples, 30% RPD	≤30% RPD	Applied to all samples and QC, Rec Range Varies, Avg. Rec ± 3SD, See attached specification sheet
Solids (TDS, TSS)	N/A	N/A	<RL	(TDS Only) 1 per Batch of 20 Samples, 70-130%	N/A	N/A	<20% RPD (Lab Dup)	≤25% RPD	N/A
Toxicity	N/A	N/A	0%	0%	NA	NA	NA	NA	NA
Triazine Pesticides	5 Pts Min. (Linear Fit, R≥0.995) 6 Pts Min. (Non-linear fit, R ² ≥0.99)	2nd Source verification following calibration, %Diff ≤ 30%, Continuing Verification every 20 field samples or	<MDL	1 per Batch of 20 Samples, Rec Range Varies, Avg. Rec ± 3SD, See attached specification sheet	1 per Batch of 20 Samples, 30% RPD	1 per Batch of 20 Samples, Rec Range Varies, Avg. Rec ± 3SD, See attached specification sheet	1 per Batch of 20 Samples, 30% RPD	≤30% RPD	Applied to all samples and QC, Rec Range Varies, Avg. Rec ± 3SD, See attached specification sheet

Parameter	Calibration	Calibration Verification	Method Blank	Laboratory Control Spike (LCS)	LCS Duplicate	Matrix Spike (MS)	Matrix Spike Duplicate (MSD), Lab Duplicate	Field Duplicate	Surrogate Recovery
		12 hours, %Diff ≤ 20%							
Turbidity	Single Point calibration plus Calibration Blank, dependent on expected range of use	2nd Source Verification following calibration, %Diff ≤ 10%, Reporting Limit Verification following calibration, %Diff ≤ 10%, Continuing Verification every 10 field samples, %Diff ≤ 10%	<RL	N/A	N/A	N/A	<20% RPD (Lab Dup)	≤25% RPD	N/A
Alkalinity - Carbonate, Bicarbonate	N/A	N/A	<RL	1 per Batch of 20 Samples, 80-120%	1 per Batch of 20 samples, 20% RPD	N/A	<20% RPD (Lab Dup)	≤25% RPD	N/A

1. Pathogen analysis requires a daily positive control and negative control. BSK also performs a daily sterility check on prepared media.

Disposal Procedures

Most of the sample collected for any given monitoring event will be consumed as part of the analyses. However, as noted above, the contract laboratory will retain the remaining sample volume for a period of 60 days from receipt of the samples, approximately 45 days from the completion based on the standard turnaround time of 10 business days.

Once identified for disposal, samples are segregated into groups according to their waste classification. Any samples identified as hazardous based on the outcome of their testing will be put into the laboratory's waste streams and handled in accordance with EPA and DTSC regulations. Samples that are not determined to be hazardous based on the results of their testing will be disposed of according to their preservation type. Acidic and caustic samples will be neutralized and discarded down the sanitary sewer according to the local and Federal pre-treatment guidelines. Samples that are neutral are poured directly into the drain and flushed. Sample containers are rinsed and then recycled according to their material classification.

The laboratory maintains disposal records to indicate when each set of samples has been disposed.

Corrective Action Measures

The laboratory will take a variety of corrective actions for material failures related to sample conditions, holding time failures, preservation problems and quality control failures. All failures and corrective actions will be documented in the form of a data qualifier and / or addressed in detail in the Case Narrative at the beginning of the laboratory report. The details of these responses are included in the various method SOPs and other related supporting documentation. However, the general corrective actions related to a number of common QC failures are listed below:

Calibration Linearity failures are often caused by instrumentation that is in need of maintenance. If a calibration curve fails to meet linearity criteria, the instrument will be repaired and likely a new set of calibration standards prepared. Once complete, the instrument will be recalibrated.

Initial (ICV) and Continuing Calibration (CCV) failures occur periodically on the laboratory instrumentation. Often times these failures are associated with running large numbers of dirty samples which deteriorate the performance of the equipment. ICV failures will generally be handled by the preparation of a new set of calibration standards and ICV standard, and reanalysis of the ICV and CCV. This is often done in conjunction with maintenance performed consistent with that tied to calibration linearity problems.

Method Blank Contamination failures indicate that the ambient laboratory background may be contributing to sample contamination. The response to specific methods will vary but in general, any detection over a Reporting Limit (RL) will result in the re-

preparation and reanalysis of the associated samples unless the sample results are greater than 10x that found in the blank. Certain methods have corrective action requirements for detections above the MDL or at a multiple of the MDL. Those will be addressed on a case by case basis. All detections in the Method Blanks having a material impact on the data as defined by the ILRP QAPP guidelines will be addressed in the report case narrative.

Laboratory Control Spike Recovery and Precision failures are indicative of a problem in the analytical procedure. Recovery failures are generally addressed by a re-preparation and reanalysis of all samples and QC indicators. Several exceptions may be made where recoveries exceed the upper control limit and samples are non-detected for the failed compound. Precision failures will generally follow the same corrective action plan unless the RPD limit is narrower than the acceptance range for Recovery performance. Under those circumstances, the laboratory will not reject the results but will qualify the data to note the failure.

Matrix Spike Recovery and Precision failures indicate that the sample matrix itself may have some adverse effect on the method performance. However, if the LCS/LCSD recoveries meet control criteria, no corrective action will be needed. The problem at that point is assumed to be associated with the sample matrix itself and beyond the reasonable control of the laboratory. Sample results will be qualified and a note will be made in the case narrative. However, repeated failures for the same analyte will trigger an investigation as the ongoing failure may indicate that the method is poorly suited for a particular sample type and should be modified to address the performance issue.

Laboratory Duplicate failure may indicate a problem with sample homogeneity. On a Lab Duplicate failure, the sample itself will be examined for obvious matrix homogeneity issues. If there are no obvious reasons for the nature of the failure, the samples will be re-prepared and reanalyzed. If an obvious cause is determined, the sample results will be qualified and a note made in the case narrative. However, laboratory duplicate failures that occur when sample results are less than 10x the RL will be ignored as the magnitude of the RPD can be disproportionately affected by low sample results.

Field Duplicate failures indicate homogeneity or sampling issues that occur in the field. No corrective action is taken with such failures with the exception of qualifying the data and making a notation in the case narrative.

Surrogate Recovery failures will be addressed on a case by case basis. Samples with failing surrogate recoveries may be biased either high or low. Surrogate failures on clean matrices with no obvious sample interferences will be re-extracted if possible. Repeated failures will be assumed to be caused by matrix interference. If no re-extraction is possible, the data will be qualified. High surrogate failures on non-detected samples will be treated as immaterial to data usability and qualified only to call attention to the failure.

ELEMENT 14: QUALITY CONTROL

The laboratory will perform the following QC measures listed in Table 10 under this Plan.

Table 10: Required Quality Control by Method

	Samples per Batch	Method Blank	LCS / LCSD	MS / MSD	Lab Dup	Surr. Spike	Field Dup
Ammonia	20	X	X	X		N/A	X
Bicarbonate/ Carbonate Alkalinity	20	X	X		X	N/A	X
Carbamates	20	X	X	X		X	X
Glyphosate	20	X	X	X		X	X
Hardness (Calc)	20	X ³	X ³	X ³		N/A	X
Herbicides	20	X	X	X		X	X
Metals	20	X	X	X		N/A	X
Anions	20	X	X	X		N/A	X
OCl Pesticides	20	X	X	X		X	X
OP Pesticides	20	X	X	X		X	X
o-Phosphate	20	X	X	X		N/A	X
Phosphorus	20	X	X	X		N/A	X
Paraquat	20	X	X	X			X
Pathogens	-	X ¹	X ¹	N/A		N/A	X
Pyrethroids	20	X	X	X		X	X
TOC	20	X	X	X		N/A	X
TDS	20	X	X ²		X	N/A	X
TSS	20	X			X	N/A	X
Triazine Pesticides	20	X	X	X		X	X
Turbidity	20	X	N/A	N/A	X	N/A	X
Toxicity	NA	X ⁴	X ⁴	N/A	NA	N/A	X

1. Laboratory performs a sterility check, positive and negative control per day
2. Laboratory analyzes a certified standard reference material for TDS
3. QC for Hardness performed in analysis of Calcium and Magnesium which are used to determine Hardness by calculation
4. Laboratory performs a 0% control per test batch and reference toxicant per test batch or monthly depending on the species.

QC Definitions and Specifications - Chemistry*Method Blank*

The method blank is a simulated sample comprised of a clean, interference-free matrix (typically deionized water) that is carried through the sample preparation and analysis procedure. It is used to determine if the ambient laboratory background is free from contaminants that may influence sample results. The results of the Method Blank are

assessed against the MDL and RL, depending on the method. Contamination in a method blank may require corrective action as described in Element 13.

Laboratory Control Spike / Duplicate (Blank Spike / Duplicate)

The Laboratory Control Spike – sometimes referred to as Blank Spike – is an interference-free matrix that is fortified with the target analyte at a level reasonably expected to be found in the field sample. Alternatively, laboratories typically fortify at a level that is roughly the midpoint of the calibration range. The result obtained for this “spike” is compared to the level of fortification that results in a recovery value. The recovery is compared to a set of control limits to determine if the method is performing as expected.

LCS or BS recovery is determined according to the following calculation:

$$\% \text{ Recovery} = \frac{\text{Result Observed}}{\text{Fortification Level}} \times 100$$

LCS or BS Duplicate results are evaluated not only for recovery but also for Relative Percent Difference (RPD), a measure of precision. RPD is determined by the following calculation:

$$\text{Relative Percent Difference} = \frac{|LCS \text{ Res} - LCSD \text{ Res}|}{\text{Avg} (LCS, LCSD)} \times 100$$

Matrix Spike / Duplicate

The Matrix Spike (MS) is a sample that has been fortified in the same manner as the LCS or BS. The MS result demonstrates the impact of the sample matrix on the method performance. MS performance is also based on recovery that is calculated as follows:

$$\% \text{ Recovery} = \frac{(\text{MS Result} - \text{MS Parent Sample Result})}{\text{Fortification Level}} \times 100$$

The Matrix Spike is also performed in duplicate to provide the data user with an indication of the impact of the sample matrix on the precision or reproducibility of the method. The MS Duplicate is assessed by RPD which is calculated as follows:

$$\text{Relative Percent Difference} = \frac{|MS \text{ Res} - MSD \text{ Res}|}{\text{Avg} (MS, MSD)} \times 100$$

Laboratory and Field Duplicates

A Laboratory Duplicate is a second aliquot of a sample taken from the same container as the original sample that is run in parallel with the original parent sample. The duplicate

performance will indicate if the method and / or sample has some inherent variability that is atypical for the method. Like the LCSD or MSD, the Laboratory Duplicate is assessed based on RPD that is calculated in the same manner, comparing the result of the parent sample to that of the duplicate and dividing by the average of the two observations.

$$\text{Relative Percent Difference} = \frac{|Parent\ Res - Duplicate\ Res|}{Avg\ (Parent, Duplicate)} \times 100$$

A Field Duplicate is a second collection of a sample, captured in its own unique container. The Field Duplicate is treated in the same manner as all other samples and is likewise assessed based on the same RPD calculation shown for the laboratory duplicate.

A failure of either the Laboratory or Field Duplicate indicates a potential lack of homogeneity in the sample collection or subsampling procedures.

- On failure of a Field Duplicate, the laboratory will inspect the sample containers for any observable differences between the primary and duplicate samples. If a material difference is observed (e.g. significant suspended or settled matter, differences in color or other physical characteristics), the laboratory will review both the field logs and the sampling procedure for any potential sources of variation. If there is an indication that a sampling error occurred, then the Coalition will be notified to make a determination regarding the usability and representativeness of the sample. If no problems are identified, the data will be qualified to indicate the discrepancy between results and reported to the Coalition.
- On failure of a Laboratory Duplicate, the laboratory will inspect the individual sample container used for the duplicate to ensure a correct subsampling occurred. If there is no obvious source of error, the laboratory will reanalyze the sample in duplicate to assess the situation. If a repeated error occurs, then the original data will be qualified and reported to the Coalition. If the error is no longer observed, then the original results will be discarded and the reanalysis will be reported. If there is an observable homogeneity issue that the laboratory cannot overcome, the results will be qualified as estimated values and reported to the Coalition.

QC Definitions and Specifications - Microbiology

Method Blank (Sterility Check)

The “method blank” for microbiology is a sterility check conducted on all the materials used in the analysis of all field samples, if the sterility check confirms there to be no ambient microbial background which could contribute to the presence of bacteria in the field samples. Positive growth in a sterility check would indicate that the materials used in

the analysis of the samples may be contaminated and therefore all associated results should be rejected as suspect.

Negative Control

A Negative Control is used to ensure that the media used in the analysis of samples does not support growth for any pathogen other than that specifically targeted by the method. Should a Negative Control exhibit growth, it would indicate that the media in use is not specific enough for the pathogen and that growth observed for the samples may be attributable to species other than that of interest for the project.

Positive Control

The Positive Control sample ensures that the media used in the analyses of a pathogen is suitable for growing the species of interest. If a positive control exhibits no growth, then sample results are suspect as potential false negatives. The positive control must exhibit some growth to prove that the media can support the culturing of the target species.

QC Definitions and Specifications – Toxicology

0% Control

The 0% Control is used to assess the cleanliness of the laboratory environment and the quality of the laboratory grade water used for sample dilution. The control should not experience any mortality, as this would be indicative of a toxic substance in the dilution water which is adding to any toxicity attributable to the sample.

Reference Toxicant

The Reference Toxicant is a known toxicant that is tested with the organisms to evaluate their response. This demonstrates that the method performance is within plus or minus two standard deviations from the mean of past tests conducted with a particular organism.

ELEMENT 15: INSTRUMENT/EQUIPMENT TESTING, INSPECTION, AND MAINTENANCE

The ready availability of equipment shall be maintained by the contract laboratory and the TBWQC as they are responsible for both the field and in-house laboratory analyses

Field Instrumentation / Equipment

Field units are maintained constantly as they are subject to use on applications other than under this Plan. The instruments are used for non ILRP activities, and any indication of failure can quickly be addressed as the need arises. Batteries are replaced on a regular schedule to insure against failure in the field. Backup batteries and other parts subject to failure will be maintained in supply to ensure no material downtime. The instruments are regularly checked for calibration against known standards. Calibration will be documented as required below.

The field sampling crew will be responsible for ensuring that all support equipment is maintained and in good working order. Equipment that is damaged in a way that will adversely affect usage will be replaced. The equipment will be cleaned according to standard operating procedures in place for environmental field sampling prior to the sampling event and between sample monitoring sites.

The field instrumentation requiring Inspection, Maintenance and Calibration includes:

Table 11: BSK Field Instrumentation

Instrument	Make	Model
DO Meter	Oakton	DO 300
EC, pH Meter, Temperature	Oakton	PC 10
Flow Meter	Global Water	FP 211

Table 12: TBWQC Field Instrumentation

Instrument	Make	Model
DO, EC, pH, Temperature Meter	YSI	Pro

Laboratory Instrumentation

The contract laboratories have sufficient redundancy in their instrumentation to recover from the failure of any particular instrument. Calibrations are ongoing, as are MDL studies and other indicators of method performance. The laboratory maintains service contracts for key pieces of equipment where redundant equipment is not feasible due to the substantial cost of replacement.

Compliance with method procedures is a must. Instrument failures or anomalous data are documented in the laboratory report either in the form of a data qualifier or in the case narrative at the beginning of the laboratory report.

Table 13: Laboratory Instrumentation

Instrument	Make	Model
pH, EC, Alkalinity Titrator	Mansci	PC-Titrate
Nutrient Analyzer	Westco	SmartChem 200
Continuous Flow Analyzer	Skalar	3000
Ion Chromatograph	Metrohm	930 Compact IC Flex
HPLC-UV/Vis, Fluor, PDA	Thermo Separations	AS 3000
HPLC-MS/MS	AB Sciex	4000
GC-ECD	Agilent	7890
GC-MS	Agilent	6890/5975, 6890/5973
TOC Analyzer	Tekmar	Phoenix 8000
Turbidimeter	HF Scientific	DRT-15CE
ICP	Perkin Elmer	Optima 8300 RL
ICP-MS	Perkin Elmer	ELAN DRC IIe
Oven	VWR	1380FM

ELEMENT 16: INSTRUMENT/EQUIPMENT CALIBRATION AND FREQUENCY**Field Instrumentation**

Laboratory field technicians and the TBWQC are responsible for ensuring the inspection, maintenance, and when appropriate, the calibration of field instruments and equipment.

Field instruments are calibrated (or verified as being in calibration) prior to the beginning of the sampling event, and rechecked in the field using known standards. Instruments that require calibration checks include the EC, pH, and DO meters listed above. Calibration procedures will be conducted according to the contract laboratory SOPs and consistent with manufacturer recommendations.

See Element 15 for a listing of equipment requiring calibration.

Laboratory Instrumentation

Laboratory analysts and technicians are responsible for the inspection, maintenance, operation and, where appropriate, calibration of their assigned laboratory instrumentation.

Calibration at the laboratory is conducted according to method requirements. Specific schedules are outlined in the laboratory specific SOPs provided in Appendix B (Proprietary copy only). Checks include initial and continuing calibration verifications to demonstrate the instrumentation remains in calibration and operating normally. The laboratory will run a calibration point or a calibration verification check at or below the equivalent of the project reporting limit. This ensures that the instrumentation has adequate sensitivity to achieve the levels needed for the project.

All calibration runs are documented and maintained by the laboratory in a manner consistent with its standard record retention requirements. Any deficiencies will be addressed according to the laboratory standard operating procedures. Corrective actions and additional details will be maintained in the laboratory's log books and raw data. Where applicable, these deficiencies will also be documented in the report Case Narrative should they have any material impact on data usability.

See Element 15 for a listing of the equipment requiring calibration.

ELEMENT 17: INSPECTION / ACCEPTANCE OF SUPPLIES AND CONSUMABLES

The contract laboratory will be solely responsible for the procurement, inspection and acceptance of supplies and consumables. Given the substantial volume of samples processed and the requirements of the ISO-17025 based quality system, the laboratory has policies and procedures in place to qualify and determine the suitability of each material for use. Suppliers of reagents, standards, consumables, parts and other supplies are limited by the laboratory purchasing system to ensure that the laboratory always receives supplies it has determined are suitable for use. A single person within the contract laboratory is responsible for the ordering and receiving of supplies.

Standards and reagents are tracked within the laboratory using a system of identification numbers. This system allows the laboratory to be able to trace the source of all measurements to a specific lot for any given critical supply. This is especially true of all standard and reference materials that serve as the basis for all laboratory calibrations. Certificates of Analysis for analytical standards and reagents are collected and retained by the Laboratory Quality Assurance Manager according to the Laboratory's record retention requirements.

Bottles and sampling supplies are included in this tracking system. Reagents used for preservatives are tracked and each bottle includes a lot number that can be traced to the day it was produced, the person who added the preservative where applicable, and the identity of the preservative used on that day. This allows the lab to trace any potential problems with a sample container back to the production source, permitting a retraction of sample container by lot number if required.

ELEMENT 18: NON-DIRECT MEASUREMENTS

There are no non-direct measurements used in this program. All flow rates within the system are obtained from the hydrologists or watermaster that supervises the delivery of irrigation water and monitors waterway flows. These values are derived based on the known discharges into the designated waterways and validated using flow measurements at key points within defined flow channels along the flow path. The flow rates are accurate to within 10% of the actual flows and deemed sufficiently accurate for the purposes of the program. Flow rates in the form of velocity measurements are one of the field parameters to be determined at the time of sample collection and will be the primary point of comparison when evaluating water flows at the time of collection.

ELEMENT 19: DATA MANAGEMENT

Presently, there are no *In Situ* or continuous measurements being made related to this Plan. Data production begins with field measurements and sample collection. All notes will be recorded on bound logbooks. Copies of the field documentation will be provided to the analytical laboratory for inclusion into the laboratory reports. The office where the sample crew originates will maintain the original records for a period of no less than five years, the same as the record retention policy of the laboratory.

The data generated by the laboratory will exist in both electronic and hardcopy records, each held for a minimum of five years from the date of generation. This includes the Laboratory Information Management System database that houses all the results and supporting data associated with the samples. The contracted laboratory scans all hardcopy records into an electronic archival which is also maintained consistent with the record retention policy.

Hardcopy data is held in a secure location controlled by the laboratory. Access is limited and records are disposed based on standard operating procedure. Electronic data – raw data files, scanned images, Adobe PDF reports, etc., – are held on secure company servers that are backed up daily. Backup media is rotated off site on a scheduled basis, a responsibility of the IT Department.

Data will be provided to the Coalition in electronic format. The analytical report will be an Adobe PDF that includes all results, QC, case narrative, chain of custody and sample receipt documentation. Laboratory raw data, other than the raw data for the toxicity testing, will not be included in the analytical report. However, all laboratory raw data such as chromatograms, spectra, summaries of initial and continuing calibrations, sample injection or sequence logs, prep sheets, etc., will be retained by the laboratory for a minimum of five years and will be provided if specifically requested by the Coalition.

In addition, the laboratory will create a CEDEN and Geotracker ESI compliant electronic data deliverable (EDD) for the SWAMP and GQTMP, respectively, that includes all required data for the programs. The EDD will be verified against the CEDEN data checker (http://ceden.org/CEDEN_checker/Checker/CEDENUpload.php) or Geotracker ESI data checker (<https://geotracker.waterboards.ca.gov/esi>) for content and structure. A copy of the error report will be provided to the Coalition in conjunction with the file for monthly, quarterly and annual reporting. Data from both the primary laboratory and the subcontract lab (toxicity data) will be produced in separate files and sent via email to the Coalition once evaluated.

Data received by the Coalition will be given a cursory review for correct format and completeness. All data, electronic or paper copy, will be filed according to sample date and monitoring site. Electronic format data will be filed in a manner that allows for historical trends and summaries to be analyzed along with quick retrieval for quarterly and annual submittals. The Coalition will work with the contracted laboratory if any issues regarding data are encountered.

ELEMENT 20: ASSESSMENT AND RESPONSE ACTIONS

The Quality Assurance Manager, in cooperation with the Laboratory Coordinators, will review both sampling procedures and laboratory performance annually. Changes in the SOPs used by any of the contracted labs will be communicated between the QA Manager and the Laboratory Coordinators as they occur. Both the QA Manager and the Laboratory Coordinator have “stop work” authority should a situation arise that necessitates an immediate corrective action.

The Laboratory Coordinator will have the responsibility of managing the contracted laboratory. Any issues encountered during the analysis of the samples are to be resolved by the Laboratory Coordinator and then communicated to the QA Manager. Any reported issues at the laboratories will be communicated to the Regional Board as needed and discussed in detail within the Annual Report.

The Laboratory Coordinator will work directly with the Laboratory Project Manager to resolve issues as they occur on any given monitoring event. For ongoing performance issues or to address matters related to the adherence to the QAPP, the Laboratory Coordinator will work directly with the Laboratory Program Manager. These two will meet at least on an annual basis to review the contract lab performance and to address any procedural changes required to ensure ongoing success of the program.

The laboratory QAPPs contained within the attached appendices all address the issue of analyst training and performance, as well as procedures for failed tests. These procedures closely match the Regional Board guidelines for standard laboratory practices and corrective actions.

A copy of the most recent MDL study is to be obtained on at least an annual basis along with a listing of the current SOPs. Material changes in any of the quality control practices, SOPs or other significant procedures may require a revision to this QAPP.

ELEMENT 21: REPORTS TO MANAGEMENT

Activities of the sampling staff are documented and reviewed as part of the submission to the laboratory for the monthly and annual monitoring events. The Laboratory Program Manager will have the responsibility to address any performance issues with the branch office where the sample crew for surface water sampling originated. The TBWQC Technical lead shall address performance issues of groundwater sampling staff. Anomalies or other failures will trigger a Non-Conformance Report ultimately leading to a Corrective Action/Preventative Action (CAPA) event. This will include a root cause determination and a remedial corrective action where necessary. These corrective action reports will be made available to the Laboratory Coordinator on request.

As a result of the meetings between the Laboratory Coordinator and the Laboratory Program Manager, the Coordinator will prepare a summary report of the outcomes of the meeting. The report will contain details on the performance of the contract laboratory, improvements or enhancements to be made that will improve the overall success of the Plan, and any remedial measures taken to address potential performance issue leading to deficiencies in data deliverables.

Quarterly reports (CEDEN formatted data) and annual reports (GeoTracker ESI) are prepared by the Laboratory Coordinators and submitted to the QA Manager for final review. Once the review is completed, the Project Coordinator will prepare a cover letter to accompany the data for the Regional Board. The Project Coordinator is responsible for the drafting of the yearly report for submission to the Regional Board.

Reports submitted to the Regional Board will be sent to the liaison within the Fresno, CA office. Additional copies of the integrated report are kept at the Coalition office.

ELEMENT 22: DATA REVIEW, VERIFICATION AND VALIDATION

Data submitted to the Coalition has undergone a thorough review process at the contracted labs. A statement that the data has been reviewed and is acceptable is provided with the lab report linked to each chain of custody.

The laboratories follow a three tier review process. The primary analyst conducting the analysis is responsible for the generation of results. This analyst performs a double check of their work as part of the reporting process. Upon completion, the data package is then handed off to a peer review, most often the immediate supervisor or another qualified peer reviewer. The peer review consists of a check against all method requirements with documentation applied to any deficiencies. Once all results have undergone a peer or secondary review, the Laboratory Project Manager will review the report in its entirety, looking for agreement within the results and consistency with project requirements. Partial results may be provided to the Coalition on a preliminary basis, if the results have been reviewed through the three-tier review process.

For this QAPP, the report will undergo a final review by the Laboratory Program Manager or his designee. This person checks reports against the requirements of the QAPP and prepares the case narrative. This person generates the CEDEN electronic deliverable and evaluates the content using the CV RDC electronic data checker. Once complete, the report is finalized and sent to the Coalition.

Once received by the Coalition, the data is further reviewed by the QA Manager for exceedances, and the appropriate communication reports are prepared, if necessary, to the Regional Board.

ELEMENT 23: VERIFICATION AND VALIDATION METHODS

The Coalition QA Manager is responsible for the final review and determination of the validity and usability of the data. The determination of completeness is performed at both the level of the field activities and the in-house laboratory activities. Any questions or anomalies resulting from this review will be addressed directly with the laboratory prior to making the final determination. The overall completeness goal for the project is 90%.

ELEMENT 24: RECONCILIATION WITH USER REQUIREMENTS

The purpose of the sampling program is to determine if any constituents of concern exceed water quality standards in the water samples. If such detections are made, the Coalition will then open an inquiry as to the persistence of the detection (is it in more than one site, is it still present in the next sample period), review the conditions prior to the sampling event that produced the detection, and begin to research the potential sources of the detection.

The data, as reported by the lab, is considered valid if no problems are identified within the laboratory report and case narrative. In the event that the laboratory data quality indicators do not meet the criteria listed in Table 8 (or exceed other requirements listed in the cited analytical method), then the data will be annotated with data qualifiers that identify the deficiency. Laboratory reports containing notations that indicate QC failures or other issues that do not meet QAPP requirements will need to be assessed for impact. Not all failures result in the rejection of data but scrutiny will be applied to all failures or QAPP deviations. It is the responsibility of the QA Manager to make the final determination of data usability and its suitability for intended use. All QC failures or other known deficiencies will be indicated on the laboratory Certificate of Analysis, either in the form of a data qualifier and/or noted in the detailed Case Narrative provided therein. These deficiencies represent the possible limitations on the use of the data but will nonetheless be reported in order for the Coalition and Board to determine their suitability for use.

All data will be uploaded into the SWAMP Information Management System or GeoTracker ESI. At this point the Board may use the data in the overall evaluation of the surface water and groundwater quality in the Tule Basin watershed. Future decisions for water regulations will be made, in part, on the information provided under this Plan.

Questions will always arise when a toxicity level shows an exceedance, but the chemistry data taken at the same time fails to show a toxic substance that might cause the problem. Given the relatively limited list of monitoring parameters versus the number of both known and unknown potential contaminants, it is not inconceivable that a constituent could contribute to toxicity but fail to be identified from the chemistry testing. Continuing discrepancies between the outcome of the toxicity testing and the chemistry testing should be further evaluated in an attempt to determine the possible presence of a persistent, harmful parameter.

Any concerns or unanswered questions that arise from the data will be addressed as comments or footnotes within the written reports submitted to the Regional Board.

ELEMENT 25: DEFINITIONS

Term	Definition
BPO	Basin Plan Objective
BS/BSD	Blank Spike / Blank Spike Duplicate
CAPA	Corrective Action / Preventative Action
CEDEN	California Environmental Data Exchange Network
CA ELAP	California Environmental Laboratory Accreditation Program
CV RDC	Central Valley Regional Data Center
EDD	Electronic Data Deliverable
ESI	Electronic Submittal of Information
General Order (Order)	CA Central Valley Regional Board Order #R5-2013-0120 (Amended by R5-2014-0143 and R5-2015-0115)
GQTMP	Groundwater Quality Trend Monitoring Program
GQTMW	Groundwater Quality Trend Monitoring Workplan
ISO	International Organization for Standardization
IT	Information Technology
LCS/LCSD	Laboratory Control Spike / Laboratory Control Spike Duplicate. Often used interchangeably with BS/BSD.
ILRP	Irrigated Lands Regulatory Program
MDL	Method Detection Limit
MRP	Monitoring and Reporting Program
MS/MSD	Matrix Spike / Matrix Spike Duplicate
NTC	
PQL	Practical Quantitation Limit
QA	Quality Assurance
QAPP	Quality Assurance Program Plan
QC	Quality Control
RDC	Regional Data Center
RL	Reporting Limit
RPD	Relative Percent Difference
SOP	Standard Operating Procedure
SSJVWQC	Southern San Joaquin Valley Water Quality Coalition
SWAMP	Surface Water Ambient Monitoring Program
SWMP (Plan)	Surface Water Monitoring Plan (Tule Basin SWMP)
TBWQC	Tule Basin Water Quality Coalition
TIE	Toxicity Identification Evaluation

APPENDIX A.1

Chain of Custody



14114 Stanislaus St., Fresno, CA 93706
 (559) 497-2888 · Fax (559) 497-2893
 www.bskaassociates.com

Turnaround Time Request
 Standard - 10 business days
 Rush (Surcharge may apply)
 Date needed: _____

**ANALYTICAL
CHAIN OF CUSTODY**

Company/Client Name: _____		Report Attention*: _____		Temp: _____		Invoice To*: _____		Phone*: _____		Fax: _____	
Address*: _____		City*: _____		State*: _____		Zip*: _____		E-mail*: _____			
Project: _____		Project # _____		How would you like to receive your completed results? <input type="checkbox"/> E-MAIL <input type="checkbox"/> Fax <input type="checkbox"/> Mail		Regulatory Compliance <input type="checkbox"/> EDT to California SWRCB (Drinking Water) System Number: _____					
Reporting Options: <input type="checkbox"/> Trace (J-Pag) <input type="checkbox"/> Swamp <input type="checkbox"/> EDO Type: _____		Regulatory Carbon Copies <input type="checkbox"/> SWRCB (Drinking Water) <input type="checkbox"/> Mendoc Co <input type="checkbox"/> Fresno Co <input type="checkbox"/> Madras Co <input type="checkbox"/> Tulare Co		Other: _____		Geotracker #: _____					
Sampler Name (Printed/Signature)*: _____		Matrix Types: SW=Surface Water BW=Borehole Water GW=Ground Water WWT=Wastewater STW=Storm Water DW=Drinking Water SCS=Solid		Comments / Station Code / WTRAX _____							
#	Sample Description*	Sampled*		Matrix*	Comments / Station Code / WTRAX	Received by: (Signature and Printed Name)		Company			
		Date	Time			Date	Time	Date	Time	Date	Time

APPENDIX A.2

Field Sample Collection Logs

ILRP/SWAMP 2.5 Discharge Worksheet						
Coalition Name:					DATE (mm/dd/yyyy):	
StationID & Name:					FIRST SAMPLE TIME:	
ProjectID:			Method: USGS (bridge), USGS (wading), culvert, other:			
Left Edge Water (LEW):			Start Time (24 hr):		Discharge (cfs):	
Right Edge Water (REW):			End Time (24 hr):		Discharge calculated by:	
#	Angle (if from bridge)	Interval Midpoint (meters or feet)	Interval Depth (meters or feet)	% Depth (from surface)*	Revolutions/Velocity (m/s or f/s)	Notes
1				0.2 / 0.8 or 0.6		
2				0.2 / 0.8 or 0.6		
3				0.2 / 0.8 or 0.6		
4				0.2 / 0.8 or 0.6		
5				0.2 / 0.8 or 0.6		
6				0.2 / 0.8 or 0.6		
7				0.2 / 0.8 or 0.6		
8				0.2 / 0.8 or 0.6		
9				0.2 / 0.8 or 0.6		
10				0.2 / 0.8 or 0.6		
11				0.2 / 0.8 or 0.6		
12				0.2 / 0.8 or 0.6		
13				0.2 / 0.8 or 0.6		
14				0.2 / 0.8 or 0.6		
15				0.2 / 0.8 or 0.6		
16				0.2 / 0.8 or 0.6		
17				0.2 / 0.8 or 0.6		
18				0.2 / 0.8 or 0.6		
19				0.2 / 0.8 or 0.6		
20				0.2 / 0.8 or 0.6		
21				0.2 / 0.8 or 0.6		
22				0.2 / 0.8 or 0.6		
23				0.2 / 0.8 or 0.6		
24				0.2 / 0.8 or 0.6		
25				0.2 / 0.8 or 0.6		
26				0.2 / 0.8 or 0.6		
27				0.2 / 0.8 or 0.6		
28				0.2 / 0.8 or 0.6		
29				0.2 / 0.8 or 0.6		

*two measurement should be taken (0.2 and 0.8 from the surface of the water) if the depth is greater than 0.76m (2.5ft).

APPENDIX A.4

Example Field and Transport Completeness Worksheet

Field Data Completeness Worksheet					
	<i>Date Sampled</i>				
		Sampling Locations			
Activity		Sample Point 1	Sample Point 2	Sample Point 3	Sample Point 4
Field Sampling					
Water Present at Location?					
Photo documentation captured?					
Field Equipment Rinsed?					
All containers for all samples filled?					
Sample Labels Verified to COC?					
Lat. / Long. Recorded?					
Field Conditions Recorded?					
Field Measurements Collected					
Flow					
Temp					
pH					
EC					
Dissolved Oxygen					
Sample Transport					
Were samples packed on ice?					
COC signed by sampler?					
Was COC included in cooler?					
Sample Receipt					
Samples received within temperature?					
If no, received on ice on date collected?					
All bottles unbroken and intact?					
Bottle labels agree with COC?					
Were bottles correct for tests requested?					
Sufficient sample received for all tests?					
Arrived at lab within hold times?					
Passing Criteria		0	0	0	0
Total Assessments		0	0	0	0
% Complete					
% Completeness - Field Activities					

Appendix F

Groundwater Sampling Form



Groundwater Sampling

Job Name: _____ Well No./ I.D.: _____
 Job Number: _____ Well Type: Monitor Extraction Other: _____
 Recorded By: _____ Well Material: PVC St. Steel Other: _____
 (Signature) Date: _____ Time: _____
 Sampled By: _____

WELL PURGING

PURGE VOLUME Casing Diameter (D inches): <input type="checkbox"/> 2 <input type="checkbox"/> 4 <input type="checkbox"/> 6 <input type="checkbox"/> Other: _____ Total Depth of Casing (TD in feet BTOC): _____ Water Level Depth (WL in feet BTOC): _____ Number of well volumes to be purged (# Vols): <input type="checkbox"/> 3 <input type="checkbox"/> 4 <input type="checkbox"/> 5 <input type="checkbox"/> 10 <input type="checkbox"/> Other: _____	PURGE METHOD <input type="checkbox"/> Bailer - Type: _____ <input type="checkbox"/> Submersible <input type="checkbox"/> Centrifugal <input type="checkbox"/> Bladder; Pump No.: _____ <input type="checkbox"/> Other Type: _____ PUMP INTAKE SETTING <input type="checkbox"/> Near <input type="checkbox"/> Bottom <input type="checkbox"/> Near Top Other: _____ Depth in ft (BTOC): _____ Screen Interval in ft (BTOC): From _____ To _____
--	---

PURGE VOLUME CALCULATION:

$$\left(\frac{\text{TD (feet)}}{\text{D (Inches)}} \right) - \left(\frac{\text{GW (feet)}}{\text{D (Inches)}} \right) \cdot \text{D (Inches)}^2 \cdot \text{\# Vols} \cdot .0408 = \text{Calculated Purge Volume (gallons)}$$

PURGE TIME Start: _____ Stop: _____ Elapsed: _____	PURGE RATE Initial: _____ gpm Final: _____ gpm	ACTUAL PURGE VOLUME _____ = _____ gallons
---	---	---

FIELD PARAMATER MEASURMENTS:					OBSERVATIONS DURING PURGING (Well Condition, Turbidity, Color, Odor):
Minutes Since Pumping Began:	pH	Cond. (μ Mhos/cm)	T <input type="checkbox"/> C° <input type="checkbox"/> F°	Other:	
					DISCHARGE WATER DISPOSAL: <input type="checkbox"/> Sanitary Sewer <input type="checkbox"/> Storm Sewer <input type="checkbox"/> Other: _____
Meter Nos.:					

WELL SAMPLING

SAMPLING METHOD <input type="checkbox"/> Same As Above <input type="checkbox"/> Bailer - Type: _____ <input type="checkbox"/> Submersible <input type="checkbox"/> Centrifugal <input type="checkbox"/> Bladder; Pump No.: _____	<input type="checkbox"/> Grab - Type: _____ <input type="checkbox"/> Other - Type: _____
---	---

SAMPLE DISTRIBUTION Sample Series: _____					
Sample No.	Volume/ Cont.	Analysis Requested	Preservatives	Lab	Comments

QUALITY CONTROL SAMPLES					
Duplicate Samples		Blank Samples		Other Samples	
Original Sample No.	Duplicate Sample No.	Type	Sample No.	Type	Sample No.

TULE SUBBASIN COORDINATION AGREEMENT ATTACHMENT 2

Tule Subbasin Setting

July 2022

Prepared for
Tule Subbasin Technical Advisory Committee

Prepared by

Thomas Harder, P.G., CH.G.
Principal Hydrogeologist

Benjamin Lewis, P.G., CH.G.
Associate Hydrogeologist



Table of Contents

CHAPTER 2: TULE SUBBASIN SETTING §354.12	1
2.1 Hydrogeologic Conceptual Model §354.14	1
2.1.1. Sources of Data	2
2.1.2. Geologic Setting §354.14 (b)(1)	3
2.1.3. Lateral Basin Boundaries §354.14 (b)(2)	5
2.1.4. Bottom of Basin §354.14 (b)(3)	6
2.1.5. Surface Water Features §354.14 (d)(5)	7
2.1.5.1. Tulare Lake	7
2.1.5.2. Lake Success	7
2.1.5.3. Tule River	7
2.1.5.4. Deer Creek	8
2.1.5.5. White River	8
2.1.5.6. Imported Water §354.14 (d)(6)	9
2.1.6. Areas of Groundwater Recharge and Discharge §354.14 (d)(4)	9
2.1.7. Principal Aquifers and Aquitards §354.14 (b)(4)	10
2.1.7.1 Aquifer Formations §354.14 (b)(4)(A)	10
2.1.7.2 Aquifer Physical Properties §354.14 (b)(4)(B)	12
2.1.7.3 Geologic Structures that Affect Groundwater Flow §354.14 (b)(4)(C)	13
2.1.7.4 Aquifer Water Quality §354.14 (b)(4)(D)	14
2.1.7.5 Aquifer Primary Uses §354.14 (b)(4)(E)	15
2.1.8. Uncertainty in the Hydrogeologic Conceptual Model §354.14 (b)(5)	15
2.2 Groundwater Conditions §354.16	15
2.2.1 Groundwater Occurrence and Flow §354.16 (a)	16
2.2.2 Groundwater Storage §354.16 (b)	17
2.2.3 Seawater Intrusion §354.16 (c)	17
2.2.4 Groundwater Quality Issues §354.16 (d)	18
2.2.5 Land Subsidence §354.16 (e)	20
2.2.6 Interconnected Surface Water Systems §354.16 (f)	21
2.2.7 Groundwater Dependent Ecosystems §354.16 (g)	21
2.3 Water Budget §354.18	22



2.3.1.	Surface Water Budget	22
2.3.1.1	Surface Water Inflow §354.18 (b)(1)	23
2.3.1.1.1.	Precipitation.....	23
2.3.1.1.2.	Stream Inflow.....	23
2.3.1.1.3.	Imported Water	24
2.3.1.1.4.	Discharge to Crops from Wells	24
2.3.1.1.5.	Municipal Deliveries from Wells.....	24
2.3.1.2	Surface Water Outflow	25
2.3.1.2.1	Areal Recharge from Precipitation	25
2.3.1.2.2	Streambed Infiltration (Channel Loss)	26
2.3.1.2.3	Canal Losses	28
2.3.1.2.4	Managed Recharge in Basins	29
2.3.1.2.5	Deep Percolation of Applied Water	30
2.3.1.2.6	Evapotranspiration	32
2.3.1.2.7	Surface Water Outflow	34
2.3.2.	Groundwater Budget §354.18 (b)(2).....	34
2.3.2.1	Sources of Groundwater Recharge §354.18 (b)(2)	35
2.3.2.1.1	Areal Recharge.....	35
2.3.2.1.2	Groundwater Recharge from the Tule River.....	35
2.3.2.1.3	Groundwater Recharge from Deer Creek.....	35
2.3.2.1.4	Streambed Infiltration in the White River	35
2.3.2.1.5	Groundwater Recharge from Imported Water Deliveries	36
2.3.2.1.6	Recycled Water	36
2.3.2.1.7	Deep Percolation of Applied Water from Groundwater Pumping	36
2.3.2.1.8	Release of Water from Compression of Aquitards	36
2.3.2.1.9	Subsurface Inflow	37
2.3.2.1.10	Mountain Front Recharge.....	37
2.3.2.2	Sources of Groundwater Discharge §354.18 (b)(3)	37
2.3.2.2.1	Municipal Groundwater Pumping	38
2.3.2.2.2	Agricultural Groundwater Pumping.....	38
2.3.2.2.3	Groundwater Pumping for Export Out of the Tule Subbasin	38
2.3.2.2.4	Subsurface Outflow	38
2.3.2.3	Changes in Groundwater Storage §354.18 (b)(4)	38



2.3.2.4	Overdraft §354.18 (b)(5).....	39
2.3.2.5	Water Year Type §354.18 (b)(6).....	39
2.3.2.6	Sustainable Yield §354.18 (b)(7)	39
2.3.3.	Current Water Budget §354.18 (c)(1).....	43
2.3.4.	Historical Water Budget §354.18 (c)(2)	44
2.3.5.	Projected Water Budget §354.18 (c)(3).....	45
2.4	Management Areas §354.20	46
2.4.1	Criteria for Management Areas §354.20 (b)(1)	47
2.4.2	Minimum Thresholds and Measurable Objectives §354.20 (b)(2).....	49
2.4.3	Monitoring Plan §354.20 (b)(3).....	49
2.4.4	Coordination with Adjacent Areas §354.20 (b)(4)	50
2.5	References	51

Tables

2-1	Summary of Active Cleanup Sites within the Tule Subbasin
2-2a	Historical Surface Water Budget - Inflow
2-2b	Historical Surface Water Budget - Outflow
2-3	Historical Groundwater Budget
2-4	Estimate of Sustainable Yield
2-5	Historical Planned vs. Actual Water Deliveries
2-6	Summary of Planned Projects Exclusive of Transitional Pumping
2-7	Planned Transitional Pumping By GSA
2-8a	Projected Future Surface Water Budget – Inflow
2-8b	Projected Future Surface Water Budget – Outflow
2-9	Projected Future Groundwater Budget

Figures

2-1	Regional Map
2-2	Tule Subbasin Area
2-3	Jurisdictional Areas
2-4	Geology and Cross Section Locations
2-5	Conceptual Cross Section A-A'



- 2-6 Conceptual Cross Section B-B'
- 2-7 Surface Water Features in the Tule Subbasin
- 2-8 Soil Map of the Tule Subbasin
- 2-9 Favorable Areas for Recharge
- 2-10 Upper Aquifer Hydraulic Conductivity
- 2-11 Lower Aquifer Hydraulic Conductivity
- 2-12 Upper Aquifer Specific Yield
- 2-13 Lower Aquifer Storage Properties
- 2-14a Arsenic Concentrations
- 2-14b Nitrate as N Concentrations
- 2-14c Hexavalent Chromium Concentrations
- 2-14d Dibromochloropropane (DBCP) Concentrations
- 2-14e 1,2,3-Trichloropropane (TCP) Concentrations
- 2-14f Tetrachloroethene (PCE) Concentrations
- 2-14g Chloride Concentrations
- 2-14h Total Dissolved Solids Concentrations
- 2-14i Perchlorate Concentrations
- 2-15a Chloride Concentrations
- 2-15b Sodium Concentrations
- 2-15c Total Dissolved Solids Concentrations
- 2-16 Active Cleanup Sites in the Tule Subbasin
- 2-17 Spring 2017 Upper Aquifer Groundwater Elevation Contour Map
- 2-18 Fall 2017 Upper Aquifer Groundwater Elevation Contour Map
- 2-19 Fall 2010 Lower Aquifer Groundwater Elevation Contour Map
- 2-20 Upper Aquifer Groundwater Level Hydrographs
- 2-21 Lower Aquifer Groundwater Level Hydrographs
- 2-22 Comparison of Upper Aquifer and Lower Aquifer Groundwater Levels
- 2-23 Cumulative Change in Groundwater Storage
- 2-24 Land Subsidence in the Tule Subbasin – 1987 – 2007
- 2-25 Land Subsidence in the Tule Subbasin – 2007 – 2011
- 2-26 Depth to Groundwater and Areas of Potential Groundwater Dependent Ecosystems



- 2-27 Isohyetal Map
- 2-28 Historical Annual Precipitation – Porterville Station
- 2-29 Correlation of Deer Creek and White River Monthly Streamflow
- 2-30 Applied Water to Irrigated Agriculture by Source
- 2-31 Tule Groundwater Subbasin Historical Crop Patterns
- 2-32 Distribution Plot of Sustainable Yield Uncertainty
- 2-33 Tule Subbasin GSA Management and Monitoring Areas
- 2-34 Groundwater Level Monitoring Network
- 2-35 Groundwater Quality Monitoring Network
- 2-36 Land Subsidence Monitoring Network

Appendices

- A. Lower Tule River Irrigation District GSA Water Budgets, Land Surface Elevations at Representative Monitoring Sites, and RMS Groundwater Elevation Hydrographs
- B. Eastern Tule GSA Water Budgets, Land Surface Elevations at Representative Monitoring Sites, and RMS Groundwater Elevation Hydrographs
- C. Delano-Earlimart Irrigation District GSA Water Budgets, Land Surface Elevations at Representative Monitoring Sites, and RMS Groundwater Elevation Hydrographs
- D. Pixley Irrigation District GSA Water Budgets, Land Surface Elevations at Representative Monitoring Sites, and RMS Groundwater Elevation Hydrographs
- E. Tri-County Water Authority GSA Water Budgets, Land Surface Elevations at Representative Monitoring Sites, and RMS Groundwater Elevation Hydrographs
- F. Alpaugh Irrigation District GSA Water Budgets, Land Surface Elevations at Representative Monitoring Sites, and RMS Groundwater Elevation Hydrographs



CHAPTER 2: TULE SUBBASIN SETTING §354.12

§ 354.12. Introduction to Basin Setting

This Subarticle describes the information about the physical setting and characteristics of the basin and current conditions of the basin that shall be part of each Plan, including the identification of data gaps and levels of uncertainty, which comprise the basin setting that serves as the basis for defining and assessing reasonable sustainable management criteria and projects and management actions. Information provided pursuant to this Subarticle shall be prepared by or under the direction of a professional geologist or professional engineer.

The Tule Subbasin is located in the southern portion of the San Joaquin Valley Groundwater Basin in the Central Valley of California (see Figure 2-1). The area of the Tule Subbasin is defined by the latest version of CDWR Bulletin 118 (CDWR, 2016) and is shown on Figures 2-1 and 2-2. The Tule Subbasin area is approximately 744 square miles (475,895 acres) and includes the jurisdictional areas of multiple water management and service entities. The subbasin has been divided into seven individual Groundwater Sustainability Agencies (GSAs): Eastern Tule GSA, Lower Tule River GSA, Pixley GSA, Delano-Earlimart GSA, Alpaugh GSA, Tri-County Water Authority GSA, and Tulare County GSA (see Figure 2-3).

Communities within the subbasin include Porterville, Tipton, Pixley, Earlimart, Richgrove, Ducor and Terra Bella (see Figure 2-2). Neighboring CDWR Bulletin 118 subbasins include the Kern County Subbasin to the south, the Tulare Lake Subbasin to the west, and the Kaweah Subbasin to the north.

2.1 Hydrogeologic Conceptual Model §354.14

§ 354.14. Hydrogeologic Conceptual Model

(a) Each Plan shall include a descriptive hydrogeologic conceptual model of the basin based on technical studies and qualified maps that characterizes the physical components and interaction of the surface water and groundwater systems in the basin.

The hydrogeologic conceptual model is a description of the groundwater flow system of the Tule Subbasin and how it interacts with surface water and land use of the area. The conceptual model includes a description of the geologic setting, geologic structure, and boundary conditions including the principal aquifers and aquitards. The hydrogeologic conceptual model of the Tule Subbasin, as described herein, has been developed in accordance with the requirements of California Code of Regulations, Title 23, Division 2, Chapter 1.5, Subchapter 2, Article 5, Subarticle 2 (§354.14) and in consideration of California Department of Water Resources' (CDWR) Best Management Practices (BMP) for the preparation of hydrogeologic conceptual models. The hydrogeologic conceptual model forms the basis for the numerical groundwater flow model of the subbasin.



2.1.1. Sources of Data

Compilation, review and analysis of multiple types of data were necessary to develop the hydrogeologic conceptual model and water budget of the Tule Subbasin. The various types of data included geology, soils/lithology, hydrogeology, surface water hydrology, climate, crop types/land use, topography, remote sensing, and groundwater recharge and recovery. Data were obtained from multiple sources:

Geological Data including geologic maps and cross sections were obtained from the United States Geological Survey (USGS), the California Geological Survey (CGS), and Kenneth D. Schmidt & Associates (KDSA) (Schmidt, 2018). Geophysical logs were obtained from the California Division of Oil, Gas and Geothermal Resources (DOGGR), Angiola Water District, Alpaugh Irrigation District, Kern-Tulare Water District (KTWD), KDSA, and private well owners.

Soils/Lithological Data were obtained from drillers' logs and reports from the CDWR, the City of Porterville, the USGS and the United States Department of Agriculture (USDA).

Hydrogeological Data including groundwater levels and pumping tests were obtained from the California Statewide Groundwater Elevation Monitoring (CASGEM) website, the Deer Creek and Tule River Authority (DCTRA), Angiola Water District, Alpaugh Irrigation District, KTWD, Delano-Earlimart Irrigation District (DEID), the City of Porterville, Kern County Water Agency, 4Creeks Inc., Schmidt (2011) and Schmidt (2018). Additional hydrogeological information was obtained from USGS reports, Semitropic Water Storage District Groundwater Banking Project Biennial Reports, and the Tulare Lake Bed Groundwater Management Plan.

Groundwater Quality Data including nitrate and electrical conductivity (EC) data from the Tule Basin Water Quality Coalition, multiple reports and studies associated with the Tulare Lakebed Municipal Delisting program, and contaminants identified in the California State Water Resources Control Board Geotracker website (Geotracker, 2018).

Groundwater Recharge and Recovery Data including spreading basin locations and dimensions, artificial recharge, water well construction, well locations, groundwater production, surface water diversions, canal losses, and river losses were obtained from Lower Tule River Irrigation District (LTRID), CDWR, Tule River Association (TRA) annual reports, and DCTRA annual reports.

Hydrological (i.e. Surface Water) Data consisting of stream gage data along the Tule River, Deer Creek, and White River were obtained from the USGS, DCTRA reports and TRA annual reports. Imported water deliveries were obtained from the United States Bureau of Reclamation (USBR) and the individual agencies within the subbasin.

Climate Data was acquired from CDWR's California Irrigation Management Information System (CIMIS) and the Western Regional Climate Center website.



Land Use Data was obtained from the CDWR, LTRID, the Kern County Department of Agriculture and Measurement Stands, and the USGS Earth Resources Observation and Science Center. Political boundaries were obtained from the California Cal-Atlas Geospatial Clearinghouse, Kern-Tulare Water District, and the LTRID.

In addition to the various types of data, numerous historical reports on the geology, hydrogeology and groundwater management of the Tule Subbasin were reviewed and analyzed. These reports included USGS publications, CDWR reports and bulletins, consultant reports, and academic publications. Publications relied on for the hydrogeological conceptual model and water budget are summarized in the References Section (Section 2.5).

2.1.2. Geologic Setting §354.14 (b)(1)

§ 354.14. (b) The hydrogeologic conceptual model shall be summarized in a written description that includes the following:

- (1) The regional geologic and structural setting of the basin including the immediate surrounding area, as necessary for geologic consistency.
- (2) Lateral basin boundaries, including major geologic features that significantly affect groundwater flow.

The Tule Subbasin is located in the Tulare Lake Hydrologic Region of the Central Valley of California (see Figure 2-1). The Central Valley is a geographically significant structural depression that extends from the Cascade Range on the north to the Tehachapi Mountains on the south (Faunt, 2009). The Central Valley groundwater basin has been subdivided on a regional scale into the Sacramento Valley Groundwater Basin north of the Sacramento River Delta, and the San Joaquin Valley Groundwater Basin south of the Sacramento River Delta. The Tulare Lake Hydrologic Region is located in the southern portion of the San Joaquin Valley Groundwater Basin. The Tulare Lake Hydrologic Region is defined by a surface water drainage watershed that includes the Sierra Nevada Mountains to the east, the Tehachapi Mountains to the south and southeast, and the Coast Ranges to the west. The northern boundary of this hydrologic region is defined by the drainage divide between the San Joaquin River to the north and the Kings River to the south.

The portion of the Central Valley structural depression that is beneath the Tulare Lake Hydrologic Region is filled with marine and nonmarine sediments, which extend to depths of more than 32,000 feet in places (Planert and Williams, 1995). The deepest sediments were deposited within a marine environment associated with an inland sea that inundated the valley between 200 million years ago (Jurassic Period) and 2 million years ago (end of the Tertiary Period) (Croft, 1972). The deeper marine sediments are overlain by as much as 9,000 ft of nonmarine continental deposits associated with Quaternary (2 million years to present) lacustrine and alluvial deposition (Planert and Williams, 1995). The current depositional environment consists of multiple coalescing alluvial



fans along the basin margins with localized lacustrine deposits at the terminus of the fans in the central portion of the basin.

The Tule Subbasin is located on a series of coalescing alluvial fans that extend toward the center of the valley from the Sierra Nevada Mountains (see Figure 2-4). The alluvial fans merge with lacustrine deposits of the Tulare Lake bed in the western portion of the subbasin. Land surface elevations within the Tule Subbasin range from approximately 850 ft above mean sea level (amsl) along the eastern margins of the subbasin to approximately 180 ft amsl at the western boundary (see Figure 2-4).

Geologic formations observed at the land surface and in the subsurface beneath the Tule Subbasin can be grouped into five generalized geologic units, described below in order of increasing age:

Unconsolidated Continental Deposits – These sediments consist of fluvial (i.e. streambed deposits), alluvial, flood plain, and lacustrine (i.e. lake bed) deposits (labeled “surficial deposits” on Figure 2-4). The unconsolidated continental deposits range in thickness from 0 ft at the eastern contact with the Sierra Nevada Mountains to more than 3,000 ft near the margins of Tulare Lake in the western part of the subbasin (see Figure 2-5; Lofgren and Klausing, 1969). Subsurface alluvial sediments consist of highly stratified layers of more permeable sand and gravel interbedded with lower permeability silt and clay. Clear correlation of individual sand or clay layers laterally across the Tule Subbasin is difficult due to the interbedded nature of the sediments. However, it is noted that the thickness of clay sediments in the upper 1,000 ft below ground surface (bgs) generally increases in the vicinity of Tulare Lake. The unconsolidated continental deposits form the primary groundwater reservoir in the Tule Subbasin.

The unconsolidated continental deposits range in age from recent in near-surface stream channels to Upper Pliocene (approximately 2.6 million years before present) at depth. In the eastern portion of the Tule Subbasin, Pleistocene sediments (2.6 million to 11,700 years before present) crop out at the land surface along the base of the Sierra Nevada Mountains, forming what is referred to as the dissected uplands (Lofgren and Klausing, 1969). These older continental deposits are semi-consolidated and contain a high percentage of clay. As such, they generally do not yield significant water to wells.

The lowermost portion of unconsolidated continental deposits is generally correlated with the Tulare Formation. The Tulare Formation is notable in that it includes the Corcoran Clay, a regionally extensive confining layer that has also been referred to as the “E-Clay” (see Figure 2-5) (Frink and Kues, 1954). The Corcoran Clay consists of a Pleistocene diatomaceous fine-grained lacustrine deposit (primarily clay; Faunt, 2009). In the Tule Subbasin, the Corcoran Clay is as much as 150 ft thick beneath the Tulare Lake bed but becomes progressively thinner to the east, eventually pinching out immediately east of Highway 99 (Lofgren and Klausing, 1969).



Pliocene Marine Deposits – These sediments underlie the continental deposits and consist of consolidated to loosely consolidated marine siltstone with minor interbedded sandstone beds. The marine siltstone unit thickens to the west, ranging from approximately 500 ft thick near State Highway 65 to more than 1,600 ft beneath State Highway 99 (Lofgren and Klausning, 1969; see Figures 2-5 and 2-6). The marine siltstone beds dip sharply from the base of the Sierra Nevada Mountains on the east to the central portion of the valley in the west. The Pliocene marine strata have relatively low permeability and do not yield significant water to wells.

Santa Margarita Formation – This formation occurs beneath the Pliocene marine strata and consists of Miocene (approximately 5.3 to 23 million years before present) sand and gravel that is relatively permeable and yields water to wells. The formation is approximately 150 to 520 feet thick and occurs at depths ranging from 1,200 feet near State Highway 65 to greater than 3,000 feet beneath State Highway 99. This formation is a significant source of groundwater to wells in the southeastern portion of the Tule Subbasin near the community of Richgrove.

Tertiary Sedimentary Deposits – Beneath the Santa Margarita Formation exists an interbedded assemblage of semi-consolidated to consolidated sandstone, siltstone and claystone of Tertiary age (approximately 2.6 to 66 million years before present). Some irrigation wells in the southeastern part of the Tule Subbasin are known to produce fresh water from the Olcese Sand Formation, which is in the uppermost portion of the unit (Ken Schmidt, 2019. Personal Communication). The water quality of the groundwater in the Tertiary sedimentary deposits becomes increasingly saline to the southwest and most of the groundwater in the unit is not useable for crop irrigation or municipal supply except near Highway 65.

Granitic Crystalline Basement – Sedimentary deposits beneath the Tule Subbasin are underlain by a basement consisting of Mesozoic granitic rocks that compose the Sierra Nevada batholith (Faunt, 2009). At depth, the basement rocks are assumed to be relatively impermeable.

There are no significant faults mapped in the Tule Subbasin that would form a groundwater flow barrier or affect groundwater flow.

2.1.3. Lateral Basin Boundaries §354.14 (b)(2)

The lateral boundaries of the Tule Subbasin are defined in CDWR Bulletin 118 and include both natural and political boundaries. The eastern boundary of the Tule Subbasin is defined by the surface contact between crystalline rocks of the Sierra Nevada and surficial alluvial sediments that make up the groundwater basin (see Figure 2-4). The northern boundary is defined by the LTRID and Porterville Irrigation District (PID) boundaries. The western boundary is defined by the Tulare



County/Kings County boundary, except for a portion of the Tulare Lake Basin Water Storage District that extends east across the county boundary and is excluded from the subbasin. The southern boundary is defined by the Tulare County/Kern County boundary except for the portion of the Delano-Earlimart Irrigation District (DEID) that extends south of the county boundary and is included in the subbasin. The total area of the Tule Subbasin is approximately 744 square miles (475,895 acres).

2.1.4. Bottom of Basin §354.14 (b)(3)

§ 354.14. (b) (3) The definable bottom of the basin.

The physical bottom of the Tule Subbasin is defined by the interface between the Tertiary sedimentary deposits and the relatively impermeable granitic bedrock below them. This depth ranges from zero at the eastern margins of the subbasin where the continental deposits meet the granitic bedrock to approximately 5,000 feet below ground surface in the western portion of the subbasin (Planert and Williams, 1995).

The physical bottom of the subbasin is deeper than the bottom of the fresh water aquifer. The total dissolved solids (TDS) concentration of the groundwater generally increases with increasing depth such that below a certain level, the groundwater is not suitable for municipal, irrigation or other beneficial uses. Accordingly, a better measure of the bottom of the basin is the fresh water/brackish water interface, as defined in Page (1973) by an electrical conductivity of 3,000 micromhos per centimeter ($\mu\text{mhos/cm}$), which is approximately correlative to a total dissolved solids (TDS) concentration of 2,000 milligrams per liter (mg/L).

In the Tule Subbasin, the fresh water/brackish water interface varies across the subbasin but is generally 1,500 to 3,000 feet below land surface (Page, 1973; Planert and Williams, 1995). The deepest fresh water occurs in the western portion of the Tule Subbasin. Agricultural irrigation wells in the western Tule Subbasin are as deep as 1,500 feet and some agricultural wells west of the Tulare/Kings County boundary are as deep as 2,200 feet. The bottom of the effective groundwater basin, based on the fresh water/brackish water interface, is shown on Figures 2-5 and 2-6.



2.1.5. Surface Water Features §354.14 (d)(5)

§ 354.14. (d) (5) Surface water bodies that are significant to the management of the basin.

2.1.5.1. *Tulare Lake*

Although now largely a dry lake bed, prior to the mid-1800s Tulare Lake was the largest fresh water lake, by area, west of the Mississippi River. The original area of the lake was approximately 570 square miles and was fed from surface water discharges at the terminus of the Kern River, Tule River, Kaweah River, and Kings River. Beginning in the mid-1800s, surface water from the rivers feeding the lake was diverted for agricultural irrigation and municipal supply. By 1900, the lake was dry except for residual marshes and wetlands and occasional flooding. This condition continues to the present.

2.1.5.2. *Lake Success*

Lake Success is a manmade reservoir created by the construction of Success Dam that was completed in 1961 and serves as a flood control and water conservation project for the Tule River. Success dam and reservoir are managed by the United States Army Corps of Engineers (ACOE). Water storage in Lake Success is subject to the ACOE's flood control diagram and released as directed by the ACOE and downstream water rights holders as administered by the Tule River Association (TRA), in accordance with the Tule River Water Diversion Schedule and Storage Agreement (TRA, 1966).

2.1.5.3. *Tule River*

The Tule River is the largest natural drainage feature in the Tule Subbasin. From its headwaters in the Sierra Nevada Mountains, the Tule River flows first into Lake Success and then, through controlled releases at the dam, flows through the City of Porterville where it is diverted at various points before flowing into the LTRID. A significant diversion point is the Porter Slough, which flows to the north and semi-parallel to the main river channel and is used to convey surface water to various recharge facilities and canals. Downstream of Porterville, the Tule River ultimately discharges onto the Tulare Lakebed during periods of above-normal precipitation. Stream flow is measured via gages located below Success Dam, at Rockford Station downstream of Porterville, and at Turnbull Weir (see Figure 2-7). From water years 1986/87 to 2016/17, releases from Lake Success to the Tule River, quantified in TRA annual reports as the sum of Pioneer Water Company diversion and stream flow at the Below Success Dam gage, has ranged from 8,820 acre-ft in water year 2014/15 to 439,125 acre-ft in water year 1997/98 with an annual average during this time period of approximately 118,300 acre-ft.



Releases of water below Lake Success dam are diverted from the Tule River channel at various locations in accordance with TRA (1966). Diversion points along the river are located at the Porter Slough headgate, Campbell and Moreland Ditch Company, Vandalia Water District, Poplar Irrigation Company, Hubbs and Miner Ditch Company, and Woods-Central Ditch Company. The lower portion of the Tule River channel is also used as a conveyance mechanism to convey imported water from the Friant-Kern Canal to the PID and LTRID. Within the PID and LTRID, a combination of natural stream flow and imported water are further diverted into unlined canals for distribution to artificial recharge basins and farmers. Any residual stream flow left in the Tule River after diversions is measured at the Turnbull Weir, located at the west end of the LTRID (see Figure 2-7).

2.1.5.4. Deer Creek

Deer Creek is a natural drainage that originates in the Sierra Nevada Mountains, flowing in a westerly direction north of Terra Bella and into Pixley (see Figure 2-7). Although the Deer Creek channel extends past Pixley, discharges rarely reach the historical Tulare Lakebed. Stream flow in Deer Creek has been measured at the USGS gaging station at Fountain Springs from 1968 to present time. Average annual flow at this gage between water year 1986/87 and 2016/17 was approximately 17,800 acre-ft/yr with a low of approximately 2,000 acre-ft in water year 2014/15 and a high of approximately 88,000 acre-ft in water year 1997/98. Stream flow has also been measured at a second USGS gaging station on Deer Creek at Terra Bella although the period of record (1971 through 1987) is not as complete as the station at Fountain Springs. Friant-Kern Canal water is also diverted and monitored into Deer Creek and again measured at Trenton Weir before being delivered to riparian lands via unlined canals (see Figure 2-7). During wet years, water that reaches the terminus of Deer Creek is discharged into the Homeland Canal.

2.1.5.5. White River

The White River drains out of the Sierra Nevada Mountains east of the community of Richgrove in the southern portion of the Tule Subbasin (see Figure 2-7). Stream flow in the White River has been measured at the USGS gaging station near Ducor from 1972 to 2005. Data after 2005 has been interpolated. Average annual flow between water year 1986/87 and 2016/17 was approximately 5,800 acre-ft/yr with a low of approximately 250 acre-ft in water year 2014/15 and a high of approximately 37,000 acre-ft in 1997/98. The White River channel extends as far as State Highway 99 but does not reach the historical Tulare Lakebed.



2.1.5.6. Imported Water §354.14 (d)(6)

§ 354.14. (d) (6) The source and point of delivery for imported water supplies.

Most of the water imported into the Tule Subbasin is from the Central Valley Project (CVP) and delivered via the Friant-Kern Canal (see Figure 2-7). Angiola Water District also imports water from other various sources including the King’s River and State Water Project. The water is delivered to farmers and recharge basins via the Tule River and Deer Creek channels, unlined canals, and pipeline distribution systems of PID, LTRID, Terra Bella Irrigation District, Teapot Dome Water District, DEID, and Saucelito Irrigation District.

Distribution of stream flow diversions and imported water occur via a system of manmade canals and pipeline distribution systems that extend throughout the Tule Subbasin. The largest of these is the Friant-Kern Canal, which supplies imported water through the Federal Central Valley Project (CVP). The Friant-Kern Canal is concrete lined and trends approximately north-south through the eastern part of the Tule Subbasin (see Figure 2-7). Numerous other canals and pipeline distribution systems are located within the Tule Subbasin to convey surface water from the Friant-Kern Canal, Tule River and Deer Creek to various recharge facilities and agricultural areas. The canals are unlined and occur primarily in the LTRID, Pixley Irrigation District, PID, Alpaugh Irrigation District, and Atwell Island Water District. The Angiola Water District receives deliveries from the Tule River and Kings River via the Homeland Canal and distributes that water via an internal system of unlined canals.

Many of the irrigation districts and water districts in the Tule Subbasin that receive imported water from the Friant-Kern Canal distribute the water exclusively via pipeline distribution systems. These districts include the Delano-Earlimart Irrigation District, Kern-Tulare Water District, Terra Bella Irrigation District, Saucelito Irrigation District, and Tea Pot Dome Water District.

2.1.6. Areas of Groundwater Recharge and Discharge §354.14 (d)(4)

§ 354.14. (d) (4) Delineation of existing recharge areas that substantially contribute to the replenishment of the basin, potential recharge areas, and discharge areas, including significant active springs, seeps, and wetlands within or adjacent to the basin.

Groundwater recharge in the Tule Subbasin occurs within stream channels, unlined canals, in managed recharge basins, and in areas of the subbasin with irrigated agriculture. Favorable areas for deep percolation of surface water are characterized by relatively permeable surface soils (see Figure 2-8), and lack of subsurface impediments to groundwater recharge.

The University of California at Davis has developed a Soil Agricultural Groundwater Banking Index (SAGBI) that identifies favorable areas of recharge based on deep percolation potential, root



zone residence time, topography, chemical limitations, and soil surface condition. The SAGBI zones for the Tule Subbasin are shown on Figure 2-9. In general, the most favorable areas for recharge are within the stream channels of the Tule River, Deer Creek and White River, in the Porterville area, and in a north-south zone in the west-central portion of the subbasin. Areas that are not favorable for deep percolation of surface water and recharge of groundwater are in the furthest east portion of the subbasin along the base of the Sierra Nevada Mountains and in the furthest west portion of the subbasin coincident with Tulare Lake lacustrine deposits. It is noted that the SAGBI zones shown on Figure 2-9 are limited to the surface deposits and any areas to be considered for additional recharge basins should be further investigated with boreholes and recharge tests to confirm the recharge potential of the location.

There are no areas of groundwater discharging at the land surface in the Tule Subbasin due to the depth of the groundwater. The primary source of groundwater discharge is pumping from wells (see Section 2.3.1.1.4), which occurs across most of the subbasin.

2.1.7. Principal Aquifers and Aquitards §354.14 (b)(4)

§ 354.14. (b) (4) Principal aquifers and aquitards, including the following information:

- (A) Formation names, if defined.
- (B) Physical properties of aquifers and aquitards, including the vertical and lateral extent, hydraulic conductivity, and storativity, which may be based on existing technical studies or other best available information.
- (C) Structural properties of the basin that restrict groundwater flow within the principal aquifers, including information regarding stratigraphic changes, truncation of units, or other features.
- (D) General water quality of the principal aquifers, which may be based on information derived from existing technical studies or regulatory programs.
- (E) Identification of the primary use or uses of each aquifer, such as domestic, irrigation, or municipal water supply.

2.1.7.1 Aquifer Formations §354.14 (b)(4)(A)

In general, there are five general aquifer/aquitard units in the subsurface beneath the Tule Subbasin (see Figures 2-5 and 2-6):

1. Upper Aquifer
2. The Corcoran Clay Confining Unit
3. Lower Aquifer
4. Pliocene Marine Deposits (generally considered an aquitard)
5. Santa Margarita Formation and Olcese Formation of the Southeastern Subbasin



The upper aquifer occurs across the entire Tule Subbasin area. This aquifer is generally unconfined to semi-confined. The upper aquifer occurs in the upper 450 ft of sediments on the western side of the subbasin and shallows to the east to less than approximately 100 ft of sediments in the Porterville area. In the southeastern portion of the basin, the upper aquifer is generally considered unsaturated although there may be local areas of groundwater.

The Corcoran Clay confining unit occurs beneath the upper aquifer in the western half of the Tule Subbasin (see Figures 2-4, 2-5 and 2-6). This unit consists primarily of blue or green diatomaceous clay although in places it is interbedded with sandy sediments. The Corcoran Clay is thickest in the western part of the subbasin and thins to the east, pinching out approximately two to three miles east of State Highway 99 (see Figure 2-4). It is noted that, in places, the Corcoran Clay, as formally defined in Frink and Kues (1954) and later Davis et al. (1959), is bounded above and below by fine-grained clay not specifically associated with the Corcoran Clay. As such, the thickness of the Corcoran Clay unit, as shown on Figures 2-5 and 2-6 has been defined to include these adjacent clays.

The lower aquifer extends across the entire western portion of the Tule Subbasin and beneath the northeastern portion of the subbasin. The total depth of this aquifer ranges from approximately 400 bgs in the eastern Tule Subbasin to more than 2,000 feet in the western portion of the subbasin. This aquifer is confined beneath the Corcoran Clay where this confining layer exists, and beneath other clay lenses in other parts of the subbasin. The lower aquifer system is conceptualized to be semi-confined in the northeastern portion of the subbasin east of the Corcoran Clay.

In the southeastern portion of the Tule Subbasin, the lower aquifer is separated from the underlying Santa Margarita Formation aquifer by a relatively thick (500 to 1,600 feet) layer of Pliocene marine deposits. These deposits consist primarily of siltstone with minor interbedded sandstone and are conceptualized as a confining unit that separates the deep alluvial aquifer from the Santa Margarita Formation aquifer. Some wells in the southeastern portion of the Tule Subbasin are perforated partially within this unit but the contribution of groundwater from the formation is low (Lofgren and Klausung, 1969).

The Santa Margarita Formation and Olcese Formation underlie the Pliocene marine deposits and forms a localized aquifer in the southeastern portion of the Tule Subbasin. This aquifer is a primary source of groundwater for agricultural irrigation in the southeastern portion of the subbasin. The aquifer is relatively permeable and well yields greater than 1,500 gallons per minute have been reported (Kern-Tulare Water District, 2018). Until additional data are collected, this localized aquifer is conceptualized as hydrologically separate from the deep aquifer in the rest of the subbasin.



2.1.7.2 *Aquifer Physical Properties §354.14 (b)(4)(B)*

Where saturated in the subsurface, the permeable sand and gravel layers form the principal aquifers in the Tule Subbasin and adjacent areas to the north, south and west. Individual aquifer layers consist of lenticular sand and gravel deposits of varying thickness and lateral extent. The aquifer layers are interbedded with low permeability silt and clay lenses. In general, shallow saturated sediments in the Tule Subbasin are unconfined to semi-confined. The aquifer beneath the Corcoran Clay unit in the western portion of the basin is confined. The hydrologic characteristics of the deeper aquifer system in the western portion of the subbasin are unknown but are expected to change with depth.

The ability of aquifer sediments to transmit and store water is described in terms of the aquifer parameters transmissivity, hydraulic conductivity, and storativity. The most reliable estimates of these parameters are obtained from long-term (e.g. 24-hr or more constant rate) controlled pumping tests in wells. In the absence of this type of test, estimates can be obtained through short-term pumping tests and/or assignment of literature values based on the soil types observed in driller's logs. Long-term pumping test data was obtained from KDSA and DEID for wells located in the southern part of the subbasin. Short-term pumping test data was obtained from driller's logs, KDSA for Angiola Water District and City of Porterville wells, and KTWD for selected wells. Where pumping test data were not available, aquifer parameters were assigned from literature values in published in Faunt (2009).

Transmissivity is a measure of the ability of groundwater to flow within an aquifer and is defined as the rate of groundwater flow through a unit width of aquifer under a unit hydraulic gradient (Fetter, 1994). Transmissivity was estimated from short-term pumping test data based on Theis et al., 1963 and the following relationship:

$$T = \frac{S_c \times 2,000}{E}$$

Where:

T	=	Transmissivity (gpd/ft);
S _c	=	Specific Capacity (gpm/ft);
E	=	Well Efficiency (assumed to be 0.7)

Transmissivity values at individual wells were converted into hydraulic conductivity (i.e. aquifer permeability) by dividing by the aquifer thickness (in this case the perforation interval of the well). Horizontal hydraulic conductivity values for the upper aquifer are shown on Figure 2-10 and range from less than 5 ft/day to greater than 160 ft/day, the higher values indicating more permeable



sediments. Hydraulic conductivity values for the lower aquifer are shown on Figure 2-11 and range from less than 5 ft/day to greater than 80 ft/day.

Storage properties of the upper aquifer are expressed in terms of specific yield since the majority of this aquifer is conceptualized as unconfined. Specific yield is the ratio of the volume of water sediment will yield by gravity drainage to the volume of the sediment. Specific yield values for the upper aquifer were assigned based on a USGS texture analysis published in Faunt (2009). Textural descriptions describe the percent coarse-grained sediment as inferred from drillers' logs from boreholes or wells drilled within or immediately outside the Tule Subbasin. Higher percent coarse-grained sediment descriptions are correlated with higher specific yield (see Figure 2-12). As shown, higher percent coarse-grained sediments are observed in the upper aquifer through most of the Tule Subbasin with the exception of the southwestern portion. Values of specific yield for the upper aquifer range from 0.05 to greater than 0.2.

The lower aquifer in the Tule Subbasin is confined to semi-confined and, as such, storage properties for this aquifer are expressed in terms of storativity. Storativity is a measure of the volume of water an aquifer can release from, or take into, storage per unit of aquifer surface area per unit change in hydraulic head. Storativity is derived from long-term pumping tests where pumping interference is measured in a monitoring well located a known distance from the pumping well. As no pumping interference data are available for the Tule Subbasin, storativity values for the lower alluvial aquifer were originally based on values published in Faunt (2009) and modified during calibration of the numerical model for the Tule Subbasin. Values for storativity in the deep aquifer range from 0.00015 to 0.001 (see Figure 2-13). These values indicate confined to semi-confined aquifer conditions.

2.1.7.3 Geologic Structures that Affect Groundwater Flow §354.14 (b)(4)(C)

There are no significant faults mapped in the Tule Subbasin that affect groundwater flow.

The Corcoran Clay unit is the most significant geologic feature that affects vertical groundwater flow in the Tule Subbasin. In general, the aquifer system above the clay unit is unconfined to semi-confined and the aquifer system below it is confined. The hydraulic head in the upper aquifer is higher than that of the lower aquifer, such that there is vertical downward hydraulic gradient between the two. Despite the low vertical hydraulic conductivity of the Corcoran Clay, the area for downward flow is large (hundreds of thousands of acres), and the vertical gradients are relatively steep (commonly 20 to 40 feet per 100 feet). This allows for significant downward flow of water through the clay on a regional basis. In addition, many wells in the subbasin are perforated across both the upper and lower aquifers (composite wells) creating communication between the two. As such, these wells facilitate some recharge of the lower aquifer from the upper aquifer. East of the Corcoran Clay, other localized confining beds are present that separate the upper aquifer from the lower aquifer.



2.1.7.4 Aquifer Water Quality §354.14 (b)(4)(D)

Groundwater quality in the Tule Subbasin varies across the subbasin and with depth in the aquifer system. Overall, the native groundwater quality is generally very good, with historical EC measurements generally less than approximately 600 $\mu\text{mohs/cm}$ (Tule Basin Water Quality Coalition, 2017) (see Figure 2-14). Groundwater quality issues in the subbasin include both regional non-point sources of groundwater quality degradation and point-source contaminant issues.

On a regional level, non-point source constituents of concern for groundwater quality include nitrate, pesticides, 1,2-dibromo-3-chloropropane (DBCP), and 1,2,3, trichloropropane (TCP) in the upper aquifer and arsenic, manganese, and, hydrogen sulfide for the lower aquifer. In the western part of the subbasin, color and methane gas are also non-point constituents of concern.

Nitrate is the primary non-point constituent of concern (Tule Basin Water Quality Coalition, 2017). Historical nitrate concentrations (reported as nitrate) in the subbasin range from non-detect to greater than 300 mg/L (see Figure 2-15). The highest nitrate concentrations have been detected in shallow groundwater in the northwest portion of the subbasin and are likely correlated with overlying land use.

Wells from which elevated EC values have been detected above the subbasin average occur in shallow groundwater in the northwest and southwest portions of the subbasin (see Figure 2-14). High EC values measured in groundwater in the northwest part of the subbasin are likely associated with overlying land use. High EC has also been detected in shallow and locally perched groundwater in the southwestern part of the subbasin. This area of the subbasin is on the historical Tulare Lakebed where the Regional Water Quality Control Board – Central Valley Region and California State Water Resources Control Board (SWRCB) has removed the municipal and agricultural beneficial use designation (SWRCB, 2017).

For point-source contaminants, there are 26 active cleanup sites in the Tule Subbasin identified on the California Geotracker website (see Figure 2-16; Table 2-1). Twelve of the point source contamination sites are associated with leaking underground storage tanks (LUSTs) for which the primary contaminant is petroleum hydrocarbons (gasoline, diesel and kerosene). There are 14 Regional Water Quality Control Board Cleanup Program or Department of Toxic Substance Control (DTSC) sites within the subbasin (see Figure 2-16). Contaminants associated with these sites include metals, volatile organic compounds (VOCs), pesticides, herbicides, cyanide, and polyaromatic hydrocarbons (PAHs). Groundwater contaminant plumes associated with these sites are highly localized.



2.1.7.5 Aquifer Primary Uses §354.14 (b)(4)(E)

The predominant beneficial use of groundwater in the Tule Subbasin is agricultural irrigation. Other beneficial uses include municipal water supply, private domestic water supply, and livestock washing and watering.

2.1.8. Uncertainty in the Hydrogeologic Conceptual Model §354.14 (b)(5)

§ 354.14. (b) (5) Identification of data gaps and uncertainty within the hydrogeologic conceptual model

The primary sources of uncertainty in the hydrogeologic conceptual model include:

- Knowledge of the hydraulic interaction between the shallow and deep aquifer
- Lack of aquifer-specific groundwater levels with adequate spatial distribution to enable preparation of representative groundwater level maps of each aquifer in parts of the subbasin
- Characteristics of the Santa Margarita Formation aquifer
- Groundwater underflow into the alluvial aquifer system from the Sierra Nevada mountain block
- Aquifer characteristics of hydraulic conductivity, transmissivity and storativity
- Agricultural groundwater pumping
- Well construction and pumping distribution between the shallow and deep aquifers
- Canal seepage
- Travel time for recharge from the land surface through the unsaturated zone to the groundwater

Uncertainty in the hydrogeologic conceptual model is being addressed through a sensitivity and uncertainty analysis of the numerical model results from the Tule Subbasin model (TH&Co, 2020) (see Section 2.3.2.7).

2.2 Groundwater Conditions §354.16

§ 354.16. Groundwater Conditions

Each Plan shall provide a description of current and historical groundwater conditions in the basin, including data from January 1, 2015, to current conditions, based on the best available information that includes the following:



2.2.1 Groundwater Occurrence and Flow §354.16 (a)

§ 354.16. (a) Groundwater elevation data demonstrating flow directions, lateral and vertical gradients, and regional pumping patterns, including:

- (1) Groundwater elevation contour maps depicting the groundwater table or potentiometric surface associated with the current seasonal high and seasonal low for each principal aquifer within the basin.
- (2) Hydrographs depicting long-term groundwater elevations, historical highs and lows, and hydraulic gradients between principal aquifers.

In general, groundwater in the Tule Subbasin flows from areas of natural recharge along major streams at the base of the Sierra Nevada Mountains on the eastern boundary towards a groundwater pumping depression in the west-central portion of the subbasin (see Figures 2-17 and 2-18). The pumping depression has reversed the natural groundwater flow direction in the western portion of the subbasin, inducing subsurface inflow along the southern and western boundaries.

In the upper aquifer, the pumping depression is most pronounced between the Tule River and Deer Creek west of Highway 99 and east of Highway 43. The pumping depression has persisted in this area since at least 1987, even during periods of above-normal precipitation when groundwater levels temporarily recovered. Recharge from the Tule River results in a groundwater flow divide in the upper aquifer along the northern boundary of the Tule Subbasin. As such, upper aquifer groundwater on the north side of the river flows to the north and out of the subbasin. Groundwater flow patterns in the upper aquifer have generally not changed significantly since 1990.

In the lower aquifer, groundwater flows to the southwest toward a pumping depression in the western portion of the subbasin (see Figure 2-19). This pumping depression extends from west of Corcoran in the northwest to the Alpaugh area in the southwestern Tule Subbasin west of Highway 43. There is inadequate data to prepare groundwater contour maps specific to the lower aquifer for spring and fall of 2017. The groundwater contour map provided on Figure 2-19 for 2010 is the most recent year for which data were available to prepare a contour map.

Groundwater level changes over time can be observed from hydrographs developed from wells monitored in the Tule Subbasin. Despite a relatively wet hydrologic period between 1995 and 1999 and periodic wet years (2005 and 2011), groundwater levels in upper aquifer wells show a persistent downward trend between approximately 1987 and 2017 (see Figure 2-20). Groundwater level trends in wells perforated exclusively in the lower aquifer vary depending on location in the subbasin. In the northwestern part of the subbasin, lower aquifer groundwater levels have shown a persistent downward trend from 1987 to 2017. In the southern part of the subbasin, groundwater levels were relatively stable between 1987 and 2007 but began declining after 2007 (see Figure 2-21).

Comparisons of hydrographs from wells perforated in the upper aquifer with wells perforated predominantly in the lower aquifer and in close proximity show that groundwater levels in the



upper aquifer are higher than groundwater levels in the lower aquifer (see Figure 2-22). This indicates a downward hydraulic gradient and indicates that the upper aquifer is recharging the lower aquifer of the Tule Subbasin. This is corroborated by depth-specific isolated aquifer zone testing conducted by the City of Porterville in three wells in which the equilibrated groundwater level (i.e. hydraulic head) in the deepest isolated zones, which also correspond to the lower aquifer, were as much as 180 ft lower than the groundwater level in the shallowest isolated zones (Schmidt, 2009). Faunt (2009) has suggested that the recharge of the lower aquifer via wells that are perforated across both aquifers has increased with the number of deep wells constructed in the San Joaquin Valley.

2.2.2 Groundwater Storage §354.16 (b)

§ 354.16. (b) A graph depicting estimates of the change in groundwater in storage, based on data, demonstrating the annual and cumulative change in the volume of groundwater in storage between seasonal high groundwater conditions, including the annual groundwater use and water year type.

Changes in groundwater storage within the Tule Subbasin have been estimated through analysis of the water budget for the subbasin. Annual change in groundwater storage in the subbasin between 1986/87 and 2016/17 is shown in Table 2-3 and is graphically presented on Figure 2-23. Comparison of the groundwater inflow elements of the water budget with the outflow elements shows a cumulative change in groundwater storage over the 31-year period between 1986/87 and 2016/17 of approximately -4,948,000 acre-ft. The average annual change in storage resulting from the groundwater budget is approximately -160,000 acre-ft/yr over this time period.

2.2.3 Seawater Intrusion §354.16 (c)

§ 354.16. (c) Seawater intrusion conditions in the basin, including maps and cross-sections of the seawater intrusion front for each principal aquifer.

Seawater intrusion cannot occur in the Tule Subbasin due to its location with respect to the Pacific Ocean. The Tule Subbasin is approximately 110 miles inland of the Pacific Ocean (see Figure 2-1) and is separated from the ocean by approximately 90 miles of sedimentary rocks that make up the Coast Ranges. These sedimentary rocks effectively separate the Pacific Ocean hydraulically from the aquifer system in the San Joaquin Valley. Further, the Coast Ranges are dissected by multiple northwest trending faults, the largest of which is the San Andreas Fault. These faults form groundwater flow barriers, which further act to separate the San Joaquin Valley aquifers from the Pacific Ocean. Accordingly, groundwater pumping in the Tule Subbasin cannot induce seawater intrusion.



2.2.4 Groundwater Quality Issues §354.16 (d)

§ 354.16. (d) Groundwater quality issues that may affect the supply and beneficial uses of groundwater, including a description and map of the location of known groundwater contamination sites and plumes.

Groundwater quality issues have been designated based on agricultural and drinking water beneficial uses of groundwater in the Tule Subbasin. The nine constituents of concern for drinking water beneficial uses are arsenic, nitrate, hexavalent chromium, dibromochloropropane (DBCP), 1,2,3-Trichloropropane (TCP), tetrachloroethene (PCE), chloride, total dissolved solids (TDS), and perchlorate Concentrations. Concentrations of these constituents of concern based on 2017 to 2022 available data are shown on Figures 2-14a through 2-14i. The three constituents of concern for agricultural uses are chloride, sodium, and TDS. The available data from 2017 to 2022 for these constituents are shown on Figures 2-15a, 2-15b, and 2-15c.

Existing groundwater quality monitoring programs within the Tule Subbasin are summarized in the following table:



Programs or Data Portals	Tule Subbasin Agency Coordinating with GSAs	Parameters	Monitoring Frequency	Program Objectives
AB-3030 and SB-1938 Groundwater Management Plans	Tule Subbasin GSAs, requirements incorporated into GSP Annual Reports	<ul style="list-style-type: none"> Water levels are typically monitored annually. Ag Suitability analysis (limited suite of general minerals) monitoring frequency between annual to once every 3 years. 	Semiannual to Annual	-
California SDWIS	Varies Public Water Systems	Database for all public water system wells and historical sample results. Data available includes all Title 22 regulated constituents.	<ul style="list-style-type: none"> Title 22 General Minerals and Metals every 3 years. Nitrate as N annually, if ≥ 5 ppm, sampled quarterly VOCs and SOCs sampled every 3 years. Uranium sampling depends on historical results but varies between 1 sample every 3 (when ≥ 10 pCi/L), 6 (when < 10 pCi/L) or 9 (when no historical detection) years. 	Demonstrate compliance with Drinking Water Standards through monitoring and reporting water quality data.
CV-SALTS	Tule Basin Management Zone, Tule Basin Water Foundation	Sampling parameters required through Waste Discharge Requirements (WDR): typically include monthly sodium, chloride, electrical conductivity, nitrogen species (N, NO ₂ , NO ₃ , NH ₃), pH and other constituents of concern identified in the Report of Waste Discharge. A limited suite of general minerals is required quarterly from the source and annually from the wastewater.	Most constituents sampled monthly, quarterly general minerals from source water and annual general minerals from waste discharge.	To monitor degradation potential from wastewaters discharged to land application areas and provide interim replacement water when MCL for nitrate as N is exceeded while developing long term solutions for safe drinking water.
Department of Pesticide Regulation	County of Tulare	Pesticides	Annual	DPR samples groundwater to determine: <ol style="list-style-type: none"> (1) whether pesticides with the potential to pollute groundwater are present, (2) the extent and source of pesticide contamination, and (3) the effectiveness of regulatory mitigation measures.
GAMA (Collaboration with SWQCB, RWQCB, DWR, DPR, NWIS, LLNL)		<ul style="list-style-type: none"> Constituents sampled vary by the Program Objectives. Typically, USGS is the technical lead in conducting the studies and reporting data. 	Varies	<ul style="list-style-type: none"> Improve statewide comprehensive groundwater monitoring. Increase the availability of groundwater quality and contamination information to the public.
Geotracker and Envirostor Databases		Many contaminants of concern, organic and inorganic.	Depends on program. Monthly, Semiannually, Annually, etc.	Records database for cleanup program sites, permitted waste dischargers
ILRP	Tule Basin Water Quality Coalition	<ul style="list-style-type: none"> Annually: static water level, temperature, pH, electrical conductivity, nitrate as nitrogen, and dissolved oxygen. Once every five years: general minerals collection 	Annual and Every 5 years	Monitor impacts of agricultural and fertilizer
USGS California Water Science Center		Conducted multiple groundwater quality studies of the Tule Subbasin.	Reports, factsheet, and data publications range from 1994 through 2017.	Special studies related to groundwater quality that provide comprehensive studies to characterize the basin.



There are 26 active cleanup sites in the Tule Subbasin identified on the California Geotracker website (see Figure 2-16; Table 2-1). Twelve of the point source contamination sites are associated with LUSTs for which the primary contaminant is petroleum hydrocarbons (gasoline, diesel and kerosene). There are 14 Regional Water Quality Control Board Cleanup Program or Department of Toxic Substance Control (DTSC) sites within the subbasin (see Figure 2-16). Contaminants associated with these sites include metals, VOCs, pesticides, herbicides, cyanide, and PAHs.

2.2.5 Land Subsidence §354.16 (e)

§ 354.16. (e) The extent, cumulative total, and annual rate of land subsidence, including maps depicting total subsidence, utilizing data available from the Department, as specified in Section 353.2, or the best available information.

Land surface subsidence in the Tule Subbasin as a result of lowering the groundwater level from groundwater production has been well documented (Ireland et al., 1984; Faunt, 2009; Luhdorff and Scalmanini, 2014). Prior to 1970, as much as 12 ft of land surface subsidence was documented for the area immediately south of Pixley (Ireland et al., 1984). As groundwater levels rose in the area throughout the 1970s and early 1980s, land subsidence was largely arrested. During this time, monitoring for land subsidence that had previously been conducted along the portion of the Friant-Kern Canal that is within the Tule Subbasin was discontinued.

From the late 1980s into the 2000s, it is suspected that land subsidence in the Tule Subbasin was reactivated as groundwater levels declined. Groundwater flow model simulations of land subsidence in the Central Valley by Faunt et al. (2009), which were calibrated to historical land subsidence that occurred in the 1960s, simulated an additional two to four feet of land subsidence between 1986 and 2003.

The reactivation of land subsidence was confirmed in the late 2000s based on data from Interferometric Synthetic Aperture Radar (InSAR) satellites and one Global Positioning System (GPS) station located in Porterville, California. InSAR data showed as much as four feet of additional land subsidence occurring in the northwestern portion of the Tule Subbasin between 2007 and 2011 (see Figure 2-24) (Luhdorff and Scalmanini, 2014). Approximately 0.4 ft of land subsidence occurred in the Porterville area between 2007 and 2011. From 2015 through 2018, land subsidence in the Tule Subbasin, as observed from InSAR data, continued with as much as 2.75 ft of additional land subsidence in the northwest portion of the subbasin and as much as 0.75 ft of additional land subsidence at the Porterville GPS station (see Figure 2-25). Based on benchmarks located along the Friant-Kern Canal and monitored by the Friant Water Authority, cumulative land subsidence along the canal between 1959 and 2017 has ranged from approximately 1.7 ft in the Porterville area to 9 feet in the vicinity of Deer Creek (see Figure 2-24).

For the time period between 1987 and 2018, cumulative subsidence across the Tule Subbasin was estimated (in feet) based on model simulation results of land subsidence using a groundwater flow



model equipped with a subsidence simulation package calibrated to observed land subsidence from InSAR and GPS data. The highest cumulative land subsidence for the time period was estimated for the northwestern portion of the subbasin where approximately 12 feet was simulated. The lowest rates of land subsidence were observed in the southeast portion of the subbasin between Delano and Richgrove where less than one foot of cumulative land subsidence was simulated.

The rate of land subsidence in the Tule Subbasin varies both spatially, according to the geology of the subsurface sediments, and temporally with changes in groundwater levels. The average rate of change in land surface elevation between 1987 and 2018 for the area of maximum subsidence was estimated to be approximately 12 feet over the 32-year period for a rate of 0.4 ft/yr. At the Porterville GPS station, the annual rate of subsidence between 2006 and 2013 was approximately 0.09 ft/yr but increased to approximately 0.29 ft/yr between 2013 and 2019 (see Figure 2-25).

2.2.6 Interconnected Surface Water Systems §354.16 (f)

§ 354.16. (f) Identification of interconnected surface water systems within the basin and an estimate of the quantity and timing of depletions of those systems, utilizing data available from the Department, as specified in Section 353.2, or the best available information.

Interconnected surface water is surface water that is hydraulically connected at any point by a continuous saturated zone to the underlying aquifer and the overlying surface water is not completely depleted. As of January 2015, there are no areas within the Tule Subbasin where the depth to groundwater is within 25 ft of the land surface (see Figure 2-26). Based on the depth to groundwater, it is assumed that an unsaturated zone exists between surface water features and the aquifer system during average and dry periods. It is noted that there may be periods of time when the groundwater level temporarily rises to within 25 feet of the land surface in only a few relatively small areas of the Tule Subbasin, namely along the Tule River in and upstream of Porterville, and in the upper reaches of Deer Creek and White River. However, this condition, if it occurs, would be temporary and is not the normal hydrologic relationship between surface water and groundwater in these areas.

2.2.7 Groundwater Dependent Ecosystems §354.16 (g)

§ 354.16. (g) Identification of groundwater dependent ecosystems within the basin, utilizing data available from the Department, as specified in Section 353.2, or the best available information.

Groundwater dependent ecosystems require shallow groundwater or groundwater that discharges at the land surface. Throughout the Tule Subbasin, the depth to groundwater is well below the level required to support riparian vegetation (vegetation that draws water directly from groundwater) or near surface ecosystems, except some areas along the Tule River east of Porterville. Based on the CDWR Groundwater Dependent Ecosystems database



(www.groundwaterresourcehub.org), the deepest root zones for groundwater dependent plants in the Tule Subbasin are for Valley Oak, which can reach a depth of approximately 25 feet. Figure 2-26 is a depth to groundwater map based on groundwater levels in January 2015. As shown, there were no areas of the subbasin where the groundwater was within 25 feet of the land surface at that time. It is noted that there may be periods of time when the groundwater level is within 25 feet of the land surface in some areas of the subbasin. The areas most likely to support groundwater dependent ecosystems are along the Tule River in and upstream of Porterville, and in the upper reaches of Deer Creek and White River.

2.3 Water Budget §354.18

§ 354.18. Water Budget

(a) Each Plan shall include a water budget for the basin that provides an accounting and assessment of the total annual volume of groundwater and surface water entering and leaving the basin, including historical, current and projected water budget conditions, and the change in the volume of water stored. Water budget information shall be reported in tabular and graphical form.

2.3.1. Surface Water Budget

The surface water budget for the Tule Subbasin was developed for the 31-year period from 1986/87 to 2016/17 (see Table 2-2a for Inflow Terms and Table 2-2b for Outflow Terms). Inflow terms for the surface water budget include precipitation, stream inflow, imported water, and discharge to the land surface from wells. Outflow terms include infiltration of precipitation, evapotranspiration of precipitation from areas of native vegetation and crops, stream infiltration, canal loss, recharge in basins, return flow, and consumptive use.

Ideally, the total surface water inflow to the subbasin would equal the total surface water outflow, indicating a complete and accurate accounting of water at the surface. In reality, there is uncertainty in many of the surface water budget terms for the Tule Subbasin that does not allow for a perfect surface water accounting. These include estimates for agricultural groundwater production, crop consumptive use, precipitation recharge, surface water outflow to Homeland Canal from Deer Creek, and others. For the Tule Subbasin surface water budget, the percent difference between the average annual surface water inflow (1,477,000 acre-ft; Table 2-2a) and average annual outflow (1,474,000 acre-ft; Table 2-2b) is approximately 0.2 percent. This represents a very good match between surface water inflows and outflows and indicates that the water budget is a good representation of actual conditions. As additional data become available, it is anticipated that the surface water budget will become more accurate with time.

It is noted that many of the surface water outflow terms are also groundwater inflow (i.e. groundwater recharge) terms. Of the surface water outflow terms that become groundwater recharge, many are associated with water diverted in accordance with pre-existing water rights or



purchased imported water. Sources of surface water outflow that become groundwater recharge and are associated with existing rights and/or imported water deliveries are excluded from the Sustainable Yield estimate and are indicated with magenta-colored columns in Table 2-2b. Surface water losses that become groundwater recharge and are used to estimate Sustainable Yield are indicated with blue-colored columns in Table 2-2b. Surface water losses that do not become groundwater recharge, such as through evapotranspiration, crop consumptive use, or surface water outflow are indicated with yellow-colored columns in Table 2-2b (page 2).

Details of the individual surface water budget terms are provided in the following sections.

2.3.1.1 Surface Water Inflow §354.18 (b)(1)

§ 354.18. (b) The water budget shall quantify the following, either through direct measurements or estimates based on data:

- (1) Total surface water entering and leaving a basin by water source type.

2.3.1.1.1. Precipitation

The annual volume of water entering the Tule Subbasin as precipitation was estimated for the surface water budget based on the long-term average annual isohyetal map shown on Figure 2-27 and the annual precipitation data reported for the Porterville precipitation station. As annual precipitation values are not available throughout the entire Tule Subbasin, it was assumed that the relative precipitation distribution for each year was the same as that shown on the isohyetal map. The magnitude of annual precipitation within each isohyetal zone was varied from year to year based on the ratio of annual precipitation at the Porterville Station (see Figure 2-28) to annual average precipitation at the Porterville isohyetal zone multiplied by the isohyetal zone average annual precipitation. Using this method, total annual precipitation in the Tule Subbasin between water years 1986/87 and 2016/17 ranged from approximately 99,000 to 728,000 acre-ft/yr with an average of 306,000 acre-ft/yr (see Column A of Table 2-2a).

2.3.1.1.2. Stream Inflow

Surface water inflow to the Tule Subbasin occurs primarily via three native streams: Tule River, Deer Creek, and the White River (see Columns B through D of Table 2-2a). Flow in the Tule River is controlled through releases from Lake Success, which are documented in TRA annual reports. For water years 1986/87 to 2016/17, annual surface water inflow to the Tule Subbasin via the Tule River, measured as releases from Lake Success, ranged from 8,820 to 439,125 acre-ft/yr with an average of 118,300 acre-ft/yr. The long-term 114-year average (1904 to 2017) inflow to Lake Success via the Tule River channels is 139,187 acre-ft/year.



Annual inflow from Deer Creek is measured at Fountain Springs by the USGS and has varied from approximately 2,000 to 88,000 acre-ft/yr with an average of 17,800 acre-ft/yr over water years 1986/87 to 2016/17. The long-term average inflow via Deer Creek for the period of record from 1920 to 2017 is 22,035 acre-ft/year. It is noted that although the Fountain Springs gage is located approximately five miles upstream of the Tule Subbasin, the creek flows over granitic bedrock between the gage and the alluvial basin boundary and losses along this reach are assumed to be limited to evapotranspiration.

Surface water inflow from the White River is based on USGS stream gage data from the White River station near Ducor. The measured data from this station is only available from 1971 to 2005. In order to estimate annual streamflow from 1986/87 to 2016/17, it was assumed that the magnitude of flow in the White River is proportional to the magnitude of flow in Deer Creek. TH&Co plotted monthly White River streamflow against monthly Deer Creek streamflow for the period 1971 to 2005. A linear regression through the data resulted in a correlation coefficient of 0.91, suggesting that the relationship is applicable (see Figure 2-29). White River streamflow between 2006 and 2017 was based on the linear interpolation of measured data. Based on the measured and interpolated data, annual inflows from the White River ranged from approximately 250 to 37,000 acre-ft/yr and averaged 5,800 acre-ft/yr from water years 1986/87 to 2016/17.

2.3.1.1.3. Imported Water

Imported water is delivered to eleven water agencies within the Tule Subbasin from the Friant-Kern Canal (see Columns E through O of Table 2-2a). Data from PID, Saucelito Irrigation District, Tea Pot Dome Water District, Alpaugh Irrigation District, Atwell Island Irrigation District, and Terra Bella Irrigation District was obtained from USBR Central Valley Operation Annual Reports. Imported water data for the other agencies was provided by the respective agencies. Based on these data, an average of 345,600 acre-ft/yr was imported into the Tule Subbasin for the period from 1986/87 to 2016/17.

2.3.1.1.4. Discharge to Crops from Wells

Water applied to crops from wells is assumed to be the total applied water minus surface water deliveries from imported water and diverted streamflow (see Figure 2-30). The total crop demand was estimated based on consumptive use estimates and an assumed irrigation efficiency of 79 percent. The estimated average annual discharge to crops from wells for water years 1986/87 to 2016/17 was approximately 664,000 acre-ft/yr (see Column P of Table 2-2a).

2.3.1.1.5. Municipal Deliveries from Wells

Groundwater pumping for municipal supply is conducted by the City of Porterville and small municipalities for the local communities in the Tule Subbasin. From water years 1986/87 to



2016/17, municipal pumping from wells was estimated to average approximately 20,000 acre-ft/yr (see Column Q of Table 2-2a).

It is noted that there are some households in the rural portions of the Tule Subbasin that rely on private wells to meet their domestic water supply needs. However, given the low population density of these areas, the volume of pumping from private domestic wells is considered negligible compared to the other pumping sources.

2.3.1.2 Surface Water Outflow

2.3.1.2.1 Areal Recharge from Precipitation

Areal recharge from precipitation falling on the valley floor in the Tule Subbasin was estimated based on Williamson et al., (1989). As part of a regional hydrogeological study of the California Central Valley, Williamson et al., (1989) developed a monthly soil-moisture budget for the Sacramento Valley and San Joaquin Valley areas. The soil moisture budget was based on precipitation records for the 50-yr period from 1922 to 1971. The analysis considered potential evapotranspiration, assumed plant root depth, soil moisture-holding capacity, and precipitation. Monthly precipitation that exceeded monthly potential evapotranspiration and soil-moisture storage was computed as net infiltration to the groundwater system. The results were simplified with a linear regression model that estimates net infiltration (i.e. groundwater recharge) from annual precipitation (herby referred to as the Williamson Method). The resulting relationship for the San Joaquin Valley region was:

$$PPT_{ex} = (0.64)PPT - 6.2$$

Where:

$$\begin{aligned} PPT_{ex} &= \text{Excess Annual Precipitation (ft/yr);} \\ PPT &= \text{Annual Precipitation (ft/yr)} \end{aligned}$$

It is noted that the Williamson Method applied to the San Joaquin Valley results in no groundwater recharge if average annual precipitation is less than 9.69 inches per year. Results of the net infiltration analysis from Williamson et al., (1989) were used in the development of the Central Valley Groundwater Model developed by the USGS and documented in Faunt (2009).

For each year, annual groundwater recharge from precipitation (i.e. PPT_{ex}) was estimated for each isohyetal zone (see Section 2.3.1.1.1 and Figure 2-27) using the above equation from the Williamson Method. The resulting annual groundwater recharge from areal precipitation for the period 1986/87 to 2016/17 ranged from 0 acre-ft/yr to 219,000 acre-ft/yr with an average of approximately 21,000 acre-ft/yr (see Column A of Table 2-2b) or approximately 7 percent of total precipitation.



2.3.1.2.2 Streambed Infiltration (Channel Loss)

Tule River

The Tule River is a losing stream such that infiltration of surface water within the stream channel recharges the groundwater system beneath it. Total channel loss (i.e. streambed infiltration) in the Tule River between Lake Success and Oettle Bridge is based on TRA annual reports. Streambed infiltration in the Tule River between Oettle Bridge and Turnbull Weir was estimated based on LTRID monthly water use summaries and TRA annual reports. Measured channel loss includes infiltration as well as evapotranspiration. Therefore, infiltration is equal to channel loss, as reported in TRA reports, minus evapotranspiration (described in Section 2.3.1.2.6).

It is noted that there are two sources of water in the Tule River channel: 1) native flow associated with releases from Lake Success and 2) imported water from the Friant-Kern Canal. Surface water in the Tule River channel from Lake Success to Oettle Bridge is exclusively native water (Column B of Table 2-2b). Surface water in the Tule River channel from Oettle Bridge to Turnbull Weir is primarily native flow but periodically includes imported water released to the channel from the Friant-Kern Canal.

As there is no current accounting of Tule River channel loss from Oettle Bridge to Turnbull Weir, it was necessary to estimate it based on available data and an assumed loss factor. The loss factor was based on the assumption that the ratio of streamflow to channel losses upstream of Oettle Bridge is the same as the ratio downstream. Thus, the ratio of streamflow to channel losses observed upstream of Oettle Bridge (the “loss factor”) was applied to measured flow Below Oettle Bridge. The loss factor was applied separately to native Tule River water and imported water releases to develop streambed infiltration estimates specific to both. From water years 1986/87 to 2016/17, average annual streambed infiltration from Success to Oettle Bridge was approximately 16,500 acre-ft/yr (Column B of Table 2-2b). During the same time period, average annual streambed infiltration between Oettle Bridge and Turnbull Weir was approximately 3,200 acre-ft/yr (see Column C of Table 2-2b).

Deer Creek

Deer Creek is a losing stream such that infiltration of surface water within the stream channel recharges the groundwater system beneath it. Streambed infiltration (channel loss) is estimated for the stream reaches between the Fountain Springs gaging station and Trenton Weir and between Trenton Weir and Homeland Canal. The difference in streamflow between Fountain Springs station and Trenton Weir is assumed to be total channel loss along this section. Streambed and canal infiltration in the Deer Creek channel between Trenton Weir and Homeland Canal were estimated based on Pixley Irrigation District monthly water use summaries. Measured channel loss includes infiltration as well as evapotranspiration. Therefore, infiltration is channel loss minus evapotranspiration (described in Section 2.3.1.2.6).



It is noted that there are two sources of water in the Deer Creek channel: 1) native flow and 2) imported water from the Friant-Kern Canal. Imported water is introduced into the Deer Creek channel by the Friant Water Authority via controlled and measured releases from the Friant-Kern Canal upstream of Trenton Weir. Thus, until a stream gage is established upstream of the Friant-Kern Canal/Deer Creek intersection, the separate accounting of losses associated with imported water and native Deer Creek surface flow will have to be approximated.

Deer Creek channel loss from Fountain Springs to Trenton Weir was estimated based on the difference in measured flows between the two stations. The surface flow between these two stations is assumed to be, for this water budget, native Deer Creek water. Average annual infiltration from Fountain Springs to Trenton Weir was approximately 12,100 acre-ft/yr between water years 1986/87 to 2016/17 (see Column D of Table 2-2b).

Flow in the Deer Creek channel from Trenton Weir to Homeland Canal is a combination of native Deer Creek water and imported water purchased by the Pixley Irrigation District for distribution in their service area. For this water balance, it is assumed that all of the water that flows through Trenton Weir is either delivered to riparians and farmers or becomes channel or canal loss (i.e. there is no data available to document surface flow from the Deer Creek channel to Homeland Canal although it is known that this occurs during periods of above normal precipitation). The infiltration of native Deer Creek water in the Deer Creek channel downstream of Trenton Weir is estimated for each month based on Pixley Irrigation District's annual water use summaries in the following way:

1. Imported water deliveries discharged from the Friant-Kern Canal to the Deer Creek channel were subtracted from the total flow measured at Trenton Weir to estimate the volume entering Pixley Irrigation District that is attributed to native Deer Creek flow.
2. Pixley Irrigation District sales and deliveries to basins were subtracted from the total flow through Trenton Weir to determine the volume of water presumably lost as infiltration in the Deer Creek channel and canals.
3. The total loss in No. 2 was multiplied by the ratio of Deer Creek water to total water measured at Trenton Weir to estimate the total losses attributed to native Deer Creek water.
4. A ratio was developed for the length of Deer Creek channel versus the length of canals downstream of the Trenton Weir (0.21).
5. The total loss attributed to native Deer Creek flow, as estimated from No. 3, was multiplied by the ratio of Deer Creek channel length to canal length from No. 4 to estimate the volume of native Deer Creek flow loss estimated to occur in the Deer Creek channel.
6. The volume of native Deer Creek flow lost in canals was estimated as the total loss (No. 3) minus the loss estimated to occur in the Deer Creek channel (No. 5).

Using the methodologies described above, average annual native Deer Creek infiltration from Fountain Springs to Trenton Weir for water years 1986/87 to 2016/17 was 12,100 acre-ft/yr (see



Column D of Table 2-2b). The average annual native Deer Creek infiltration in the Deer Creek channel between Trenton Weir and Homeland Canal was approximately 700 acre-ft/yr (see Column E of Table 2-2b).

White River

All of the surface water flow measured or interpolated at the White River stream gage, after accounting for ET losses, is assumed to become streambed infiltration. Average annual infiltration from White River flow for water year 1986/87 to 2016/17 was estimated to be approximately 5,600 acre-ft/yr (see Column F of Table 2-2b).

2.3.1.2.3 Canal Losses

Canal Losses from Tule River Diversions

A portion of the native Tule River water that is diverted into unlined canals is lost through infiltration into the subsurface groundwater subbasin. For PID, Vandalia Water District, and Woods-Central Ditch Co., delivery losses in unlined canals are accounted for in the portion of the water budget that address deep percolation of applied water.

In the LTRID, canal losses attributed to Tule River diversions are estimated from the District's annual water use summaries reports. Total canal losses within the LTRID (which include both native river water and imported water) are estimated by subtracting streambed infiltration and ET from the total losses reported in the annual water use summaries. Canal losses attributed to native Tule River water are based on the ratio of native Tule River water to imported water (Table 2-2b, Column G). The average annual Tule River canal loss from water years 1986/87 to 2016/17 was approximately 22,300 acre-ft/yr.

Canal Losses from Deer Creek Diversions

It is assumed that canal losses from delivery of native Deer Creek water to riparians and farmers occur only within the Pixley Irrigation District. To estimate canal losses within the Pixley Irrigation District, the estimated infiltration and ET within the Deer Creek channel (see Section 2.3.1.2.6) was subtracted from total losses. The average annual Deer Creek canal loss for water years 1986/87 to 2016/17 was approximately 2,600 acre-ft/yr (see Column H of Table 2-2b).

Canal Losses from Imported Water Deliveries

With the exception of canal losses within the Angiola Water District and PID, imported water that infiltrates into the subsurface groundwater subbasin from the Tule River channel, Deer Creek channel, and unlined canals is grouped together. Within the Angiola Water District and PID, canal losses are accounted for in the portion of the water budget that addresses deep percolation of applied water.



For the LTRID GSA and Pixley Irrigation District GSA areas, imported water losses in channels and canals are estimated by subtracting infiltration losses attributed to native Tule River and Deer Creek water from the total losses estimated to occur in the LTRID and Pixley Irrigation District service areas as documented in their respective annual water use summary reports. The resulting estimate of average annual imported water canal loss for water years 1986/87 to 2016/17 was approximately 50,600 acre-ft (see Column I of Table 2-2b).

2.3.1.2.4 Managed Recharge in Basins

Managed Recharge of Tule River Diversions

Managed recharge (i.e. recharge in basins) of diverted streamflow, imported water, and recycled water is accomplished within the Tule Subbasin via multiple recharge facilities (see Figure 2-7). Native Tule River water is diverted to basins for recharge by Pioneer Water Company, Campbell and Moreland Ditch Company, Vandalia Water District, PID, and LTRID. All of the water diverted to basins by Campbell and Moreland Ditch Company and Vandalia Water District is native Tule River flow. To estimate the portion of basin recharge attributable to native Tule River water in LTRID basins downstream of Oettle Bridge, TH&Co multiplied the ratio of Tule River gaged flow below Oettle Bridge to the total water delivered to the LTRID by the total recharge in basins reported in the LTRID annual water use summaries. Using this methodology, the average annual Tule River recharge in basins from water years 1986/87 to 2016/17 was approximately 11,600 acre-ft (see Column J of Table 2-2b).

Managed Recharge of Deer Creek Diversions

Managed recharge (i.e. recharge in basins) of diverted Deer Creek streamflow is accomplished via multiple recharge facilities (see Figure 2-7). Native Deer Creek water is diverted to basins for recharge by Pixley Irrigation District and DCTRA. Artificial recharge attributed to native Deer Creek water is estimated by multiplying the total recharge in basins reported in Pixley Irrigation District annual water use summaries by the ratio of native Deer Creek water to total water flowing through the Trenton Weir. The average annual Deer Creek recharge in basins for water years 1986/87 to 2016/17 was estimated to be approximately 800 acre-ft/yr (see Column K of Table 2-2b).

Managed Recharge of Imported Water

Managed recharge of imported water is accomplished via multiple recharge facilities within the LTRID, Pixley Irrigation District, PID, Teapot Dome Water District and DEID. Managed recharge attributed to imported water in the LTRID is estimated by multiplying the total recharge in basins reported in annual water use summaries by the ratio of imported water to total surface water flow available. Managed recharge attributed to imported water in the Pixley Irrigation District is estimated by multiplying the total recharge in basins reported in annual water use summaries by



the ratio of imported water to total water flowing through the Trenton Weir. Volumes of imported water delivered to recharge in basins for PID, Teapot Dome Water District, and DEID were provided by the respective agencies. The resulting estimated average annual imported water recharge in basins for water years 1986/87 to 2016/17 was approximately 11,100 acre-ft (see Column L of Table 2-2b).

Recharge of Recycled Water in Basins

A portion of recycled water from the City of Porterville is discharged to basins where it infiltrates into the subsurface. Artificial recharge of recycled water was estimated as 75 percent of all available recycled water from 1990/91 to 2003/04 based on California Regional Water Quality Control Board Order No. R5-2008-0034. Artificial recharge was assumed to be 2,000 acre-ft/yr from 2004/05 to 2009/10 based on Schmidt (2009). The average annual recycled water recharge for water years 1986/87 to 2016/17 was estimated to be approximately 3,200 acre-ft/yr (see Table 2-2b, Column M).

2.3.1.2.5 Deep Percolation of Applied Water

Deep Percolation of Applied Tule River Diversions

A portion of native Tule River water that is delivered and applied for agricultural irrigation is assumed to infiltrate below the root zones of plants and become deep percolation to the groundwater. Deep percolation from irrigated agriculture was applied to the various land uses in the Tule Subbasin according to the irrigation method (e.g. drip irrigation, flood irrigation, micro sprinkler, etc.) for each land use type reported in CDWR on-line land use maps. Irrigation efficiencies were applied to the different irrigation methods based on tables reported in California Energy Commission (2006).

Tule River water is diverted for agricultural irrigation by the Pioneer Water Company, Porter Slough Headgate, Porter Slough Ditch Company, Campbell and Moreland Ditch Company, Poplar Irrigation Company, Woods-Central Ditch Company, Hubbs and Miner Ditch Company, and LTRID. In the LTRID, applied water attributed to native Tule River water is based on the ratio of total native Tule River water entering the LTRID to the total water available to the district (including imports) multiplied by the volume of water delivered for irrigation. Using this methodology, the average annual deep percolation of native Tule River water for water years 1986/87 to 2016/17 was approximately 14,200 acre-ft/yr (see Column N of Table 2-2b).

Deep Percolation of Applied Deer Creek Diversions

The portion of native Deer Creek water delivered for agricultural use within the Pixley Irrigation District is estimated by multiplying the total deliveries reported in Pixley Irrigation District annual water use summaries by the ratio of native Deer Creek water to total water flowing through the



Trenton Weir. Deep percolation of applied Deer Creek diversions is estimated based on the irrigation method (e.g. drip irrigation, flood irrigation, micro sprinkler, etc.) for each land use type reported in DWR on-line land use maps. Irrigation efficiencies were applied to the different irrigation methods based on tables reported in California Energy Commission (2006). From water years 1986/87 to 2016/17, average annual deep percolation of native Deer Creek water was estimated to be approximately 300 acre-ft/yr (see Column O of Table 2-2b).

Deep Percolation of Applied Imported Water

The estimate of imported water delivered and applied to crops within the agencies that receive imported water is based on the total imported water delivery minus losses and recharge in basins. Deep percolation of applied imported water is estimated based on the irrigation method (e.g. drip irrigation, flood irrigation, micro sprinkler, etc.) for each land use type reported in DWR on-line land use maps. Irrigation efficiencies were applied to the different irrigation methods based on tables reported in California Energy Commission (2006). For water years 1986/87 to 2016/17, the estimated average annual deep percolation from imported water was approximately 64,300 acre-ft/yr (see Column P of Table 2-2b).

Deep Percolation of Applied Recycled Water

The estimate of recycled water delivered and applied to crops was provided by the City of Porterville. Deep percolation of applied recycled water is estimated based on the irrigation method (e.g. drip irrigation, flood irrigation, micro sprinkler, etc.) for each land use type reported in DWR on-line land use maps. Irrigation efficiencies were applied to the different irrigation methods based on tables reported in California Energy Commission (2006). For water years 1986/87 to 2016/17, the estimated average annual deep percolation from recycled water was approximately 400 acre-ft/yr (see Column Q of Table 2-2b).

Deep Percolation of Applied Native Groundwater for Agricultural Irrigation

The balance of agricultural irrigation demand not met by imported water or stream diversions is assumed to be met by groundwater pumping. Deep percolation of applied native groundwater is estimated based on the irrigation method (e.g. drip irrigation, flood irrigation, micro sprinkler, etc.) for each land use type reported in DWR on-line land use maps. Irrigation efficiencies were applied to the different irrigation methods based on tables reported in California Energy Commission (2006). For water years 1986/87 to 2016/17, average annual deep percolation from applied agricultural pumping was approximately 145,400 acre-ft/yr (see Column R of Table 2-2b).

Deep Percolation of Applied Native Groundwater for Municipal Irrigation

Deep percolation from applied landscape irrigation was estimated for the urbanized portions of the Tule Subbasin. Because the cities within the Tule Subbasin do not have surface water rights on



the Tule River or Deer Creek and do not purchase imported water, 100 percent of their water demand is met from groundwater pumping. For the City of Porterville, landscape irrigation was estimated to be 47 percent of the total water delivered to each home based on an analysis of the total groundwater production and influent flows to the wastewater treatment plant (City of Porterville draft Urban Water Management Plan 2010 Update, 2014). Of the water used for irrigation, 25 percent was assumed to become return flow.

For the other smaller communities in the Tule Subbasin, wastewater discharge was assumed to be through individual septic systems. For water discharged to septic systems, it was assumed that 100 percent of the discharge became return flow. As with the City of Porterville, 47 percent of total water use was assumed to be for landscape irrigation and 25 percent of the landscape irrigation is assumed to become return flow.

For water years 1986/87 to 2016/17, average annual return flow from municipal production was estimated to be approximately 6,700 acre-ft/yr (see Column S of Table 2-2b).

2.3.1.2.6 Evapotranspiration

Evapotranspiration of Precipitation from Crops and Native Vegetation

Evapotranspiration (ET) is the loss of water to the atmosphere from free-water evaporation, soil-moisture evaporation, and transpiration by plants (Fetter, 1994). Evapotranspiration of precipitation is assumed to be the balance between total precipitation and areal recharge. This value includes evapotranspiration of precipitation from crops as well as native vegetation. From water years 1986/87 to 2016/17, evapotranspiration of precipitation was estimated to average approximately 286,000 acre-ft/yr (see Column T of Table 2-2b, Page 2).

Evapotranspiration of Surface Water within the Tule River Channel

Evapotranspiration of surface water within the Tule River channel is a function of the ET rate and wetted channel surface area. The ET rate was based on published data for riparian vegetation in an intermittent stream (Leenhouts et al., 2005). As the channel width of the Tule River varies, TH&Co identified reaches with similar average channel width using aerial photographs (Google Earth). The ET rate was applied to the surface area of each reach to obtain an estimate of ET. The sum of reach by reach ET estimates between Lake Success and the western Tule Subbasin boundary represents the total Tule River ET shown in Table 2-2b, Page 2, Column U. The resulting average annual ET is approximately 700 acre-ft/yr for water years 1986/87 to 2016/17 (see Table 2-2b, Page 2, Column V).

Evapotranspiration of Surface Water within the Deer Creek Channel

Evapotranspiration within the Deer Creek channel was estimated using the same methodology as for the Tule River. Average annual ET within the Deer Creek channel was estimated to be



approximately 300 acre-ft/yr for water years 1986/87 to 2016/17 (see Table 2-2b, Page 2, Column X).

Evapotranspiration of Surface Water within the White River Channel

Evapotranspiration in the White River channel was estimated using the same methodology as for the Tule River. For water year 1986/87 to 2016/17, the average annual evapotranspiration was estimated to be approximately 100 acre-ft/yr (see Column Y of Table 2-2b, Page 2).

Evapotranspiration of Recycled Water in Basins

Evapotranspiration of recycled water delivered to recharge basins was estimated to be 50 acre-ft/yr (see Column AB of Table 2-2b, Page 2) based on Schmidt (2009).

Agricultural Consumptive Use

Columns U, W, Z, AA and AC of Table 2-2b includes agricultural consumptive use of applied water, not including the portion of the consumptive use met by precipitation, which is included in Column T. Historical agricultural crop water demand (i.e. applied water demand) was estimated based on records of the types and areas of crops grown, estimates of consumptive use for each crop, and estimates of the irrigation efficiency. Information on the types and areas of crops for the LTRID and Pixley Irrigation District were obtained from annual crop surveys from each respective district. The types and areas of crops in other parts of the Tule Groundwater Subbasin within Tulare County were estimated from land use maps and associated data published by the CDWR for 1993, 1999, and 2007 (see Figure 2-31). For the portion of the Subbasin in Kern County (DEID), land use maps were obtained from CDWR (1990) and Kern County Department of Agriculture and Measurement Standards (1999 and 2007). Consumptive use estimates for the various crop types were based on crop coefficients published in ITRC (2003). In order to estimate a total agricultural irrigation water demand, the consumptive use estimates for each crop were multiplied by the area of the crop, which in turn was multiplied by a return flow factor reflecting the irrigation efficiency (see Section 2.3.1.2.5).

The estimated average annual agricultural consumptive use for the period of the groundwater budget was approximately 773,900 acre-ft/yr (sum of Columns U, W, Z, AA and AC of Table 2-2b).

Municipal Consumptive Use

Consumptive use of landscaping associated with applied municipal groundwater pumping was estimated based on an assumed applied water to landscaping and return flow factor. As presented in Section 2.3.1.2.5, it is assumed 47 percent of municipal water use is applied to landscaping. It is assumed that 75 percent of applied water to landscaping is consumptively used by the plants and



25 percent becomes return flow. For water years 1986/87 to 2016/17, estimated average annual municipal consumptive use was approximately 6,800 acre-ft/yr (see Column AD of Table 2-2b).

2.3.1.2.7 Surface Water Outflow

Tule River

Any residual stream flow in the Tule River that reaches the Turnbull Weir, located at the west (downstream) end of the Tule Subbasin, is assumed to flow out of the subbasin (see Figure 2-7). From water years 1986/87 to 2016/17, surface water outflow ranged from 0 to 121,000 acre-ft/yr and averaged 14,000 acre-ft/yr (see Table 2-2b, Page 2, Column AE).

It is noted that additional outflow may occur at smaller canal outlets at the west end of the Tule Subbasin. The data for these outflows was unavailable for this report.

Deer Creek

During periods of above-normal precipitation, residual stream flow left in the Deer Creek after diversions has historically flowed into Homeland Canal, located at the west end of the Tule Subbasin (see Figure 2-7). The data for this outflow was unavailable for this report (see Column AF of Table 2-2b, Page 2). As this data becomes available, it will be incorporated into the surface water budget.

2.3.2. Groundwater Budget §354.18 (b)(2)

The groundwater budget describes the sources and estimates the volumes of groundwater inflow and outflow within the Tule Subbasin (see Table 2-3). A fundamental premise of the groundwater budget is the following relationship:

$$\text{Inflow} - \text{Outflow} = +/- \Delta S$$

Inflow terms include groundwater recharge to the subbasin including areal recharge from precipitation, recharge in stream/river channels, artificial recharge, canal losses, return flow, release of water from compression of aquitards, and subsurface inflow. It is noted that many of the groundwater inflow terms are surface water outflow terms from Table 2-2b. Outflow terms include groundwater pumping, evapotranspiration, and subsurface outflow. The difference between the sum of inflow terms and the sum of outflow terms is the change in groundwater storage (ΔS) (see Table 2-3).

As with the surface water budget tables, the individual columns in the groundwater budget table are color coded to reflect their role in the Sustainable Yield estimate. Sources of groundwater recharge (i.e. inflow) that are associated with pre-existing water rights and/or imported water



deliveries are indicated with magenta-colored columns in Table 2-3 and are not used to estimate the Sustainable Yield. Groundwater recharge elements that are used to estimate Sustainable Yield are indicated with blue-colored columns. Groundwater pumping is not used in the equation to estimate Sustainable Yield and is shown as yellow-colored columns in Table 2-3.

2.3.2.1 Sources of Groundwater Recharge §354.18 (b)(2)

§ 354.18. (b) (2) Inflow to the groundwater system by water source type, including subsurface groundwater inflow and infiltration of precipitation, applied water, and surface water systems, such as lakes, streams, rivers, canals, springs and conveyance systems.

2.3.2.1.1 Areal Recharge

Groundwater recharge from precipitation falling on the valley floor in the Tule Subbasin was estimated based on Williamson et al., (1989) (see Section 2.3.1.1.1). The resulting annual groundwater recharge from areal precipitation using this method ranged from 0 acre-ft/yr to 219,000 acre-ft/yr with a 31-yr average of approximately 21,000 acre-ft/yr (see Column A, Table 2-3).

2.3.2.1.2 Groundwater Recharge from the Tule River

Groundwater recharge of native Tule River water occurs as streambed infiltration, infiltration of water in unlined canals, recharge in basins, and deep percolation of applied water. Tule River water that becomes groundwater recharge is described in Section 2.3.1.2 and summarized in Columns B through F of Table 2-3. Average annual groundwater recharge of native Tule River water was estimated to be approximately 67,800 acre-ft/yr for water years 1986/87 to 2016/17.

2.3.2.1.3 Groundwater Recharge from Deer Creek

Groundwater recharge of native Deer Creek water occurs as streambed infiltration, canal loss, recharge in basins, and deep percolation of applied water. Deer Creek water that becomes groundwater recharge is described in Section 2.3.1.2 and summarized in Columns G through K of Table 2-3. For water years 1986/87 to 2016/17 average annual groundwater recharge of native Deer Creek water was estimated to be approximately 16,500 acre-ft/yr.

2.3.2.1.4 Streambed Infiltration in the White River

Groundwater recharge of White River water occurs as streambed infiltration as described in Section 2.3.1.2 and summarized in Column L of Table 2-3. Estimated average annual groundwater recharge from White River water was approximately 5,600 acre-ft/yr for water years 1986/87 to 2016/17.



2.3.2.1.5 Groundwater Recharge from Imported Water Deliveries

Groundwater recharge of imported water occurs as canal loss, recharge in basins, and deep percolation of applied water as described in Section 2.3.1.2 and summarized in Columns M through O of Table 2-3. For water years 1986/87 to 2016/17 average annual groundwater recharge from imported water was estimated to be approximately 126,000 acre-ft/yr.

2.3.2.1.6 Recycled Water

Groundwater recharge of recycled water occurs as artificial recharge and return flow of applied water as described in Section 2.3.1.2 and summarized in Columns R and S of Table 2-3. For water years 1986/87 to 2016/17 average annual groundwater recharge from recycled water was estimated to be approximately 3,600 acre-ft/yr.

2.3.2.1.7 Deep Percolation of Applied Water from Groundwater Pumping

A portion of irrigated agriculture and municipal applied water from groundwater pumping becomes deep percolation and groundwater recharge as described in Section 2.3.1.2.5 and summarized in Columns P and Q of Table 2-3. For water years 1986/87 to 2016/17 average annual groundwater recharge associated with return flow from groundwater pumping was estimated to be approximately 152,100 acre-ft/yr.

2.3.2.1.8 Release of Water from Compression of Aquitards

Prolonged lowering of groundwater levels in the Tule Subbasin results in the drainage of water from low permeability subsurface aquitards that occur beneath the potentiometric groundwater surface. Aquitards are low permeability layers with relatively high silt and clay content. As the aquitards are compressible, the release of pore pressure caused by the lowering of groundwater levels also results in compression of the low permeability layers. Within a limited range of groundwater level fluctuation, the compressed aquitard can accept water back into its structure when groundwater levels rise resulting in elastic rebound. However, if groundwater levels are maintained at low elevations for long enough periods of time as a result of groundwater pumping, the compression of aquitards becomes permanent. This permanent compression of subsurface layers results in land surface subsidence, which has been observed in the Tule Subbasin prior to 1970 (Ireland et al., 1984) and between 2007 and 2011 (Luhdorff and Scalmanini, 2014). The slow release of water from the permanent compaction of subsurface aquitards also results in a one-time contribution of water to the aquifer system. However, it is noted that this is not a renewable source of water to the aquifer.

The estimate of the volume of water contributed to the aquifer through compression of aquitards between 1986 and 2017 was based on groundwater flow model analysis and output using the subsidence package in MODFLOW. The total volume of water contributed to the aquifer from



aquitard compression during this time period is estimated to be approximately 2,400,000 acre-ft with an annual average of approximately 77,000 acre-ft/yr (see Column T of Table 2-3).

2.3.2.1.9 Subsurface Inflow

The Tule Subbasin is not a closed basin and the aquifer is in hydrologic connection with adjacent subbasins to the north, west and south. Groundwater flow into and out of the Tule Subbasin along these boundaries varies over time in accordance with the groundwater level conditions and flow patterns within and outside the subbasin. The only source of subsurface inflow to the Tule Subbasin along the eastern boundary is mountain-front inflow resulting from infiltration of precipitation in the secondary porosity features (joints and fractures) of the bedrock east of the basin and along the mountain front. This recharge enters the alluvial groundwater basin where the alluvium is in hydrologic connection with the fractures in the bedrock in the subsurface.

A summary of subsurface inflow values estimated for 1986/87 to 2016/17 is provided in Table 2-3 (Column U). As shown, inflow through the southern and western boundary across both the shallow and deep aquifers ranges from 83,000 acre-ft in 2009/10 to 144,000 acre-ft in 1990/91 with an average over the years of interest of 118,000 acre-ft/yr. The average net inflow into the Tule Subbasin along the south and west boundaries for the time period is approximately 53,000 acre-ft/yr after accounting for outflow (see Section 2.3.2.3.4).

2.3.2.1.10 Mountain Front Recharge

Mountain front recharge represents the infiltration of precipitation into the fractures in the bedrock east of the Tule Subbasin, which eventually flows into the alluvial aquifer system of the Tule Subbasin in the subsurface where the fractured rock aquifer system is in hydrologic communication with the alluvial aquifer system. Subsurface inflow along the eastern Tule Subbasin boundary was estimated through a parameter estimation calibration process of the groundwater flow model of the subbasin. In this calibration method, the model was given a wide range of potential recharge along the eastern Tule Subbasin. The model automatically varied aquifer parameters and mountain-front recharge through an iteration process until it arrived at an optimum fit of measured and model-generated groundwater levels. Tule Subbasin mountain-front recharge that resulted in the best model calibration was approximately 29,000 acre-ft/yr (see Column V of Table 2-3 and Column J of Table 2-4).

2.3.2.2 Sources of Groundwater Discharge §354.18 (b)(3)

§ 354.18. (b) (3) Outflows from the groundwater system by water use sector, including evapotranspiration, groundwater extraction, groundwater discharge to surface water sources, and subsurface groundwater outflow.



2.3.2.2.1 Municipal Groundwater Pumping

Groundwater pumping for municipal supply is conducted by the City of Porterville and small municipalities for the local communities in the Tule Subbasin as described in Section 2.3.1.1.5. For water years 1986/87 to 2016/17, municipal groundwater production was estimated to average approximately 19,400 acre-ft/yr (see Column W of Table 2-3, Page 2).

2.3.2.2.2 Agricultural Groundwater Pumping

Agricultural groundwater production is estimated as the total applied water demand for crops minus surface deliveries. The estimated average annual discharge to crops from wells for water years 1986/87 to 2016/17 is approximately 664,000 acre-ft/yr (see Column X of Table 2-3, Page 2).

2.3.2.2.3 Groundwater Pumping for Export Out of the Tule Subbasin

Some of the groundwater pumping that occurs on the west side of the Tule Subbasin is exported out of the subbasin for use elsewhere. Angiola Water District and the Boswell/Creighton Ranch have historically exported pumped groundwater out of the Tule Subbasin. Annual groundwater exports have ranged from 0 between 1995 and 1999 to 63,640 acre-ft in the 2012/13 water year (see Column Y of Table 2-3, Page 2) with the average for water years 1986/87 to 2016/17 of 28,200 acre-ft/yr. This water is accounted for separately because the water is not applied within the subbasin and there is no associated return flow.

2.3.2.2.4 Subsurface Outflow

Outflow estimates (Table 2-3; Column AA) range from 51,000 acre-ft in 1988/89 to 92,000 acre-ft in 2009/10, with an average of 65,000 acre-ft/yr.

2.3.2.3 Changes in Groundwater Storage §354.18 (b)(4)

§ 354.18. (b) (4) The change in the annual volume of groundwater in storage between seasonal high conditions.

Comparison of the groundwater inflow elements of the water budget with the outflow elements shows a cumulative change in groundwater storage over the period between 1986/87 to 2016/17 of approximately -4,948,000 acre-ft (see Table 2-3). The average annual change in storage resulting from the groundwater budget is approximately -160,000 acre-ft/yr. It is noted that this time period was used as it matches the calibration period for the Tule Subbasin groundwater flow model used to evaluate future projects and management actions for the subbasin. However, the average hydrology over the time period is relatively dry (see Figure 2-28) and the resulting change in storage is not representative of long-term average conditions. A groundwater change in storage



value representative of average hydrological conditions is provided in Section 2.3.2.5 for the period 1990/91 to 2009/10.

2.3.2.4 Overdraft §354.18 (b)(5)

§ 354.18. (b) (5) If overdraft conditions occur, as defined in Bulletin 118, the water budget shall include a quantification of overdraft over a period of years during which water year and water supply conditions approximate average conditions.

The average annual change in groundwater storage over the period from 1990/91 to 2009/10, which represents average hydrologic conditions within the Tule Subbasin, was approximately -115,300 acre-ft/yr. This value represents the average annual historical overdraft of the subbasin.

2.3.2.5 Water Year Type §354.18 (b)(6)

§ 354.18. (b) (6) The water year type associated with the annual supply, demand, and change in groundwater stored.

All water budget elements and change in groundwater storage presented herein are based on a water year, which begins October 1 and ends September 30. Water year types with respect to hydrologic conditions (i.e. above average, average or below average precipitation conditions based on Figure 2-28) are shown in the historical water budget tables (Tables 2-2a, 2-2b, and 2-3).

2.3.2.6 Sustainable Yield §354.18 (b)(7)

§ 354.18. (b) (7) An estimate of sustainable yield for the basin.

Sustainable yield is defined in the Sustainable Groundwater Management Act (SGMA) Chapter 2, §10721 (v) as:

The maximum quantity of water, calculated over a base period representative of long-term conditions in the basin and including any temporary surplus, that can be withdrawn annually from a groundwater supply without causing an undesirable result.

The Sustainable Yield of the Tule Subbasin is a function of the overall water balance of the area. Changes in surface water/groundwater inflow to the basin and surface water/groundwater outflow from the basin impact the Sustainable Yield. As groundwater management and land use changes impact the water balance, they also impact the Sustainable Yield. A generalized expression of the water balance is as follows:



$$\text{Inflow} - \text{Outflow} = +/- \text{Change in Storage} \quad (1)$$

The water balance equation for pre-developed conditions (prior to human occupation) can be further expressed as:

$$(I_{pr} + I_{str} + I_{ss} + I_{mb}) - (O_{ss} + O_{et}) = \Delta S \quad (2)$$

Where:

I_{pr} = Inflow from Areal Recharge of Precipitation

I_{str} = Inflow from Infiltration of Runoff in Stream Beds

I_{ss} = Inflow from Subsurface Underflow

I_{mb} = Inflow from Mountain-Block Recharge

O_{ss} = Subsurface Outflow

O_{et} = Evapotranspiration

ΔS = Change in Groundwater Storage

Under pre-developed conditions, the groundwater basin would be in a state of equilibrium such that the inflow and outflow would balance and there would be no significant long-term change in storage assuming a static climatic condition. Under this condition, groundwater levels would be relatively stable.

Under developed land use conditions, the water balance changes as groundwater is pumped from the basin for irrigation and municipal supply. Lowering of the groundwater table resulting from pumping reduces the amount of groundwater that would otherwise leave the basin and reduces evapotranspiration losses in areas of shallow groundwater (e.g. Tulare Lake). Some of the pumped groundwater used for irrigation infiltrates past the roots of the plants and returns to the groundwater as return flow. Water imported into the area is applied to crops but some is lost as infiltration in unlined canals and as return flow. Groundwater return flow also occurs as a result of discharges from individual septic systems. Other sources of recharge to the groundwater under developed land use include wastewater treatment plant discharges and artificial recharge in spreading basins.

The water balance equation for developed land use conditions can be modified as follows:

$$(I_{pr} + I_{str} + I_{can} + I_{ar} + I_{rgw} + I_{rfimp} + I_{com} + I_{ss} + I_{mb}) - (O_{ss} + O_{et} + O_p) = \Delta S \quad (3)$$

Where:

I_{can} = Inflow from Canal Losses



I_{ar} = Inflow from Artificial Recharge

I_{rfgw} = Inflow from Return Flow of Applied Water from Groundwater Pumping

I_{rfimp} = Inflow from Return Flow of Applied Water from Imported Water

I_{com} = Inflow of Water Released from Compression of Aquitards

O_p = Outflow from Groundwater Pumping

If the inflow terms exceed the outflow terms, then the groundwater in storage increases (become positive) and groundwater levels rise. If the outflow terms exceed the inflow, then the groundwater in storage decreases (become negative) and groundwater levels drop. It is assumed that the Sustainable Yield of the Tule Subbasin is the long-term average groundwater pumping rate, under projected land use conditions, that results in no significant long-term net negative change in groundwater storage in the basin. Based on this premise, the water balance equation can be rearranged and simplified to estimate Sustainable Yield:

$$\text{Sustainable Yield} = \Delta S + O_p - I_{can} - I_{ar} - I_{rfimp} - I_{com} \quad (4)$$

Thus, if the change in groundwater storage over the planning period is zero and there is no imported water or release of water from compression of aquitards, then the Sustainable Yield is equal to the pumping. This relationship is valid if the following conditions are met:

1. The Sustainable Yield incorporates a hydrology that is representative of a relatively long period of record that includes multiple wet and dry hydrologic cycles.
2. The land use conditions are representative of the time period.

The Sustainable Yield can also be expressed as all of the components of the water balance not explicitly expressed in Equation 4:

$$\text{Sustainable Yield} = I_{pr} + I_{str} + I_{rfgw} + I_{ss} + I_{mb} - O_{ss} \quad (5)$$

It is noted that the Tule Subbasin Technical Advisory Committee has determined that recharge to the Tule Subbasin associated with the delivery of imported water and the diversion of water from the Tule River and Deer Creek associated with Pre-1914 water rights will not be included in the Sustainable Yield of the subbasin. This includes canal losses from delivery of imported water and diverted stream flow, deep percolation of applied imported water and diverted stream flow, and managed recharge in basins.

Applying Equations 4 and 5 to the historical water budget of the Tule Subbasin does not result in a representative Sustainable Yield because the subbasin was in overdraft during the historical water budget period. Groundwater pumping depressions that have developed in the western portion of the subbasin have historically captured groundwater that would have otherwise left the subbasin.



This increase in groundwater inflow and subsequent decrease in groundwater outflow increased the apparent Sustainable Yield, which was reported to be approximately 257,725 acre-ft/yr based on the water budget from water year 1990/91 to 2009/10 (TH&Co, 2017). However, since the downward groundwater trends that resulted in this condition are not sustainable, the associated Sustainable Yield from this water budget is not representative.

The Sustainable Yield of the Tule Subbasin will change in the future as a result of changes in groundwater levels and flow associated with planned projects and management actions and changes in deep percolation of applied water (i.e. return flow) from reduced groundwater pumping. Most of the GSAs in the subbasin plan management actions that include a reduction in irrigated acreage to address the need to reduce groundwater production. This necessary action will change the water budget by not only decreasing outflow from groundwater pumping but also reducing deep percolation of applied water (return flow) and changing the dynamics of inflow and outflow at the subbasin boundaries. This new water budget regime will result in a Sustainable Yield that is different from what was realized historically. Thus, the Sustainable Yield of the Tule Subbasin presented herein was estimated based on the projected future water budget (see Section 2.3.5), which is more representative than the Sustainable Yield from the historical water budget.

The projected water budget that was the basis for the Sustainable Yield estimate was developed using a calibrated groundwater flow model of the Tule Subbasin (TH&Co, 2020). The projected water budgets incorporated all planned projects and management actions of the Tule Subbasin GSAs as well as adjustments to hydrology and water deliveries from climate change guidelines provided by the CDWR (see Section 2.3.5). In order to address uncertainty in the model results, the projected water budget was initially analyzed with 240 realizations of the groundwater flow model. In each realization, aquifer parameters, consumptive use, and mountain front recharge were varied within acceptable ranges that produced acceptable overall model calibrations. The resulting water budgets were processed, based on Equation 5 above, to produce Sustainable Yield estimates for each year of the 50-yr implementation and planning horizon (2020 to 2070). Of the original 240 model realizations, 175 resulted in a projected average annual change in groundwater storage greater than -5,000 acre-ft/yr. The average Sustainable Yield for the time period from 2040 to 2050 was used as the Sustainable Yield for the 175 model realizations resulting in greater than -5,000 acre-ft/yr of annual storage change. The 175 estimates of Sustainable Yield formed a normal distribution when plotted (see Figure 2-32). The time period from 2040 to 2050 was selected because it occurs after all planned projects and management actions have been implemented but before the time when long-term climate change adjustments to hydrology and water deliveries are applied to the projected water budget (2050). The long-term climate change adjustments were not considered as reliable as the near-term adjustments.

The projected future Sustainable Yield of the Tule Subbasin, which is the 50th percentile of the distribution of estimates derived from the uncertainty analysis, is estimated to be approximately 130,000 acre-ft/yr (see Table 2-4). The plausible range of Sustainable Yield was selected as the



values between the 20th and 80th percentile, resulting in a range of approximately 108,000 to 162,000 acre-ft/yr (see Figure 2-32). The projected Sustainable Yield does not include:

- Water released to the aquifer system from the compression of aquitards,
- Diverted Tule River water canal losses, recharge in basins, and deep percolation of applied water,
- Diverted Deer Creek water canal losses, recharge in basins, and deep percolation of applied water,
- Imported water canal losses, recharge in basins, and deep percolation of applied water, and
- Deep percolation of applied recycled water and recycled water recharge in basins.

Each GSA will determine their allowable groundwater pumping by multiplying that GSA's proportionate areal coverage of the Tule Subbasin times the total Sustainable Yield of the subbasin (130,000 acre-ft/yr), as described in the Coordination Agreement. The estimated consumptive use rate that can be sustained under the Subbasin-wide Sustainable Yield is 65,000 acre-ft/yr. When applied across the entire 475,895 acres of the subbasin, this consumptive use rate is approximately 0.14 acre-ft/acre. This consumptive use rate incorporates consumptive use from both agriculture and municipal demand. This "sustainable" consumptive use rate does not equal the Sustainable Yield on an acre-ft/acre basis because it does not account for irrigation return flow and changes to subbasin inflow and outflow caused by changes in pumping stress within the subbasin. It is noted that the consumptive use rate of 0.14 acre-ft/acre is for irrigation water only (i.e. does not include consumptive use of precipitation) and is the baseline sustainable consumptive use as applied across the entire subbasin. Each GSA will individually estimate their total allowable consumptive use as the sum of the baseline sustainable consumptive use, available precipitation, and surface water supplies.

As additional data become available and as projects and management plans are implemented, the groundwater flow model used to estimate the Sustainable Yield of the Tule Subbasin will be updated and the Sustainable Yield may be adjusted to reflect the new data.

2.3.3. Current Water Budget §354.18 (c)(1)

§ 354.18. (c) Each Plan shall quantify the current, historical, and projected water budget for the basin as follows:

- (1) Current water budget information shall quantify current inflows and outflows for the basin using the most recent hydrology, water supply, water demand, and land use information.

The surface water and groundwater budget for the Tule Subbasin in 2017 is shown in Tables 2-2a, 2-2b, and 2-3. Total groundwater inflow to the subbasin for water year 2016/17 was approximately 855,000 acre-ft. Total groundwater outflow from the subbasin for water year 2016/17 was approximately 550,000 acre-ft. The net change in storage during the water year was approximately 305,000 acre-ft.

